PRELIMINARY DRAINAGE REPORT

for THE COMMONS AT FALCON FIELD

El Paso County, Colorado

June 2024

PCD FILE NO. SP-232

Prepared for:

Falcon Field, LLC

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PRELIMINARY DRAINAGE REPORT

for

THE COMMONS AT FALCON FIELD

Falcon, Colorado

1.0 CERTIFICATION STATEMENTS

ENGINEER'S STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by El Paso County for drainage reports, and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omission on my part in preparing this report.

Tim D. McConnell, P.E. Colorado P.E. License No. 33797 For and on Behalf of Drexel, Barrell & Co.

DEVELOPER'S STATEMENT

I, the developer have read and will comply with all the requirements specified in this drainage report and plan.

Business Name: Falcon Field, LLC.

By:

PJ Anderson Title: Owner Address: 30 N. Tejon St., #516 Colorado Springs, CO 80903 Date

EL PASO COUNTY

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Criteria Manual, as amended.

Joshua Palmer, P.E. County Engineer/ECM Administrator CONDITIONS: Date

Date

PRELIMINARY DRAINAGE REPORT

for THE COMMONS AT FALCON FIELD Falcon, Colorado

2.0 PURPOSE

This report is prepared by Drexel, Barrel & Co in support of The Commons at Falcon Field project. The purpose of this report is to identify onsite and offsite drainage patterns, storm sewer, inlet locations, and areas tributary to the site, and to safely route developed storm water runoff to adequate outfall facilities.

3.0 GENERAL SITE DESCRIPTION

<u>Location</u>

The Commons at Falcon Field site is approximately 57.7 acres and is bounded by U.S. Highway 24 along the northwest, a school to the south, and a large-lot residential development to the east and northeast. The site is in the east half of Section 7, Township 13 South, Range 64 West of the 6th PM.

Drainage Fees will be assessed and paid according to the current rates at the time of platting. All easements for utilities and drainage features will be provided with the final plat process.

Existing Site Conditions

The site is currently open grass land with one single-family residence and barn. The residence is supported by a well and individual septic system. There are no known utilities on site. Offsite runoff enters the site through a box culvert under Highway 24, along the northern boundary of the property. The box culvert discharges through the site in an open drainage to the south. Smaller offsite basins, including Highway 24 along the northern boundary currently discharge onto the property, these basins are further described below.

Proposed Site Conditions

The Commons at Falcon Field is a proposed mixed-use commercial and residential development and is proposed to consist of 169 single-family lots and 8 commercial pads, along with associated roadways and open space. This development is anticipated to be phased into three separate areas – commercial, south residential and east residential.

Soils

According to the Soil Survey of El Paso County Area, Colorado, prepared by the U.S. Department of Agriculture Soil Conservation Service, the site is partially underlain by

Blakeland Loamy Sand (Soil No. 8), and predominantly by Columbine gravelly sandy loam (Soil No. 19). Both soils are type 'A' hydrological soil group. See appendix for map.

<u>Climate</u>

This area of El Paso County can be described as the foothills, with total precipitation amounts typical of a semi-arid region, roughly 15 inches annually. The climate of the site is typical of a sub-humid to semi-arid climate with mild summers and winters. The average temperature is 31 degrees F in the winter and 68.4 degrees F in the summer.

Floodplain Statement

The Flood Insurance Rate Maps (FIRM No. 08041C0553-G & 08041C0561-G both dated 12/7/18) indicate that there is a Zone A floodplain area that covers the "Falcon Creek East Tributary" that bisects the site, but this area is not a designated regulatory floodway. This reach of the channel is the subject of a FEMA floodplain study currently being completed by separate report and analysis.

Previous Drainage Studies

The site is located within the East Tributary Basin of the Falcon Basin Watershed, as studied in the Falcon Drainage Basin Planning Study, prepared by Matrix Design Group, September, 2015. DBPS recommendations are presented later in this report.

4.0 DRAINAGE CRITERIA

The drainage analysis has been prepared in accordance with the current El Paso County Drainage Criteria Manual. Calculations were performed to determine runoff quantities during the 5-year and 100-year frequency storms for historic and developed conditions using the Rational Method as required for basins containing less than 100 acres.

In addition, the following Mile High Flood District (MHFD) provided spreadsheet MHFD-Detention v4.04 was used for preliminary design of the detention facilities.

5.0 DBPS ANALYSIS

Existing Conditions

The Falcon DBPS watershed establishes three major basins, including the "East Tributary" which covers this property. The DBPS completed hydrologic analysis for the Falcon Basin Watershed, using HEC-HMS v.3.5 software, for historical, existing and future land use conditions by applying a 24-hour storm event with 2-, 5-, 10-, 25-, 50-, and 100-year recurrence intervals and current drainage conveyance infrastructure.

As mentioned earlier, offsite flows from the Woodmen Hills Detention Pond #4 enter the Commons at Falcon Field site via two 4.83'x12' box culverts underneath U.S. Highway 24 (DBPS identifier ET14), these combine with onsite flows and follow the historic reach RET100 of the Falcon Creek East Tributary to the south.

The following table details the HEC-HMS analysis of existing conditions across the Commons at Falcon Field development.

	Existing Conditions (source: Falcon Basin, Drainage Planning Study, HEC-HMS model)								
Location	HEC-		Peak Flow (cfs)						
	HMS Element	Area (sq mi)	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr	
East tributary at North									
Property Line of	RET090	1.66	14	36	55	170	230	320	
Commons at Falcon Field									
East tributary through Commons at Falcon Field	RET100	1.78	15	39	64	170	270	370	
Local Basin	ET100	0.05	1	6	10	21	27	34	
East tributary South of Commons at Falcon Field Property Line	RET110	1.83	15	40	65	170	270	380	

Peak Discharges for the Existing Condition at Points of Interest in vicinity of The Commons at Falcon Field Development (DBPS)

The DBPS flow rates shown in the table above were used as the basis of the existing condition analysis of the Commons at Falcon Field development. Site specific basins have been allocated and referenced on the existing conditions map in the appendix.

The Falcon DBPS recommends junction and reach improvements for RET100 (reach through project site) and subsequent reach RET110 downstream junction ET13 at Pinto Pony to Falcon Highway. The existing culvert at Highway 24 was identified as undersized, but not included in the DBPS recommendations as it is a CDOT owned structure. The improvements include the following recommendations:

Reach RET100 – Installation of small drop structures with toe protection Reach RET110 – Installation of small drop structures with toe protection Junction ET13 (Pinto Pony) – replace existing crossing with (2) 6'x8' culverts Junction ET11 (Falcon Highway) – replace existing crossing with (2) 6'x8' culverts

The Commons at Falcon Field development proposes regrading and rerouting a portion of the East Tributary. The proposed improvements will intercept the Highway 24 (CDOT owned) culvert immediately south of the Highway 24 and convey via a public 10'x4' concrete box culvert 750-If to the south through the project site towards an open channel. The proposed public box culvert will discharge to the proposed open channel via a headwall. The proposed open channel conveys the flow 275-If downstream to tie into the existing creek and will be vegetated with mowable short grasses. The open channel is proposed with a 20-foot bottom width in a v-shape with two 10-foot sections set as a 2% slope to the invert. Despite this drainageway being identified in the DBPS as a County cost item, this box culvert is proposed to be privately owned and maintained. A non-exclusive permanent easement will be provided at Final Plat outlining restrictions and responsibilities within the easement area. Hydraulic analysis of the drainageway downstream of the Commons at Falcon Marketplace project will be completed at the final plat stage of development. See section 11.0 of this report for further discussion.

6.0 EXISTING CONDITION

In addition to the DBPS, a site specific analysis of the existing conditions was completed. The flows determined by the DBPS for the tributary entering the site from the north (RET090), were used in combination with rational method analysis for the surrounding onsite/offsite flows. For this preliminary analysis, the DBPS flows were directly added to the rational method flows. Further analysis of the flows will be completed with the CLOMR study.

BASIN & DESIGN POINT SUMMARY							
BASIN	DP	AREA (AC)	Q5 (cfs)	Q100 (cfs)			
OS1	А	1.34	3.4	7.6			
E1		13.85	3.2	22.4			
RET090 (DBPS)		-	36.0	320.0			
DPA+E1+RET090	В	15.19	41.0	346.4			
OS2	С	0.60	1.4	3.2			
OS3	D	2.56	0.7	4.5			
E2		12.88	2.5	18.6			
DPC+DPD+E2	E	16.04	3.8	23.9			
E3	F	13.11	2.7	19.6			
OS4	G	1.54	1.6	4.8			
E4		1.57	0.3	2.6			
DPG+E4	Н	3.11	1.5	6.1			
E5		5.91	2.2	11.7			
OS5	J	16.62	6.2	22.6			
OS6	L	0.91	2.6	5.5			
E6		10.37	1.7	12.5			
DPJ+DPL+E6	М	27.89	7.4	30.7			

RATIONAL METHOD RUNOFF SUMMARY

RET090 represents the upstream watershed tributary to the Falcon Field project. This area is identified as RET090 in the DBPS and is replicated here for clarity. DBPS established flows of Q_5 =36 cfs and Q_{100} =320 cfs currently discharge into an open channel on the Falcon Field property via existing dual 12'Hx4.83'W box culverts under Highway 24. There is an 8' concrete vertical drop immediately downstream of the culvert, then a short riprap channel section before the open channel returns to a vegetated section through the site.

Basin OS1 represents a portion of the southern half of U.S. Highway 24 along the northwest boundary for the Commons at Falcon Field site. Due to no curb and gutter along this stretch of U.S. Highway 24, flows from this basin discharge directly into basin E1 as overland flow and are represented by **Design Point DPA**. Runoff rates at existing DPA are $Q_5=3.4$ cfs and $Q_{100}=7.6$ cfs.

Basin E1 covers 13.85 acres of open space in the northwestern portion of the site. Flows from this basin combine with those from DPA and travel towards the existing open vegetated channel at rates of Q_5 =3.2 cfs and Q_{100} =22.4 cfs. These flows are consistent with those established by the DBPS for the local basin, see table above. These flows combine with those from the DBPS RET090 at **Design Point DPB** and discharge to the south as defined channel flow at rates of Q_5 =41.0 cfs and Q_{100} =346.4 cfs. As previously mentioned for the purposes of this preliminary analysis, the DBPS flows were directly added to the Rational Method flows. Further detailed flow analysis will be completed as part of the CLOMR study.

Basin OS2 represents the remainder of the southern half of U.S. Highway 24 along the northwest boundary for the Commons at Falcon Field site. Due to no curb and gutter along this stretch of U.S. Highway 24, flows from this basin discharge as overland flow directly into basin E2 and are represented by **Design Point DPC**. Runoff rates at existing DPC are $Q_5=1.4$ cfs and $Q_{100}=3.2$ cfs.

Basin OS3 is located along the southeastern edge of Basin E2. This basin consists of native grasses and vegetation, and a small outbuilding. The flows within this basin travel to the southwest where they will discharge as overland flow into basin E2 at **Design Point DPD**. The runoff rates entering basin E2 at DPD are $Q_5=0.7$ cfs and $Q_{100}=4.5$ cfs.

Basin E2 is 12.88 acres of open space located to the west of Basin E1. The basin is sloped to the southeast at roughly 3% before turning directly south upon reaching the eastern border of the basin. Flows combine with those from Basin OS2 then travel south until roughly halfway down the basin where Basin OS3 adds to the flows. From there the combined flows from Basins OS2, OS3, and E2 continue to the south as overland flow where they are released from the site at **Design Point DPE** at rates of Q₅=3.8 cfs and Q₁₀₀=23.9 cfs.

Basin E3 represents 13.11 acres in the southwest corner of the site. Basin E3 directs flows from the north and south to the southern border, exiting the site as overland flow with runoff rates of $Q_5=2.7$ cfs and $Q_{100}=19.6$ cfs at **Design Point DPF**.

Basin OS4 runs down the western side of the site and includes a portion of the southern edge of U.S. Highway 24. The 1.54 acre, offsite basin, generates flows that will travel to the south until they reach **Design Point DPG** at the bottom of the basin. Where they will enter Basin E4 as overland flow at rates of $Q_5=1.6$ cfs and $Q_{100}=4.8$ cfs.

Basin E4 is a small, 1.57-acre basin on the far western side of the site. The basin will receive offsite flows from Basin OS4 before directing all of flow south where it exits the western side of the site as overland flow at **Design Point DPH**, with runoff rates of $Q_5=1.5$ cfs and $Q_{100}=6.1$ cfs.

Basin E5 is 5.91 acres located on the eastern side of the site, sandwiched between the southern portions of Basin E1 and E6. The basin directs all of its flows south as overland flow towards the existing **Design Point DPG** which sits on the southern border of the site. This basin generates runoff rates of $Q_5=2.2$ cfs and $Q_{100}=11.7$ cfs.

Basin OS5 is an offsite basin located to the north of Rio Lane and includes the northern half of Rio Lane. Runoff generated by this basin ($Q_5=6.2$ cfs and $Q_{100}=22.6$ cfs) is captured by a roadside ditch and travels towards an existing 18" CMP culvert underneath Rio Lane, located approximately two-thirds of the way along the project boundary. These flow rates will be used for comparison in this report, however the full-flow capacity of this existing 18" CMP culvert at 1.0% (field-surveyed grade) is significantly less ($Q_{100}=6.6$ cfs) than the calculated flow rates for the upstream basin. As field observations indicate no evidence of roadway overtopping in this area, it is assumed that the existing roadside ditch along the north side of Rio Lane acts as emergency overflow bypass for flows not captured by the existing culvert. Bypass flows appear to continue on to the east before reaching an additional culvert across Rio Lane and discharging via historic drainage patterns to the south.

Basin OS6 covers the southern half of Rio Lane along the northern boundary of the Commons at Falcon Field site. Due to no curb and gutter along Rio Lane, flows from this basin discharge as overland flow directly into Basin E6 and are represented by **Design Point DPL** with runoff rates of $Q_5=2.6$ cfs and $Q_{100}=5.5$ cfs.

Basin E6 represents the eastern most basin of the site. At 10.37 acres, the basin directs flows from its northwestern corner, and from Basins OS5, and OS6, southeast until they reach the existing **Design Point M** where they exit the site as overland flow at rates of $Q_5=7.4$ cfs and $Q_{100}=30.7$ cfs.

7.0 DEVELOPED CONDITION

For the purposes of site specific analysis, the project site has been divided into several grouped drainage basins as shown on the proposed drainage plan.

The Rational Method was used to determine runoff quantities for the 5- and 100-year storm recurrence intervals. Mile High Flood District MHFD-Detention v,4.04 was used for preliminary pond sizing, see appendix for calculations and below for a summary runoff table.

A site investigation is currently underway to evaluate existing groundwater conditions. In order to mitigate potential issues, the site grading in several areas of the site will be raised from the existing condition and as such, will increase the separation above shallow water areas. The results of the groundwater monitoring will indicate whether further mitigation measures will be required on the site, particularly at the detention basins. This analysis will be completed at the final plat stage with the construction documents.

The existing channel through the site is proposed to be piped via 10'x4' box culvert from the existing outfall south of U.S. Highway 24, through the site before discharging into a redefined open channel to the south of the proposed Retail Row St. A CLOMR study is currently underway to determine the feasibility of this approach.

Any underdrain system to be installed will be the responsibility of the Falcon Field District. State and Groundwater District permitting for discharges will be the responsibility of the of the District.

<u>A-group basins</u> represent flows at the eastern residential portion of the site that will be intercepted by Pond A, ultimately discharging out to the redefined tributary open channel.

BASIN & DESIGN POINT SUMMARY								
BASIN	DP	AREA (AC)	Q5	Q100				
A-BASINS								
OSA		16.62	10.7	38.8				
A1	1	0.74	3.3	6.0				
A2		1.52	2.9	7.4				
	2	2.27	6.2	13.2				
A3	3	1.48	3.0	7.0				
A4	4	2.87	6.0	13.7				
A5		1.47	3.7	7.8				
	5	4.34	8.8	19.5				
A6	6	3.30	5.4	11.8				
	6A	7.64	12.6	27.8				
A7	7	1.76	3.0	6.6				
A8	8	0.65	1.4	3.0				
A9		2.56	5.9	12.7				
	9	4.97	8.7	18.9				
A10		1.10	2.0	4.5				
	10	2.57	4.7	10.6				
	10A	15.18	24.5	54.0				
A11		1.07	0.3	2.2				
	11	18.51	39.2	88.2				
A12		1.32	0.5	12.5				
	12	17.94	9.3	34.5				
A13	13	1.20	0.5	3.6				
RET090 (DBPS)			36.0	320.0				
A14		0.61	0.2	1.6				
POND A OUTFALL			0.5	12.7				
	14		37.2	344.1				

Rational Method Runoff Summary (A-group)

Basin OSA is an offsite basin north of Rio Lane. This basin is as described in the existing condition as Existing Basin OS5.

Basin A1 is located on the western side of Rio Lane. Runoff will flow south via curb and gutter at rates of $Q_5=3.3$ cfs and $Q_{100}=6.0$ cfs towards **Design Point DP1**. At DP1, flows will

be captured by a proposed public sump curb inlet located at the southwestern most point of Rio Lane.

Basin A2 covers the eastern side of Rio Lane and a portion of the rear of the lots along Jacamar Place. Flows of $Q_5=2.9$ cfs and $Q_{100}=7.4$ cfs will travel south overland and via curb and gutter towards the knuckle with Retail Row St. and **Design Point DP2**.

DP2 is a proposed public sump curb inlet that is located at the very southeastern point of Rio Lane. The inlet will capture all of the runoff generated within basin A2, before combining that with the runoff captured by DP1. Together this runoff, at rates of $Q_5=6.2$ cfs and $Q_{100}=13.2$ cfs, will discharge into the proposed full-spectrum detention facility **Pond A**.

Basin A3 is located between Rio Lane to the west and Jacamar Place to the east. Runoff flows overland and via curb and gutter from the northwest corner of the basin, down Jacamar Place, to the southeast corner at **DP3** with runoff rates of Q_5 =3.0 cfs and Q_{100} =7.0 cfs. From this point flows will continue to the east via curb and gutter flow to **DP10**.

As described in the existing conditions section of this report, an existing 18" CMP culvert currently discharges onto the project site. In the developed condition, it is proposed that this culvert flow be directed to the east via 18" RCP storm sewer extension, under the proposed Tody Way intersection with Rio Lane. The roadside ditch east of the proposed Tody Way and Rio Lane intersection is to be redefined with outfall protection to protect from downstream erosion and scour. Required drainage easements will be established at the final plat stage, however an existing 10' drainage and utility easement exists along the rear of the adjacent Falcon Estates subdivision to the east, and an existing 20' drainage and utility easement exists along the rear of the south.

Basin A4 covers the south side of Rio Lane, which section with curb and gutter and sidewalk on the s north side of Sapoya Place. Runoff (Q_5 =4.0 cfs and sidewalk of the ease property line.

way 1 the st to

southeast as side lot flow and curb and gutter flow towards the intersection with Tody Way and **Design Point DP4.**

Basin A5 covers 1.47-acres of lots along the west side of Tody Way and the north side of Buteos Lane. Flows generated by this basin ($Q_5=3.7$ cfs and $Q_{100}=7.8$ cfs) are directed towards the south and west of the basin via side-lot swale and curb and gutter towards a proposed public at-grade storm inlet at **Design Point DP5**. Captured flows will continue to the south via proposed public storm sewer, bypass flows will continue west along Buteos Lane towards a low point at Design Point 9.

Basin A6 covers 3.3-acres of lots along the east side of Tody Way and the south side of Buteos Lane. Flows generated by this basin ($Q_5=5.4$ cfs and $Q_{100}=11.6$ cfs) are directed towards the south and west of the basin via side-lot swale and curb and gutter towards a proposed public at-grade storm inlet at **Design Point DP6**. Captured flows will continue to the northwest via proposed public storm sewer, bypass flows will continue west along Buteos Lane towards a low point at Design Point 9.

Design Point 6A is located at a proposed public storm manhole and represents the combining of flows from DP5 and DP6. Flows continue to the west from this design point via proposed public storm sewer.

Basin A7 covers 1.76-acres of lots along the east side of Motmot Way. Flows generated by this basin (Q_5 =3.0 cfs and Q_{100} =6.6 cfs) are directed towards the south of the basin via side-lot swale and curb and gutter towards **Design Point DP7** at the intersection with Buteos Lane. Flows will continue to the west as curb and gutter flow.

Basin A8 covers the front of a portion of residential lots along the east side of Jacamar Place. Flows from this basin ($Q_5=1.4$ cfs and $Q_{100}=3.0$ cfs) are directed south via curb and gutter towards **Design Point DP8.** From this point flows will continue to the east via curb and gutter flow.

Basin A9 covers the central portion of residential lots along Motmot Way and generates flows of $Q_5=5.9$ cfs and $Q_{100}=12.7$ cfs. Flows will generally travel as side-lot swale and curb and gutter flow to the east and south towards **Design Point DP9**.

DP9 covers flow from DP8, Basin A9 and bypass flows from DP7. Flows at this design point are captured by a proposed public sump curb inlet and will be discharged to the south via public storm system. Emergency flow path for this inlet will be contained within the street section, or discharge to the south via side lot swale between Lots 41 and 42.

Basin A10 covers 1.10 acres of residential lots along Buteos Lane. Flows from this basin will be directed via side lot swales and curb and gutter at rates of $Q_5=2.0$ cfs and $Q_{100}=4.5$ cfs, towards a proposed public at-grade curb inlet at **Design Point DP10.** Flows captured by this inlet will discharge to the north via proposed public storm sewer. Emergency flow path for this inlet will be contained within the street section, or discharge to the south via side lot swale between Lots 41 and 42.

Design Point 10A represents the combining of flows from DP9 and DP10 at a proposed storm sewer manhole. Piped flows reaching this point will continue to the west via proposed storm sewer.

Basin A11 covers the area of the proposed full-spectrum detention facility **Pond A**. Flows generated by this basin ($Q_5=0.3$ cfs and $Q_{100}=2.2$ cfs) will be captured by the pond in their entirety.

Design Point DP11 represents all flows reaching the full-spectrum detention facility (Basins A1-A14). Pond A will discharge at historic rates into the redefined open channel. See further detention facility discussion below.

Basin A12 covers a portion of Tract A along the eastern boundary. Flows generated by this 1.32-acre basin combine with redirected flows from offsite basin OSA and are proposed to be channelized along the eastern boundary via grass lined swale, before discharging via level spreader as offsite overland sheet flow at **Design Point DP12**. Basin A12 will be regraded but will remain undeveloped as an open space tract. It is anticipated that this area will fall under ECM 1.7.1.C.1. as the ability to capture and treat flows generated by Basin A12 is restricted due to grading constraints. Any area outside of

the criteria exclusion limit will be considered for runoff reduction. This will be further analyzed at the final drainage report stage.

Basin A13 covers a portion of Tract A along the southern boundary. Flows generated by this 1.20-acre basin are directed offsite as overland sheet flow. This basin will be regraded but will remain undeveloped as an open space tract. It is anticipated that this area will fall under ECM 1.7.1.C.1. as the ability to capture and treat flows generated by Basin A13 is restricted due to grading constraints. Any area outside of the criteria exclusion limit will be considered for runoff reduction. This will be further analyzed at the final drainage report stage.

Basin A14 is 0.61-acres located between the 2 northern proposed full-spectrum detention facilities, **Pond A and B**. This basin will generate runoff at rates of $Q_5=0.2$ cfs and $Q_{100}=1.6$ cfs. These rates will combine with those discharged via the proposed box culvert, and the two detention ponds before discharging from the site at Design Point 14 at rates of $Q_5=37.2$ cfs and $Q_{100}=344.1$ cfs

<u>B-group basins</u> represent the central commercial portion of the site that will be intercepted by Pond B, ultimately discharging out to the redefined tributary open channel.

Basin OSB1-OSB3 represent the south side of US-HWY 24, along the northern boundary of the site. The ultimate design for US HWY 24 is currently underway and as such, the final layout and drainage design is not known at this time. Conservatively, these offsite basins consider the south side of the highway draining on to the property as it does in the current existing condition.

Basin B1 is 1.99 acres at the northeast corner of the commercial area. Flows from this basin are intended to be captured and routed to a proposed storm sewer stub at the southwest corner. During the overlot grading phase, temporary diversion swales will be utilized to direct the basin towards the associated storm sewer stub at **Design Point 1**. Flows from this basin combine with those from Basin OSB1 before reaching this proposed private storm sewer at Design Point 1 at rates of $Q_5=11.6$ cfs and $Q_{100}=21.1$ cfs. Flows from this stub will travel to the southwest via proposed private storm sewer.

Basin B2 is located along the northern boundary of the commercial area. Flows of $Q_5=4.7$ cfs and $Q_{100}=8.5$ cfs are generated by this basin, combine with those from offsite basin OSB2 and are intended be captured and routed to a proposed storm sewer stub at the southwest corner at **Design Point 2** and routed to the southeast via private storm sewer. During the overlot grading phase, temporary diversion swales will be utilized to direct the basin towards the associated storm sewer stub.

The intent of the proposed storm sewer stubs at each of the commercial lots is to provide for a connection point to the storm sewer system, once development of the specific lot occurs.

Basin B3 covers a portion of the proposed Woodmen road right-of-way at the center of the commercial area. Flows of $Q_5=1.6$ cfs and $Q_{100}=2.9$ cfs are generated by this basin, and travel via curb and gutter to the south towards a proposed at-grade curb inlet at

Design Point 3. Captured flows continue to the east via proposed storm sewer. Bypass flows will continue to the south as curb and gutter flow towards DP9.

Basin B4 is located along the northern boundary of the commercial area, to the southwest of Basin B2. Flows of $Q_5=6.4$ cfs and $Q_{100}=11.7$ cfs are generated by this basin, combine with those from offsite basin OSB3 and travel overland to the southeast towards **Design Point 4** and a proposed storm sewer stub. As with the previous commercial lot basins, the intention is to provide a storm sewer stub for the future lot developer to connect to, during the overlot grading phase, temporary diversion swales will be utilized to direct the basin towards the associated storm sewer stub.

BASIN & DESIGN POINT SUMMARY								
BASIN	DP	AREA (AC)	Q5	Q100				
B-BASINS								
OSB1		0.83	3.8	6.8				
OSB2		0.32	1.5	2.7				
OSB3		0.56	2.6	4.7				
B1		1.99	8.3	15.2				
	1	2.82	11.6	21.1				
B2		1.11	4.7	8.5				
	2	1.44	6.0	10.9				
B3	3	0.35	1.6	2.9				
B4		1.53	6.4	11.7				
	4	2.09	8.6	15.6				
	4A	2.44	10.2	18.4				
	4B	6.70	27.1	49.2				
B5	5	0.25	1.2	2.1				
B6		0.37	1.7	3.1				
	6	0.62	2.9	5.2				
B7		1.97	8.2	15.0				
	7	9.29	38.8	70.4				
B8	8	1.52	6.4	11.6				
B9		0.89	4.1	7.4				
	9	2.41	10.5	19.0				
B10		0.71	3.3	5.9				
	10	3.12	13.7	24.7				
	10A	12.41	51.6	93.5				
B11		1.14	0.5	3.5				
	11	13.55	51.6	95.9				
POND B OUTFALL			0.5	9.8				

Rational Method Runoff Summary (B-group)

Design Point 4A represents the combining of flows from DP3 and DP4 at a proposed storm sewer manhole. Flows reaching this Design Point will continue to the east via proposed storm sewer.

Design Point 4B represents the combining of flows from DP1A, DP2, and DP4A at a proposed storm sewer manhole. Flows reaching this Design Point will continue to the south via proposed storm sewer.

Basin B5 covers a portion of the proposed Perula Pt and Jackdaw Pt at the center of the commercial area. Flows of $Q_5=1.2$ cfs and $Q_{100}=2.1$ cfs are generated by this basin, and travel via curb and gutter to the south towards a proposed sump curb inlet at **Design Point 5.** Captured flows continue to the west via proposed storm sewer.

Basin B6 covers a portion of the proposed Perula Pt and Jackdaw Pt at the center of the commercial area. Flows of $Q_5=1.7$ cfs and $Q_{100}=3.1$ cfs are generated by this basin, and travel via curb and gutter to the south towards a proposed sump curb inlet at **Design Point 6.** Captured flows combine with those from Design Point 5 and continue to the west via proposed storm sewer.

Basin B7 is located in the central portion of the commercial area. Flows of Q_5 =8.2 cfs and Q_{100} =15.0 cfs are generated by this basin. As with the previous commercial lot basins, the intention is to provide a storm sewer stub, located at the southeast corner for the future lot developer to connect to. During the overlot grading phase, temporary diversion swales will be utilized to direct the basin towards the associated storm sewer stub.

Design Point 7 represents the combining of flows from DP4B and DP7 and Basin B7 at a proposed storm sewer manhole. Flows reaching this Design Point will continue to the south via proposed storm sewer.

Basin B8 covers 1.52-acres in the central portion of the commercial area. Flows of $Q_5=6.4$ cfs and $Q_{100}=11.6$ cfs are generated by this basin. As with the previous commercial lot basins, the intention is to provide a storm sewer stub, located at the southeast corner at **Design Point 6** for the future lot developer to connect to with temporary diversion swales installed at the overlot grading stage. Piped flows will discharge to the south via proposed storm sewer.

Basin B9 covers a portion of Woodmen Road and Retail Row St. right-of-way at the center of the commercial area. Flows of $Q_5=4.1$ cfs and $Q_{100}=7.4$ cfs are generated by this basin, and travel via curb and gutter to the south and northeast towards a proposed low point and public sump curb inlet at **Design Point DP9**. Captured flows at this inlet combine with those from DP8 and continue to the south via proposed storm sewer.

Basin B10 covers the southern portion of Retail Row St. right-of-way at the center of the commercial area, to the south of Basin B9. Flows of $Q_5=3.3$ cfs and $Q_{100}=5.9$ cfs are generated by this basin, and travel via curb and gutter to the northeast towards a proposed low point and public sump curb inlet. At **Design Point DP10**, flows captured by this inlet combine with the piped flows from DP9 and continue to the south and west via proposed storm sewer.

Design Point 10A represents the combining of piped flows from DP7 and DP10 at a proposed storm sewer manhole. Flows reaching this Design Point will continue to the south via proposed storm sewer towards the full-spectrum detention facility **Pond B**.

Basin B11 covers the area of the proposed full-spectrum detention facility Pond B. Flows generated by this basin ($Q_5=0.5$ cfs and $Q_{100}=3.5$ cfs) will be captured by the pond in their entirety.

Design Point DP11 represents all flows reaching the full-spectrum detention facility (Basins OSB1-OSB3 & B1-B11). Pond B will discharge at historic rates into the redefined open channel. See further detention facility discussion below.

<u>C-group basins</u> represent the western commercial portion of the site that will be intercepted by Pond C, ultimately discharging out to follow historic conditions to the south.

Basin OSC1 represents 0.37-acres of US-HWY 24, which acts as the northwestern boundary for the site. The runoff generated by this basin, $Q_5=1.7$ cfs and $Q_{100}=3.1$ cfs, is directed northeast via proposed curb and gutter. As with the US HWY 24 offsite basins described in the B-basins section of this report, coordination with CDOT is ongoing and final layout and drainage design will be confirmed at final plat stage for this area.

Basin C1 covers a portion of Woodmen Road right-of-way at the center of the commercial area, adjacent to Basin B3. Flows of $Q_5=1.2$ cfs and $Q_{100}=2.1$ cfs are generated by this basin, and travel via curb and gutter to the south towards a proposed at-grade public curb inlet at **Design Point DP1**.

DP1 combines flows from DPC1 and Basin C1 at a proposed at-grade curb inlet. Captured flows will continue to the west via proposed private storm sewer. Bypass flows will continue to the south via curb and gutter.

Basin C2 covers 2.26-acres in the west-central portion of the commercial area. Flows of $Q_5=9.4$ cfs and $Q_{100}=17.2$ cfs are generated by this basin and are intended be captured and routed to a proposed storm sewer stub at the southwest corner at Design Point DP2. As with the previous commercial lot basins, the intention is to provide a storm sewer stub, located at the southeast corner for the future lot developer to connect to. During the overlot grading phase, temporary diversion swales will be utilized to direct the basin towards the associated storm sewer stub.

Design Point DP2 is located at a proposed private storm manhole and combines flows from DP1 and Basin C2 and continues on to the west via proposed private storm sewer.

Basin C3 covers 1.15-acres in the commercial area. Runoff rates of Q_5 =4.8 cfs and Q_{100} =8.8 cfs are generated by this basin and as with other commercial basins, are intended be captured and routed to a proposed storm sewer stub at the southwest corner at Design Point DP3. As with the previous commercial lot basins, the intention is to provide a storm sewer stub, located at the southeast corner for the future lot developer to connect to. During the overlot grading phase, temporary diversion swales will be utilized to direct the basin towards the associated storm sewer stub.

BASIN & DESIGN POINT SUMMARY								
BASIN	DP	AREA (AC)	Q5	Q100				
C-BASINS								
OSC1	1.7	3.1						
C1		0.25	1.2	2.1				
	1	0.62	2.8	5.0				
C2		2.26	9.4	17.2				
	2	2.88	11.6	21.0				
C3	3	1.15	4.8	8.8				
OSC2		1.36	2.2	6.0				
C4		1.41	5.9	10.8				
	4	2.78	7.6	15.8				
C5		0.17	0.8	1.5				
	5	1.32	5.6	10.2				
C6		0.18	0.8	1.5				
	6	1.50	6.4	11.6				
	6A	7.16	24.5	34.1				
C7	7	0.88	4.1	7.4				
C8	8	0.65	3.0	5.4				
	8A	8.69	30.1	44.4				

Rational Method Runoff Summary (C-group)

Basin OSC2 covers an offsite area along the western boundary of the project site, and includes a portion of U.S. Highway 24. The 1.36-acre offsite basin, will sheet flow into basin C4 at rates of $Q_5=2.2$ cfs and $Q_{100}=6.0$ cfs.

Basin C4 is located along the western boundary of the commercial area. Runoff rates of $Q_5=5.9$ cfs and $Q_{100}=10.8$ cfs are generated by this basin as with other commercial basins, are intended be captured and routed to a proposed storm sewer stub at the southwest corner at Design Point DP4. As with the previous commercial lot basins, the intention is to provide a storm sewer stub, located at the southeast corner for the future lot developer to connect to. During the overlot grading phase, temporary diversion swales will be utilized to direct the basin towards the associated storm sewer stub.

DP4 represents the combining of flows from OSC2 and Basin C4 at a proposed private storm sewer stub. Flows reaching this Design Point will continue to the east via proposed private storm sewer.

Basin C5 covers a portion of the proposed Dunlin Heights at the center of the commercial area. Flows of $Q_5=0.8$ cfs and $Q_{100}=1.5$ cfs are generated by this basin, and travel via curb and gutter to the south towards a proposed sump curb inlet at **Design Point 5.** Captured flows combine with those from Design Point 3 and continue to the west via proposed storm sewer.

Basin C6 covers a portion of the proposed Dunlin Heights at the center of the

commercial area. Flows of $Q_5=0.8$ cfs and $Q_{100}=1.5$ cfs are generated by this basin, and travel via curb and gutter to the south towards a proposed sump curb inlet at **Design Point 6.**

DP6A represents the combining of flows from DP2, DP4 and DP6 at a proposed private storm sewer manhole. Flows reaching this Design Point will continue to the south via proposed private storm sewer.

Basin C7 covers a portion of Woodmen Road and Retail Row St. right-of-way to the west and south of the commercial area. Flows of $Q_5=4.1$ cfs and $Q_{100}=7.4$ cfs are generated by this basin, and travel via curb and gutter to the south and west towards a proposed lot point and public sump inlet at **Design Point DP7.** From this point flows will continue to the south via proposed storm sewer.

Basin C8 covers a portion of Retail Row St. right-of-way to the south of the commercial area. Flows of $Q_5=3.0$ cfs and $Q_{100}=5.4$ cfs are generated by this basin, and travel via curb and gutter to the southwest towards a proposed low point and public sump curb inlet at **Design Point DP8**. Flows captured by this inlet continue to the north via proposed storm sewer.

Design Point 8A represents the combining of flows from DP6A, DP7 and DP8 at a proposed storm sewer manhole. Piped flows reaching this Design Point will continue to the south via proposed storm sewer into the D-group basins.

D-group basins represent the southern residential portion of the site that will be intercepted by Pond C, ultimately discharging out to follow historic conditions to the southeast.

Basin D1 is located to the north of this residential portion of the development. Flows generated by this basin ($Q_5=2.0$ cfs and $Q_{100}=4.9$ cfs) travel to the southeast via side lot swale and curb and gutter towards **Design Point DP1**.

Basin D2 is located at the northwest corner of this residential portion of the development along Dovekie Drive. Flows generated by this basin ($Q_5=2.9$ cfs and $Q_{100}=7.1$ cfs) travel to the east and south via curb and gutter eventually reaching **Design Point DP2**.

DP2 combines flows from Basins D1 and D2, to be captured by a proposed public sump curb inlet at the intersection of Dovekie Drive and Becard Road. Captured flows will continue to the east via public storm sewer.

Basin D3 is located centrally within this residential portion of the development and covers the front of lots along the south side of Dovekie Drive. Flows generated by this basin $(Q_5=1.4 \text{ cfs} \text{ and } Q_{100}=3.3 \text{ cfs})$ travel to the northwest via side lot swale and curb and gutter towards a low point and proposed sump curb inlet at **Design Point DP3**. Flows from this point continue to the west via proposed storm sewer.

Design Point 3A represents the combining of flows from DP6A(C-Basins), DP2 and DP3 at a proposed storm sewer manhole. Flows reaching this Design Point will continue to the south via proposed storm sewer.

BASIN & DESIGN POINT SUMMARY								
BASIN	DP	AREA (AC)	Q5	Q100				
D-BASINS								
D1	1	1.36	2.0	4.9				
D2		1.95	2.9	7.1				
	2	3.30	4.7	11.6				
D3	3	0.91	1.4	3.3				
	3A	12.90	31.5	52.2				
D4	4	2.75	4.3	10.3				
D5		0.62	1.6	3.3				
	5	3.37	5.6	13.1				
D6	6	2.68	4.7	10.3				
D7		0.74	1.9	4.1				
	7	6.79	11.5	25.9				
D8	8	0.44	0.8	1.8				
D9	9	0.31	0.5	1.2				
D10	10	1.34	1.8	4.6				
D11		0.61	2.9	5.1				
	11	1.95	3.9	8.4				
D12		1.51	0.6	4.3				
	12	23.91	47.4	90.4				
OSD1	D1	2.70	0.9	6.7				
D13		1.98	0.7	5.0				
	13	4.68	1.6	11.4				
D14	0	0.76	0.3	2.1				
POND C OUTFALL			0.7	21.1				
	14		1.0	23.2				

Rational Method Runoff Summary (D-group)

Basin D4 is located centrally within this residential portion of the development. Flows generated by this basin (Q_5 =4.3 cfs and Q_{100} =10.3 cfs) travel to the south and east via side lot swale and curb and gutter towards **Design Point 4** at the intersection of Becard Road and Hoopoe Lane. Flows from this point continue to the south via cross-pan and curb and gutter flow.

Basin D5 is located centrally within this residential portion of the development, to the south of Basin D4 along Becard Road. Flows generated by this basin (Q_5 =1.6 cfs and Q_{100} =3.3 cfs) travel to the north and east via side lot swale and curb and gutter towards **Design Point DP5**, where flows combine with those from DP4 and continue to the south.

Basin D6 is 2.87 acres along Hoopoe Lane at the eastern boundary. Flows of Q_5 =4.7 cfs and Q_{100} =10.3 cfs travel to the west and south as curb and gutter flow towards a low point and proposed sump curb inlet at **Design Point DP7**.

Basin D7 covers the front of a portion of residential lots at the south of this residential area along Hoopoe Lane. Flows of $Q_5=1.9$ cfs and $Q_{100}=4.1$ cfs travel to the east and south as curb and gutter flow, combining with street flows from DP5 and DP6 towards a proposed sump curb inlet at **Design Point DP7**. Captured flows continue via proposed storm sewer to the west.

Basin D8 covers the rear of a portion of residential lots directly south of Basin D5. Flows of $Q_5=0.8$ cfs and $Q_{100}=1.8$ cfs travel to the east and south towards **Design Point 8** and the adjacent detention facility. Final grading within this basin will be established at the final drainage report stage to ensure all flows generated by this basin are directed to the detention facility.

Basin D9 covers the rear of a portion of residential lots directly west of Basin D7. Flows of $Q_5=0.5$ cfs and $Q_{100}=1.2$ cfs travel to the west and south towards **Design Point DP9** and the adjacent detention facility. Final grading within this basin will be established at the final drainage report stage to ensure all flows generated by this basin are directed to the detention facility.

Basin D10 covers the southern portion along Dovekie Drive at the western boundary. Flows of $Q_5=1.8$ cfs and $Q_{100}=4.6$ cfs generated by this basin will be directed east via side lot swale before traveling south via curb and gutter towards a low point and proposed inlet structure at **Design Point DP11**.

Basin D11 covers the southern portion of Dovekie Drive adjacent to Basin D10. Flows of $Q_5=2.9$ cfs and $Q_{100}=5.1$ cfs generated by this basin will combine with those from Basin D10 and travel south via curb and gutter towards a low point and proposed inlet structure at **Design Point DP11**. Captured flows will discharge directly into the proposed detention facility.

Basin D12 covers the area of the proposed full-spectrum detention facility **Pond C**. Flows generated by this basin ($Q_5=0.6$ cfs and $Q_{100}=4.3$ cfs) will be captured by the pond in their entirety.

Design Point D12 represents all flows reaching the full-spectrum detention facility (Basins OSC1-OSC2, C1-C8 & D1-D12). **Pond C** will discharge at historic rates to the south to follow historic drainage patterns. See further detention facility discussion below.

Basin OSD1 is located along the eastern side of the upper half of Basin D13. This basin consists almost entirely of native grasses and vegetation, aside from a single small shed. The flows within this basin will flow to the southwest where they will naturally gather and channel along the westerly edge of Basin D13 towards **Design Point DPD1**. The runoff rates entering Basin D13 at DPD1 are $Q_5=0.9$ cfs and $Q_{100}=6.7$ cfs. Required drainage easements will be established at the final plat stage, however an existing 20' drainage and utility easement exists along the rear of the adjacent Arrowhead Estates subdivision to the south.

Basin D13 covers Tract G along the eastern boundary of this residential area. Flows generated by this 1.98-acre basin are proposed to be channelized along the eastern

boundary via grass lined swale, before discharging via level spreader as offsite overland sheet flow at **Design Point DP13**. This basin will be regraded but will remain undeveloped as an open space tract. It is anticipated that this area will fall under ECM 1.7.1.C.1. as the ability to capture and treat flows generated by Basin D13 is restricted due to grading constraints. Any area outside of the criteria exclusion limit will be considered for runoff reduction. This will be further analyzed at the final drainage report stage.

Basin D14 covers a section of open space area along the southern boundary of this residential area. While this area will be regraded, the area will remain undeveloped. Flows generated by this 0.76-acre basin combine with the outfall from Pond C at **Design Point 14** before discharging via level spreader as offsite overland sheet flow to the south. It is anticipated that this area will fall under ECM 1.7.1.C.1. as the ability to capture and treat flows generated by Basin D14 is restricted due to grading constraints. Any area outside of the criteria exclusion limit will be considered for runoff reduction. This will be further analyzed at the final drainage report stage.

Existing vs. Developed Flow Comparison

		Developed			Existing		
]	Q100	Q 5	DP	Q100	Q 5	DP
		344.1	37.2	DPA14	346.4	41.0	DPB
Please		11.4	1.6	DPD13	23.9	3.8	DPE
address		23.2 💦	1.0	DPD14	19.6	2.7	DPF
increase				None	6.1	1.5	DPH
flows at		3.6	0.5	DPA13	11.7	2.2	DPI
these design		34.5	9.3	DPA12	30.7	7.4	DPM
points ar		416.8	49.6		438.5	58.7	Total

۱e

will be

mitigated.

The developed outfall locations differ slightly from the existing conditions, but generally follow the historic flow path at or below historic rates as outlined below.

8.0 PROPOSED FULL-SPECTRUM DETENTION FACILITIES

As previously mentioned, three separate full-spectrum Extended Detention Basin facilities are proposed with this development. Further detailed design of these detention facilities will be coordinated with the CLOMR study and addressed at the Final Drainage Report stage.

<u>Pond A</u>, a private 1.91 ac-ft full-spectrum Extended Detention Basin is proposed in the southwestern corner of the A-basin neighborhood, to intercept and treat flows from the neighborhood area and discharge at historic rates into the adjacent redefined East Tributary. In accordance with El Paso County criteria, an outlet structure with a permanent micropool will release flows at or slightly below historic rates. An emergency spillway will be located on the western side of the pond, so in the case of an overflow, the runoff will be deposited between Pond's A and B. Pond design will be finalized with the final drainage report.

<u>Pond B</u>, is a proposed private 2.25 ac-ft full-spectrum Extended Detention Basin, designed to intercept the flows generated by the B-basin commercial region of the site, treat and discharge at historic rates into the adjacent redefined East Tributary. As with Pond A, in accordance with El Paso County criteria, an outlet structure with permanent micropool will release flows at or slightly below historic rates. An emergency spillway will be located on the eastern side of the pond, so in the case of an overflow, the runoff will be deposited between Pond's A and B. Pond design will be finalized with the final drainage report.

<u>Pond C</u>, is a proposed private 2.81 ac-ft full-spectrum Extended Detention Basin intended to intercept the flows generated by both the C and D-basin areas of the site. As with both other ponds, in accordance with El Paso County criteria, an outlet structure with permanent micropool will release flows at or slightly below historic rates. An emergency spillway will be located on the southern side of the pond, so in the case of an overflow, the runoff will be deposited to a similar location as the proposed outlet location. Pond design will be finalized with the final drainage report. The concentrated piped outflow from the detention facility will discharge onto a proposed grassed berm level spreader prior to discharge on to the adjacent properties to the south. The intention of this level spreader is to provide for stabilized conveyance at the historic level.

Maintenance access will be provided to each of the ponds. Private maintenance agreements and O&M manuals will be established for all 3 ponds prior to Final Plat.

9.0 FOUR-STEP PROCESS

- 1. Employ Runoff Reduction Practices: Proposed impervious areas on this site (roofs, asphalt/sidewalk) will be captured by onsite roadways and storm sewer systems as much as possible to slow runoff and increase time of concentration prior to being conveyed to the proposed detention ponds. This will minimize directly connected impervious areas within the project site.
- 2. Implement CM's that provide a Water Quality Capture Volume with slow release: The majority of runoff generated by this project will be treated through capture and slow release of the WQCV in one of 3 permanent full spectrum extended detention facility designed per current drainage criteria. The areas tributary to each of the detention facilities is described above.
- **3. Stabilize Drainage Ways:** Stabilization of the existing drainageway through the site will occur via installation of a proposed 10'x4' concrete box culvert and a small section of open channel as the drainageway exits the property. Downstream hydraulic analysis will be completed at the final plat stage.
- 4. Implement Site Specific and Other Source Control CM's: Standard residential and commercial source control will be utilized in order to minimize potential pollutants entering the storm system. Example source control measures consist of: indoor storage of household chemicals; and trash receptacles in common areas.

10.0 CONDITIONAL LETTER OF MAP REVISION (CLOMR)

A Conditional Letter of Map Revision (CLOMR) is currently in the design stage for the Falcon Creek East Tributary reach that bisects the site. Excerpts from the CLOMR report are included in the appendix, and a copy of the full report has been submitted as part of this Preliminary Plan application.

11.0 DOWNSTREAM ANALYSIS

As mentioned earlier in this report and at the request of El Paso County, a hydraulic analysis of the downstream drainageway from The Commons at Falcon Field property to Falcon Highway to the south, will be provided with the final drainage report. Analysis and possible improvements to the downstream drainageway may necessitate the need to amend the preliminary plan in order to meet criteria.

Under existing conditions, the UTBSC discharges to an open channel through the site from 2-12"x4.83' box culverts under Highway 24. The Falcon Field property limits are approximately 46 feet downstream of the Highway 24 box culvert exit. There is an 8-foot concrete vertical wall/drop immediately downstream of the culvert, then a short riprap channel section, before the open channel returns to a vegetated section through the site. There have been a number of revisions to the upstream tributary over the years, particularly as a result of the railroad and highway, and with ongoing land development in the Falcon area. As a result of the upstream modifications, the drainageway has incised its way through the Falcon Field property and significant sediment deposits have resulted in the damage and subsequent closure of Pinto Pony Road downstream. However, the improvements proposed by this Commons at Falcon Field project will work to mitigate this issue by detaining at historic flows and treating for water quality before discharge downstream.

12.0 DRAINAGE/BRIDGE FEES

Design, phasing, responsibility for and maintenance of any proposed improvements will be discussed in the final drainage report(s) as development of the site proceeds. Fees will be assessed and paid according to the current rates at the time of platting.

The Falcon DBPS – Fee Development categorizes improvements into Developer Costs, County Costs and Metro District Costs. Items identified as Developer Costs (those incurred by the Developer) are currently eligible for reimbursement. Reach RET100 is identified as a County cost, and as such the developer intends to amend the Falcon DBPS to allow for the costs of the 1,000-If of RET100 improvements to become reimbursable by the process outlined in County criteria.

13.0 CONCLUSIONS

The Commons at Falcon Field project has been designed in accordance with El Paso County criteria. The full-spectrum detention facilities have been designed to limit the release of storm runoff to historic flows. This development will not negatively impact the downstream facilities.

A small portion of the site will remain in the 100-year floodplain after grading is complete, and will be addressed further at the Final Drainage Report stage and by the CLOMR study currently underway. Upon completion, a LOMR will be submitted to FEMA after construction to revise the FIRM map. Future buildings will not be constructed in the floodplain.

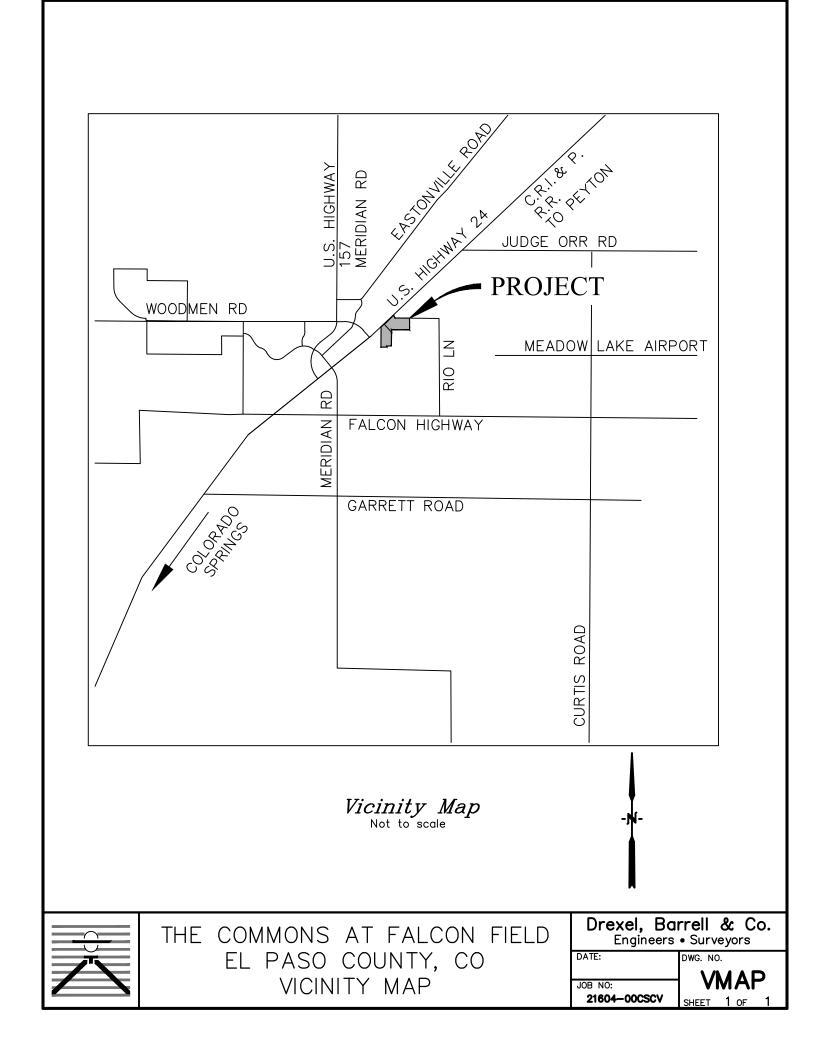
14.0 REFERENCES

The sources of information used in the development of this study are listed below:

- 1. City of Colorado Springs/El Paso County Drainage Criteria Manual, May 2014.
- 2. Urban Storm Drainage Criteria Manuals, Urban Drainage and Flood Control District. June 2001, Revised April 2008.
- 3. Natural Resources Conservation Service (NRCS) Web Soil Survey
- 4. Federal Emergency Management Agency, Flood Insurance Rate Map, El Paso County, Colorado and Unincorporated Areas, Map Numbers 8041C0553G & 8041C0561G, Effective Date December 7, 2018.
- 6. EL Paso County Board Resolution No 15-042: El Paso County adoption of Chapter 6 and Section 3.2.1, Chapter 13 of the City of Colorado Springs Drainage Criteria Manual, May 2014.
- 7. Falcon Drainage Basin Planning Study. Prepared by Matrix Design Group, September 2015.

Appendix

Vicinity Map



Soils Map

Custom Soil Resource Report Soil Map



	MAP L	EGEND		MAP INFORMATION
Area of Int	terest (AOI) Area of Interest (AOI)	8	Spoil Area Stony Spot	The soil surveys that comprise your AOI were mapped at 1:24,000.
Soils	Soil Map Unit Polygons	00 V	Very Stony Spot Wet Spot	Warning: Soil Map may not be valid at this scale.
ĩ	Soil Map Unit Lines Soil Map Unit Points	۵ •	Other Special Line Features	Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of
ల	Point Features Blowout Borrow Pit	Water Fea		contrasting soils that could have been shown at a more detailed scale.
×	Clay Spot	Transporta	ation Rails	Please rely on the bar scale on each map sheet for map measurements.
◇ ¥	Closed Depression Gravel Pit Gravelly Spot	~	Interstate Highways US Routes	Source of Map: Natural Resources Conservation Service Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)
 Ø	Landfill Lava Flow	~	Major Roads Local Roads	Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts
2 2 2	Marsh or swamp Mine or Quarry	Backgrou	na Aerial Photography	distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.
0	Miscellaneous Water Perennial Water			This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.
~ +	Rock Outcrop Saline Spot			Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 19, Aug 31, 2021
· ·: •	Sandy Spot Severely Eroded Spot			Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.
◇ ≫	Sinkhole Slide or Slip			Date(s) aerial images were photographed: Sep 11, 2018—Oct 20, 2018
ø	Sodic Spot			The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

		-	
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	18.8	32.8%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	38.6	67.2%
Totals for Area of Interest		57.4	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however,

onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

El Paso County Area, Colorado

8-Blakeland loamy sand, 1 to 9 percent slopes

Map Unit Setting

National map unit symbol: 369v Elevation: 4,600 to 5,800 feet Mean annual precipitation: 14 to 16 inches Mean annual air temperature: 46 to 48 degrees F Frost-free period: 125 to 145 days Farmland classification: Not prime farmland

Map Unit Composition

Blakeland and similar soils: 98 percent Minor components: 2 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Blakeland

Setting

Landform: Hills, flats Landform position (three-dimensional): Side slope, talf Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium derived from sedimentary rock and/or eolian deposits derived from sedimentary rock

Typical profile

A - 0 to 11 inches: loamy sand AC - 11 to 27 inches: loamy sand C - 27 to 60 inches: sand

Properties and qualities

Slope: 1 to 9 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat excessively drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 5 percent
Available water supply, 0 to 60 inches: Low (about 4.5 inches)

Interpretive groups

Land capability classification (irrigated): 3e Land capability classification (nonirrigated): 6e Hydrologic Soil Group: A Ecological site: R049XB210CO - Sandy Foothill Hydric soil rating: No

Minor Components

Other soils

Percent of map unit: 1 percent

Hydric soil rating: No

Pleasant

Percent of map unit: 1 percent Landform: Depressions Hydric soil rating: Yes

19—Columbine gravelly sandy loam, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 367p Elevation: 6,500 to 7,300 feet Mean annual precipitation: 14 to 16 inches Mean annual air temperature: 46 to 50 degrees F Frost-free period: 125 to 145 days Farmland classification: Not prime farmland

Map Unit Composition

Columbine and similar soils: 97 percent Minor components: 3 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Columbine

Setting

Landform: Flood plains, fan terraces, fans *Down-slope shape:* Linear *Across-slope shape:* Linear *Parent material:* Alluvium

Typical profile

A - 0 to 14 inches: gravelly sandy loam *C - 14 to 60 inches:* very gravelly loamy sand

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Very low (about 2.5 inches)

Interpretive groups

Land capability classification (irrigated): 4e Land capability classification (nonirrigated): 6e Hydrologic Soil Group: A Ecological site: R049XY214CO - Gravelly Foothill Hydric soil rating: No

Minor Components

Fluvaquentic haplaquolls

Percent of map unit: 1 percent Landform: Swales Hydric soil rating: Yes

Other soils

Percent of map unit: 1 percent *Hydric soil rating:* No

Pleasant

Percent of map unit: 1 percent Landform: Depressions Hydric soil rating: Yes Floodplain Map

National Flood Hazard Layer FIRMette

104°36'16"W 38°56'26"N

T13S R64W S007

250

500

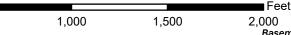
T13S R64W S006



Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT Without Base Flood Elevation (BFE) Zone A. V. A9 With BFE or Depth Zone AE, AO, AH, VE, AR SPECIAL FLOOD HAZARD AREAS **Regulatory Floodway** 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X STRUCTURE STRU Future Conditions 1% Annual Chance Flood Hazard Zone X Area with Reduced Flood Risk due to Levee. See Notes. Zone X OTHER AREAS OF FLOOD HAZARD Area with Flood Risk due to Levee Zone D 08041C0553G eff. 12/7/2018 NO SCREEN Area of Minimal Flood Hazard Zone X Effective LOMRs OTHER AREAS Area of Undetermined Flood Hazard Zone D - — – – Channel, Culvert, or Storm Sewer GENERAL Zone A STRUCTURES LIIII Levee, Dike, or Floodwall FLPASOCOUNTY 080059 20.2 Cross Sections with 1% Annual Chance 17.5 Water Surface Elevation AREA OF MINIMAL FLOOD NAZARD **Coastal Transect** Zone X Mase Flood Elevation Line (BFE) Limit of Study Jurisdiction Boundary **Coastal Transect Baseline** OTHER **Profile Baseline** FEATURES Hydrographic Feature **Digital Data Available** No Digital Data Available MAP PANELS Unmapped The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location. 08041C0561G This map complies with FEMA's standards for the use of eff. 12/7/2018 digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 4/12/2022 at 2:02 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time. This map image is void if the one or more of the following map Zone A

elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.



1:6.000

Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

104°35'38"W 38°55'58"N

Hydrology Calculations

PROJECT: PROJECT NO: DESIGN BY: REV. BY: AGENCY: REPORT TYPE: DATE: Commons at Falcon Field 21604-00 KGV TDM El Paso County Preliminary 7/5/2024



	C2*	C5*	C10*	C100*	% IMPERV
Pasture/Meadow		0.08		0.35	0
Roofs		0.73		0.81	90
Lawns		0.08		0.35	0
Streets: Paved		0.90		0.96	100
Streets: Gravel		0.59		0.70	80

EXISTING CONIDTION

SUB-BASIN	SURFACE DESIGNATION	AREA	COMPOSIT	% IMPERV		
		ACRE	C2			
OS1	Pasture/Meadow	0.67		0.08	0.35	0
	Roofs	0.00		0.73	0.81	90
	Lawns	0.00		0.08	0.35	0
	Streets: Paved	0.67		0.90	0.96	100
	Streets: Gravel	0.00		0.59	0.70	80
	WEIGHTED AVERAGE			0.49	0.66	50%
TOTAL OS1		1.34				
OS2	Pasture/Meadow	0.30		0.08	0.35	0
	Roofs	0.00		0.73	0.81	90
	Lawns	0.00		0.08	0.35	0
	Streets: Paved	0.30		0.90	0.96	100
	Streets: Gravel	0.00		0.59	0.70	80
	WEIGHTED AVERAGE			0.49	0.66	50%
TOTAL OS2		0.60				
OS3	Pasture/Meadow	2.56		0.08	0.35	0
000	Roofs	0.04		0.73	0.81	90
	Lawns	0.00		0.08	0.35	0
	Streets: Paved	0.00		0.90	0.96	100
	Streets: Gravel	0.00		0.59	0.70	80
	WEIGHTED AVERAGE			0.09	0.36	1%
TOTAL OS3		2.56				
OS4	Pasture/Meadow	1.15	-	0.08	0.35	0
	Roofs	0.10		0.73	0.81	90
	Lawns	0.00		0.08	0.35	0
	Streets: Paved	0.29		0.90	0.96	100
	Streets: Gravel	0.00		0.59	0.70	80
	WEIGHTED AVERAGE			0.28	0.50	25%
TOTAL OS4		1.54				
OS5	Pasture/Meadow	13.94		0.08	0.35	0
	Roofs	0.05		0.00	0.81	90
	Lawns	0.00		0.08	0.35	0
	Streets: Paved	2.25		0.90	0.96	100
	Streets: Gravel	0.39		0.59	0.70	80

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	C2*	C5*	C10*	C100*	% IMPERV
Pasture/Meadow		0.08		0.35	0
Roofs		0.73		0.81	90
Lawns		0.08		0.35	0
Streets: Paved		0.90		0.96	100
Streets: Gravel		0.59		0.70	80

	WEIGHTED AVERAGE	1 [0.20	0.44	16%
TOTAL OS5		16.62			
OS6	Pasture/Meadow	0.39	0.08	0.35	0
	Roofs	0.00	0.73	0.81	90
	Lawns	0.00	0.08	0.35	0
	Streets: Paved	0.52	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE	0.01	0.55	0.70	57%
TOTAL OS6		0.91			
E1	Pasture/Meadow	13.74	0.08	0.35	0
	Roofs	0.00	0.73	0.81	90
	Lawns	0.00	0.08	0.35	0
	Streets: Paved	0.00	0.90	0.96	100
	Streets: Gravel	0.11	0.59	0.70	80
	WEIGHTED AVERAGE		0.08	0.35	1%
TOTAL E1		13.85			
-0	Dest (Mass. Jac.	10.00	0.00	0.25	0
E2	Pasture/Meadow	12.88 0.00	0.08 0.73	0.35 0.81	90
	Roofs	0.00	0.73	0.81	90
	Lawns Streets: Paved	0.00	0.00	0.35	100
	Streets: Gravel	0.00	0.59	0.90	80
	WEIGHTED AVERAGE	0.00	0.08	0.70	0%
TOTAL E2		12.88	0.00	0.00	070
E3	Pasture/Meadow	13.11	0.08	0.35	0
	Roofs	0.00	0.73	0.81	90
	Lawns	0.00	0.08	0.35	0
	Streets: Paved	0.00	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.08	0.35	0%
TOTAL E3		13.11			
E4	Pasture/Meadow	1.57	0.08	0.35	0
	Roofs	0.00	0.73	0.81	90
	Lawns	0.00	0.08	0.35	0

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	C2*	C5*	C10*	C100*	% IMPERV
Pasture/Meadow		0.08		0.35	0
Roofs		0.73		0.81	90
Lawns		0.08		0.35	0
Streets: Paved		0.90		0.96	100
Streets: Gravel		0.59		0.70	80

E6	Pasture/Meadow Roofs	10.37 0.00	0.08	0.35	0 90
E6	Desture/Meedow	10.27	0.08	0.25	0
TOTAL E5		5.91			
	WEIGHTED AVERAGE		0.12	0.38	6%
	Streets: Gravel	0.17	0.59	0.70	80
	Streets: Paved	0.00	0.90	0.96	100
	Lawns	0.00	0.08	0.35	0
20	Roofs	0.25	0.73	0.81	90
E5	Pasture/Meadow	5.49	0.08	0.35	0
TOTAL E4		1.57			
	WEIGHTED AVERAGE		0.08	0.35	0%
	Streets: Gravel	0.00	0.59	0.70	80
	Streets: Paved	0.00	0.90	0.96	100

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RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

EXISTING TIME OF CONCENTRATION

	8	SUB-BASI	N				INITI	AL/OVERL	AND		TRAVEL	TIME		TIME OF CO	NCENTRATION	FINAL
		DATA						TIME (t _i)			(t _t)					t _c
BASIN	DESIGN PT:	C ₅	C ₁₀₀	AREA	COMP		LENGTH	SLOPE	ti	LENGTH	SLOPE	VEL.	t	COMP.	MINIMUM	
				Ac			Ft	%	Min	Ft	%	FPS	Min	t _c	t _c	Min
OS1	A	0.49	0.66	1.34	0.66	0.88	30	2.0	5.0	20	5.0	5.5	0.1	5.0	5.0	5.0
E1		0.08	0.35	13.85	1.16	4.88	300	3.0	22.8	530	3.0	3.5	2.5	25.3	5.0	25.3
DPA+E1	В	0.12	0.38	15.19				From E1						25.3	5.0	25.3
OS2	С	0.49	0.66	0.60	0.29	0.39	30	1.0	6.2	20	5.0	5.5	0.1	6.3	5.0	6.3
OS3	D	0.09	0.36	2.56	0.23	0.91	200	2.1	20.9	250	4.0	5.0	0.8	21.7	5.0	21.7
E2		0.08	0.35	12.88	1.03	4.51	300	2.3	24.9	1360	3.5	4.0	5.7	30.6	5.0	30.6
DPC+DPD+E2	E	0.10	0.36	16.04				From E2						30.6	5.0	30.6
E3	F	0.08	0.35	13.11	1.05	4.59	300	2.3	24.9	1120	4.2	5.0	3.7	28.6	5.0	28.6
OS4	G	0.28	0.50	1.54	0.43	0.76	75	2.0	10.6	825	5.0	5.5	2.5	13.1	5.0	13.1
E4		0.08	0.35	1.57	0.13	0.55	300	2.7	23.8	250	4.0	5.0	0.8	24.7	5.0	24.7
DPG+E4	Н	0.18	0.42	3.11				From E4						24.7	5.0	24.7
E5		0.12	0.38	5.91	0.72	2.24	100	2.0	14.5	550	2.2	1.8	5.1	19.6	5.0	19.6
OS5	J	0.20	0.44	16.62	3.40	7.34	75	2.0	11.5	2500	1.5	1.2	34.7	46.2	5.0	46.2
OS6	L	0.55	0.70	0.91	0.50	0.63	30	2.0	4.5					4.5	5.0	5.0
E6		0.08	0.35	10.37	0.83	3.63	300	2.3	24.9	1080	1.5	1.2	15.0	39.9	5.0	39.9
DPJ+DPL+E6	М	0.17	0.42	27.89				From OS5		1080	1.5	1.2	15.0	54.9	5.0	54.9

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EXISTING	EXISTING RUNOFF			YR	STORM	P1=	1.50
			DIRECT RUNC)FF			
BASIN (S)	DESIGN POINT	AREA (AC)	RUNOFF COEFF	t _c (MIN)	C * A	I (IN/HR)	Q (CFS)
OS1	Α	1.34	0.49	5.0	0.66	5.16	3.4
E1		13.85	0.08	25.3	1.16	2.73	3.2
RET090 (DBPS)							36.0
DPA+E1+RET090	В	15.19	0.12	25.3	1.82	2.73	41.0
OS2	С	0.60	0.49	6.3	0.29	4.82	1.4
OS3	D	2.56	0.09	21.7	0.23	2.97	0.7
E2		12.88	0.08	30.6	1.03	2.45	2.5
DPC+DPD+E2	E	16.04	0.10	30.6	1.55	2.45	3.8
E3	F	13.11	0.08	28.6	1.05	2.55	2.7
OS4	G	1.54	0.28	13.1	0.43	3.73	1.6
E4		1.57	0.08	24.7	0.13	2.78	0.3
DPG+E4	Н	3.11	0.18	24.7	0.55	2.78	1.5
E5	I	5.91	0.12	19.6	0.72	3.12	2.2
OS5	J	16.62	0.20	46.2	3.40	1.83	6.2
OS6	L	0.91	0.55	5.0	0.50	5.17	2.6
E6		10.37	0.08	39.9	0.83	2.05	1.7
DPJ+DPL+E6	М	27.89	0.17	54.9	4.73	1.57	7.4

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Drexel, Barrell & Co.

EXISTING	RUNOFF		100	YR	STORM	P1=	2.52
			DIRECT RUNC)FF			
BASIN (S)	DESIGN POINT	AREA (AC)	RUNOFF COEFF	t _c (MIN)	C * A	I (IN/HR)	Q (CFS)
OS1	А	1.34	0.66	5.0	0.88	8.67	7.6
E1		13.85	0.35	25.3	4.88	4.59	22.4
RET090 (DBPS)							320.0
DPA+E1+RET090	В	15.19	0.38	25.3	5.76	4.59	346.4
OS2	С	0.60	0.66	6.3	0.39	8.09	3.2
OS3	D	2.56	0.36	21.7	0.91	4.98	4.5
E2		12.88	0.35	30.6	4.51	4.12	18.6
DPC+DPD+E2	E	16.04	0.36	30.6	5.81	4.12	23.9
E3	F	13.11	0.35	28.6	4.59	4.28	19.6
OS4	G	1.54	0.50	13.1	0.76	6.26	4.8
E4		1.57	0.35	24.7	0.55	4.66	2.6
DPG+E4	Н	3.11	0.42	24.7	1.31	4.66	6.1
E5	I	5.91	0.38	19.6	2.24	5.23	11.7
OS5	J	16.62	0.44	46.2	7.34	3.07	22.6
OS6	L	0.91	0.70	5.0	0.63	8.68	5.5
E6		10.37	0.35	39.9	3.63	3.44	12.5
DPJ+DPL+E6	М	27.89	0.42	54.9	11.61	2.64	30.7

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	C2*	C5*	C10*	C100*	% IMPERV
Open Space		0.08		0.35	0
Commercial Development		0.81		0.88	95
Residential (< 1/8 Acre)		0.45		0.59	65
Streets: Paved		0.90		0.96	100
Streets: Gravel		0.59		0.70	80

DEVELOPED CONIDTION

SUB-BASIN	SURFACE DESIGNATION	AREA	COMPOSIT	E RUNOFF CO	EFFICIENTS		% IMPERV
-		ACRE	C2	C5	C10	C100	
		A	BASINS	•		•	
OSA	Open Space	13.94		0.08		0.35	0
	Roofs	0.05		0.73		0.81	90
	Lawns	0.00		0.08		0.35	0
	Streets: Paved	2.25		0.90		0.96	100
	Streets: Gravel	0.39		0.59		0.70	80
	WEIGHTED AVERAGE			0.20		0.44	16%
TOTAL OSA		16.62					
A1	Open Space	0.00		0.08		0.35	0
	Commercial Development	0.25		0.81		0.88	95
	Residential (< 1/8 Acre)	0.00		0.45		0.59	65
	Streets: Paved	0.49		0.90		0.96	100
	Streets: Gravel	0.00		0.59		0.70	80
	WEIGHTED AVERAGE			0.87		0.93	98%
TOTAL A1		0.74					
A2	Open Space	0.80		0.08		0.35	0
	Commercial Development	0.00		0.81		0.88	95
	Residential (< 1/8 Acre)	0.34		0.45		0.59	65
	Streets: Paved	0.39		0.90		0.96	100
	Streets: Gravel	0.00		0.59		0.70	80
	WEIGHTED AVERAGE			0.37		0.56	40%
TOTAL A2		1.52					
A3	Open Space	0.36		0.08		0.35	0
	Commercial Development	0.00		0.81		0.88	95
	Residential (< 1/8 Acre)	0.87		0.45		0.59	65
	Streets: Paved	0.24		0.90		0.96	100
	Streets: Gravel	0.00		0.59		0.70	80
	WEIGHTED AVERAGE			0.43		0.59	55%
TOTAL A3		1.48					
A4	Open Space	0.72		0.08		0.35	0
	Commercial Development	0.00		0.00		0.88	95
	Residential (< 1/8 Acre)	1.67		0.45		0.59	65
	Streets: Paved	0.47		0.43		0.96	100
	Streets: Gravel	0.00		0.59		0.30	80
	WEIGHTED AVERAGE	0.00		0.33		0.59	54%
TOTAL A4		2.87		0.40		0.00	J 1 /0
		0.00		0.00		0.05	
A5	Open Space	0.00		0.08		0.35	0

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	C2*	C5*	C10*	C100*	% IMPERV
Open Space		0.08		0.35	0
Commercial Development		0.81		0.88	95
Residential (< 1/8 Acre)		0.45		0.59	65
Streets: Paved		0.90		0.96	100
Streets: Gravel		0.59		0.70	80

	Commercial Development	0.00	0.81	0.88	95
	Residential (< 1/8 Acre)	1.23	0.45	0.59	65
	Streets: Paved	0.24	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.52	0.65	71%
TOTAL A5		1.47			
A6	Open Space	0.00	0.08	0.35	0
	Commercial Development	0.00	0.81	0.88	95
	Residential (< 1/8 Acre)	3.26	0.45	0.59	65
	Streets: Paved	0.04	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE	0.00	0.46	0.59	65%
TOTAL A6		3.30	0.10	0.00	0070
A7	0.000	0.00	0.08	0.35	0
A/	Open Space		0.00		95
	Commercial Development Residential (< 1/8 Acre)	0.00 1.76		0.88	
	()	0.00	0.45 0.90	0.59 0.96	65 100
	Streets: Paved	0.00	0.59	0.96	80
	Streets: Gravel	0.00	0.59	0.70	65%
TOTAL A7	WEIGHTED AVERAGE	1.76	0.45	0.59	05%
IUTALA		1.70			
A8	Open Space	0.00	0.08	0.35	0
	Commercial Development	0.00	0.81	0.88	95
	Residential (< 1/8 Acre)	0.65	0.45	0.59	65
	Streets: Paved	0.00	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.45	0.59	65%
TOTAL A8		0.65			
A9	Open Space	0.00	0.08	0.35	0
	Commercial Development	0.00	0.81	0.88	95
	Residential (< 1/8 Acre)	2.36	0.45	0.59	65
	Streets: Paved	0.20	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE	0.00	0.48	0.62	68%
TOTAL A9		2.56			
A10	Open Space	0.00	0.08	0.25	0
AIV	Open Space		0.08	0.35	95
	Commercial Development	0.00		0.88	
	Residential (< 1/8 Acre)	1.10	0.45	0.59	65
	Streets: Paved	0.00	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80

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	C2*	C5*	C10*	C100*	% IMPERV
Open Space		0.08		0.35	0
Commercial Development		0.81		0.88	95
Residential (< 1/8 Acre)		0.45		0.59	65
Streets: Paved		0.90		0.96	100
Streets: Gravel		0.59		0.70	80

	WEIGHTED AVERAGE	Г	0.45	0.59	65%
TOTAL A10		1.10			
		4.07	0.00	0.05	
A11	Open Space	1.07	0.08	0.35	0
	Commercial Development	0.00	0.81	0.88	95
	Residential (< 1/8 Acre)	0.00	0.45	0.59	65
	Streets: Paved	0.00	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.08	0.35	0%
TOTAL A11		1.07			
A12	Open Space	1.26	0.08	0.35	0
	Commercial Development	0.00	0.00	0.35	95
	Residential (< 1/8 Acre)	0.00	0.81	0.88	95 65
	Streets: Paved	0.00	0.45	0.96	100
	Streets: Gravel	0.00	0.59	0.98	80
		0.00			
	WEIGHTED AVERAGE	4.00	0.12	0.38	4%
TOTAL A12		1.32			
A13	Open Space	1.20	0.08	0.35	0
	Commercial Development	0.00	0.81	0.88	95
	Residential (< 1/8 Acre)	0.00	0.45	0.59	65
	Streets: Paved	0.00	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.08	0.35	0%
TOTAL A13		1.20			
		0.04			
A14	Open Space	0.61	0.08	0.35	0
	Commercial Development	0.00	0.81	0.88	95
	Residential (< 1/8 Acre)	0.00	0.45	0.59	65
	Streets: Paved	0.00	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.08	0.35	0%
TOTAL A14		0.61			

Area tributary to Pond A (A1-A11)

0.45

0.59

0.60

	B-BASINS								
OSB1	Open Space	0.00	0.08	0.35	0				
	Commercial Development	0.15	0.81	0.88	95				
	Residential (< 1/8 Acre)	0.00	0.45	0.59	65				
	Streets: Paved	0.68	0.90	0.96	100				
	Streets: Gravel	0.00	0.59	0.70	80				
	WEIGHTED AVERAGE		0.88	0.95	99%				

18.51

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	C2*	C5*	C10*	C100*	% IMPERV
Open Space		0.08		0.35	0
Commercial Development		0.81		0.88	95
Residential (< 1/8 Acre)		0.45		0.59	65
Streets: Paved		0.90		0.96	100
Streets: Gravel		0.59		0.70	80

TOTAL OSB1		0.83			
OSB2	Open Space	0.00	0.08	0.35	0
	Commercial Development	0.00	0.81	0.88	95
	Residential (< 1/8 Acre)	0.00	0.45	0.59	65
	Streets: Paved	0.32	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE	0.00	0.90	0.96	100%
TOTAL OSB2	0 0	0.32	0.00	0.25	
OSB3	Open Space	0.00	0.08	0.35	0
	Commercial Development	0.00	0.81	0.88	95 65
	Residential (< 1/8 Acre) Streets: Paved	0.00 0.56	0.45 0.90	0.59 0.96	65 100
	Streets: Gravel	0.00	0.59	0.96	80
	WEIGHTED AVERAGE	0.00	0.39	0.70	100%
TOTAL OSB3	WEIGHTED AVERAGE	0.56	0.50	0.90	100 /6
		0.00			
B1	Open Space	0.00	0.08	0.35	0
	Commercial Development	1.99	0.81	0.88	95
	Residential (< 1/8 Acre)	0.00	0.45	0.59	65
	Streets: Paved	0.00	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.81	0.88	95%
TOTAL B1		1.99			
50		0.00	0.00	0.05	0
B2	Open Space	0.00	0.08	0.35	0
	Commercial Development	1.11	0.81	0.88	95
	Residential (< 1/8 Acre)	0.00	0.45	0.59	65
	Streets: Paved	0.00	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.81	0.88	95%
TOTAL B2		1.11			
B3	Open Space	0.00	0.08	0.35	0
UJ	Open Space				
	Commercial Development	0.00	0.81	0.88	95
	Residential (< 1/8 Acre)	0.00	0.45	0.59	65
	Streets: Paved	0.35	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.90	0.96	100%
TOTAL B3		0.35			

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			C2*	C5*	C10*	C100*	% IMPERV
Open Space				0.08		0.35	0
Commercial Deve	elopment			0.81		0.88	95
Residential (< 1/8	Acre)			0.45		0.59	65
Streets: Paved				0.90		0.96	100
Streets: Gravel				0.59		0.70	80
B4	Open Space	0.00		0.08		0.35	0
	Commercial Development	1.53		0.81		0.88	95
	Residential (< 1/8 Acre)	0.00		0.45		0.59	65
	Streets: Paved	0.00		0.90		0.96	100
	Streets: Gravel	0.00		0.59		0.70	80
	WEIGHTED AVERAGE			0.81		0.88	95%
TOTAL B4		1.53					
B5	Open Space	0.00		0.08		0.35	0
55	Commercial Development	0.00		0.81		0.88	95
	Streets: Paved	0.00		0.90		0.88	100
	Streets: Gravel	0.23		0.59		0.90	80
	WEIGHTED AVERAGE	0.00		0.90		0.70	100%
TOTAL B5	WEIGHTED AVERAGE	0.25		0.90		0.90	100 %
		0.20					
B6	Open Space	0.00		0.08		0.35	0
	Commercial Development	0.00		0.81		0.88	95
	Residential (< 1/8 Acre)	0.00		0.45		0.59	65
	Streets: Paved	0.37		0.90		0.96	100
	Streets: Gravel	0.00		0.59		0.70	80
	WEIGHTED AVERAGE			0.90		0.96	100%
TOTAL B6		0.37					
D7	0	0.00		0.08		0.25	0
B7	Open Space					0.35	0
	Commercial Development	1.97		0.81		0.88	95
	Residential (< 1/8 Acre)	0.00		0.45		0.59	65
	Streets: Paved	0.00	ļ	0.90		0.96	100
	Streets: Gravel	0.00		0.59		0.70	80
TOTAL B7	WEIGHTED AVERAGE	1.97		0.81		0.88	95%
		1.97					
B8	Open Space	0.00	1	0.08		0.35	0
	Commercial Development	1.52		0.81		0.88	95
	Streets: Paved	0.00		0.90		0.96	100
	Streets: Gravel	0.00		0.59		0.70	80
	WEIGHTED AVERAGE			0.81		0.88	95%

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	C2*	C5*	C10*	C100*	% IMPERV
Open Space		0.08		0.35	0
Commercial Development		0.81		0.88	95
Residential (< 1/8 Acre)		0.45		0.59	65
Streets: Paved		0.90		0.96	100
Streets: Gravel		0.59		0.70	80

TOTAL B8		1.52				
B9	Open Space	0.00	0.08	().35	0
	Commercial Development	0.00	0.81	().88	95
	Streets: Paved	0.89	0.90	().96	100
	Streets: Gravel	0.00	0.59	().70	80
	WEIGHTED AVERAGE		0.90	().96	100%
TOTAL B9		0.89				
B10	Open Space	0.00	0.08	().35	0
	Commercial Development	0.00	0.81).88	95
	Streets: Paved	0.71	0.90	().96	100
	Streets: Gravel	0.00	0.59	().70	80
	WEIGHTED AVERAGE		0.90	().96	100%
TOTAL B10		0.71				
B11	Open Space	1.14	0.08	().35	0
	Commercial Development	0.00	0.81	().88	95
	Streets: Paved	0.00	0.90	().96	100
	Streets: Gravel	0.00	0.59	().70	80
	WEIGHTED AVERAGE		0.08	().35	0%
TOTAL B11		1.14				

Area tributary to Pond B (OSB1+B11)

13.55

0.78

0.89

0.86

	C-BASINS									
OSC1	Open Space	0.00		0.08		0.35	0			
	Commercial Development	0.00		0.81		0.88	95			
	Residential (< 1/8 Acre)	0.00		0.45		0.59	65			
	Streets: Paved	0.37		0.90		0.96	100			
	Streets: Gravel	0.00		0.59		0.70	80			
	WEIGHTED AVERAGE			0.90		0.96	100%			
TOTAL OSC1		0.37								
OSC2	Open Space	0.97		0.08		0.35	0			
	Commercial Development	0.00		0.81		0.88	95			

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			C2*	C5*	C10*	C100*	% IMPERV
Open Space				0.08		0.35	0
Commercial Dev	elopment			0.81		0.88	95
Residential (< 1/8 Acre)			0.45		0.59	65	
Streets: Paved				0.90		0.96	100
Streets: Gravel				0.59		0.70	80
	Residential (< 1/8 Acre)	0.00		0.45		0.59	65
	Streets: Paved	0.39		0.90		0.96	100
	Streets: Gravel	0.00		0.59		0.70	80
	WEIGHTED AVERAGE			0.32		0.53	29%
TOTAL OCOD		4.00					

	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.32	0.53	29%
TOTAL OSC2		1.36			
C1	Open Space	0.00	0.08	0.35	0
	Commercial Development	0.00	0.81	0.88	95
	Residential (< 1/8 Acre)	0.00	0.45	0.59	65
	Streets: Paved	0.25	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.90	0.96	100%
TOTAL C1		0.25			
C2	Open Space	0.00	0.08	0.35	0
	Commercial Development	2.26	0.81	0.88	95
	Residential (< 1/8 Acre)	0.00	0.45	0.59	65
	Streets: Paved	0.00	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.81	0.88	95%
TOTAL C2		2.26			
C3	Open Space	0.00	0.08	0.35	0
	Commercial Development	1.15	0.81	0.88	95
	Residential (< 1/8 Acre)	0.00	0.45	0.59	65
	Streets: Paved	0.00	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.81	0.88	95%
TOTAL C3		1.15			
C4	Open Space	0.00	0.08	0.35	0
	Commercial Development	1.41	0.81	0.88	95
	Residential (< 1/8 Acre)	0.00	0.45	0.59	65
	Streets: Paved	0.00	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.81	0.88	95%

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	C2*	C5*	C10*	C100*	% IMPERV
Open Space		0.08		0.35	0
Commercial Development		0.81		0.88	95
Residential (< 1/8 Acre)		0.45		0.59	65
Streets: Paved		0.90		0.96	100
Streets: Gravel		0.59		0.70	80

TOTAL C4		1.41			
C5	Open Space	0.00	0.08	0.35	0
00	Commercial Development	0.00	0.81	0.88	95
	Residential (< 1/8 Acre)	0.00	0.45	0.59	65
	Streets: Paved	0.00	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.30	80
	WEIGHTED AVERAGE	0.00	0.90	0.96	100%
TOTAL C5	WEIGHTED AVERAGE	0.17	0.50	0.50	100 /0
C6	Open Space	0.00	0.08	0.35	0
	Commercial Development	0.00	0.81	0.88	95
	Residential (< 1/8 Acre)	0.00	0.45	0.59	65
	Streets: Paved	0.18	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.90	0.96	100%
TOTAL C6		0.18			
C7	Open Space	0.00	0.08	0.35	0
	Commercial Development	0.00	0.81	0.88	95
	Streets: Paved	0.88	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.90	0.96	100%
TOTAL C7		0.88			
C8	Open Space	0.00	0.08	0.35	0
	Commercial Development	0.00	0.81	0.88	95
	Residential (< 1/8 Acre)	0.00	0.45	0.59	65
	Streets: Paved	0.65	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.90	0.96	100%
TOTAL C8		0.65			
		D-B	ASINS		
OSD1	Open Space	2.70	0.08	0.35	0
	Commercial Development	0.00	0.81	0.88	95

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			C2*	C5*	C10*	C100*	% IMPERV
Open Space				0.08		0.35	0
Commercial Dev	elopment			0.81		0.88	95
Residential (< 1/8	3 Acre)			0.45		0.59	65
Streets: Paved				0.90		0.96	100
Streets: Gravel				0.59		0.70	80
1						0.50	
	Residential (< 1/8 Acre)	0.00		0.45		0.59	65
	Streets: Paved	0.00		0.90		0.96	100
	Streets: Gravel	0.00		0.59		0.70	80
	WEIGHTED AVERAGE			0.08		0.35	0%
TOTAL OSD1		2.70					
D1	Open Space	0.42		0.08		0.35	0
	Commercial Development	0.00		0.81		0.88	95
	Residential (< 1/8 Acre)	0.87		0.45		0.59	65
	Streets: Paved	0.07		0.90		0.96	100
	Streets: Gravel	0.00		0.59		0.70	80
	WEIGHTED AVERAGE			0.36		0.53	47%
TOTAL D1		1.36					
D2	Open Space	0.38		0.08		0.35	0
	Commercial Development	0.00		0.81		0.88	95
	Residential (< 1/8 Acre)	1.56		0.45		0.59	65
	Streets: Paved	0.00		0.90		0.96	100
	Streets: Gravel	0.00		0.59		0.70	80
	WEIGHTED AVERAGE			0.38		0.54	52%
TOTAL D2		1.95					
D3	Open Space	0.13		0.08		0.35	0
	Commercial Development	0.00		0.81		0.88	95
	Residential (< 1/8 Acre)	0.78		0.45		0.59	65
	Streets: Paved	0.00		0.90		0.96	100
	Streets: Gravel	0.00		0.59		0.70	80
	WEIGHTED AVERAGE			0.40		0.56	56%
TOTAL D3		0.91					
D4	Open Space	0.63		0.08		0.35	0
	Commercial Development	0.00		0.81		0.88	95
	Residential (< 1/8 Acre)	1.98		0.45		0.59	65
	Streets: Paved	0.14		0.90		0.96	100
	Streets: Gravel	0.00		0.59		0.70	80
	WEIGHTED AVERAGE			0.39		0.55	52%

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	C2*	C5*	C10*	C100*	% IMPERV
Open Space		0.08		0.35	0
Commercial Development		0.81		0.88	95
Residential (< 1/8 Acre)		0.45		0.59	65
Streets: Paved		0.90		0.96	100
Streets: Gravel		0.59		0.70	80

TOTAL D4		2.75			
D5	Open Space	0.00	0.08	0.35	0
20	Commercial Development	0.00	0.81	0.88	95
	Residential (< 1/8 Acre)	0.48	0.45	0.59	65
	Streets: Paved	0.40	0.90	0.96	100
	Streets: Gravel	0.14	0.59	0.30	80
	WEIGHTED AVERAGE	0.00	0.55	0.70	73%
TOTAL D5	WEIGHTED AVERAGE	0.62	0.00	0.07	1570
IOTAL DJ		0.02			
D6	Open Space	0.00	0.08	0.35	0
	Commercial Development	0.00	0.81	0.88	95
	Residential (< 1/8 Acre)	2.68	0.45	0.59	65
	Streets: Paved	0.00	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.45	0.59	65%
TOTAL D6		2.68			
D7	Open Space	0.09	0.08	0.35	0
	Commercial Development	0.00	0.81	0.88	95
	Residential (< 1/8 Acre)	0.49	0.45	0.59	65
	Streets: Paved	0.16	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.50	0.64	65%
TOTAL D7		0.74			
D8	Open Space	0.00	0.08	0.35	0
	Commercial Development	0.00	0.81	0.88	95
	Residential (< 1/8 Acre)	0.44	0.45	0.59	65
	Streets: Paved	0.00	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.45	0.59	65%
TOTAL D8		0.44			
<u></u>		0.00	0.00	0.05	
D9	Open Space	0.09	0.08	0.35	0
	Commercial Development	0.00	0.81	0.88	95

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Commons at Falcon Field 21604-00 KGV TDM El Paso County Preliminary 7/5/2024



			C2*	C5*	C10*	C100*	% IMPERV
Open Space				0.08		0.35	0
Commercial Deve	elopment			0.81	-	0.88	95
Residential (< 1/8				0.45		0.59	65
Streets: Paved				0.90		0.96	100
Streets: Gravel				0.59		0.70	80
			1	A 1-		0.50	
	Residential (< 1/8 Acre)	0.22		0.45		0.59	65
	Streets: Paved	0.00		0.90		0.96	100
	Streets: Gravel	0.00		0.59		0.70	80
	WEIGHTED AVERAGE			0.34		0.52	45%
TOTAL D9		0.31					
D 40		0.00		0.00		0.05	0
D10	Open Space	0.38		0.08		0.35	0
	Commercial Development	0.00		0.81		0.88	95
	Residential (< 1/8 Acre)	0.96		0.45		0.59	65
	Streets: Paved	0.00		0.90		0.96	100
	Streets: Gravel	0.00		0.59		0.70	80
	WEIGHTED AVERAGE			0.35		0.52	47%
TOTAL D10		1.34					
D11	Open Space	0.00		0.08		0.35	0
	Commercial Development	0.00		0.81		0.88	95
	Residential (< 1/8 Acre)	0.00		0.45		0.59	65
	Streets: Paved	0.61		0.90		0.96	100
	Streets: Gravel	0.00		0.59		0.70	80
	WEIGHTED AVERAGE			0.90		0.96	100%
TOTAL D11		0.61					
D12	Open Space	1.51		0.08		0.35	0
	Commercial Development	0.00		0.81		0.88	95
	Residential (< 1/8 Acre)	0.00		0.81		0.88	95 65
	Streets: Paved	0.00		0.43		0.96	100
	Streets: Gravel	0.00		0.59		0.90	80
	WEIGHTED AVERAGE	0.00		0.08		0.70	0%
	WEIGHTED AVERAGE	1 5 1		0.00		0.55	0%
TOTAL D12		1.51					
D13	Open Space	1.98		0.08		0.35	0
	Commercial Development	0.00	1	0.81		0.88	95
	Residential (< 1/8 Acre)	0.00		0.45		0.59	65
	Streets: Paved	0.00		0.90		0.96	100
	Streets: Gravel	0.00		0.59		0.70	80
	WEIGHTED AVERAGE	0.00		0.08	ļ	0.35	0%

604-00CSCV\Reports\Drainage\Urban Rational - Falcon Field.xlsx **\& C-VALUES DEV**

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	C2*	C5*	C10*	C100*	% IMPERV
Open Space		0.08		0.35	0
Commercial Development		0.81		0.88	95
Residential (< 1/8 Acre)		0.45		0.59	65
Streets: Paved		0.90		0.96	100
Streets: Gravel		0.59		0.70	80

TOTAL D13		1.98			
D14	Open Space	0.76	0.08	0.35	0
	Commercial Development	0.00	0.81	0.88	95
	Residential (< 1/8 Acre)	0.00	0.45	0.59	65
	Streets: Paved	0.00	0.90	0.96	100
	Streets: Gravel	0.00	0.59	0.70	80
	WEIGHTED AVERAGE		0.08	0.35	0%
TOTAL D14		0.76			

Area tributary to Pond C 26.61 (OSC1-C8 & D1-D12) 0.48

0.63 0.58

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RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

DEVELOPED TIME OF CONCENTRATION

		SUB-BASI DATA	N		INITIAL/OVERLAND TIME (t _i)				TRAVEL (t _t)	TIME			PIPE TRA (t _t)	VEL TIME		TIME OF CO	NCENTRATION	FINAL		
BASIN	DESIGN PT:	C ₅	C ₁₀₀	AREA	COMP		LENGTH	SLOPE	ti	LENGTH	SLOPE	VEL.	t,	LENGTH	SLOPE	VEL.	t,	COMP.	MINIMUM	
				Ac			Ft	%	Min	Ft	%	FPS	Min	Ft	%	FPS	Min	tc	t _c	Min
									A-BA	SINS										
OSA		0.20	0.44	16.62	3.40	7.35	75	2.0	11.3	2500	1.5	5.2	8.0					19.3	5.0	19.3
A1	1	0.87	0.93	0.74	0.65	0.69	20	3.3	1.3	500	3.3	7.7	1.1					2.4	5.0	5.0
A2		0.37	0.56	1.52	0.56	0.85	20	3.5	3.9	514	3.4	7.8	1.1					5.0	5.0	5.0
DP1+A2	2	0.53	0.68	2.27	1.21	1.54		From DP1						70	0.7	5.8	0.2	5.2	5.0	5.2
A3	3	0.43	0.59	1.48	0.64	0.87	20	2.0	4.3	835	2.4	6.2	2.2					6.6	5.0	6.6
A4	4	0.43	0.59	2.87	1.24	1.70	20	2.0	4.4	750	1.8	6.3	2.0					6.3	5.0	6.3
A5	-	0.52	0.65	1.47	0.77	0.95	20	2.0	3.8	720	1.0	5.0	2.4					6.2	5.0	6.2
DP4+DP5 A6	5	0.46	0.61	4.34	2.01	2.65	100	From DP4 1.0	11.0	650	1.0	5.0	2.2					8.5	5.0	8.5
DP5+DP6	6A	0.46	0.59	3.30 7.64	1.50 3.51	1.96 4.61	100	From DP6	11.8	835	1.8	5.7	2.4	20	1.0	6.5	0.1	14.3 14.3	5.0 5.0	14.3 14.3
A7	7	0.40	0.59	1.76	0.79	4.01	100	1.5	10.4	440	0.5	3.8	1.9	20	1.0	0.0	0.1	14.3	5.0	14.3
A8	8	0.45	0.59	0.65	0.29	0.38	40	2.0	6.0	390	1.8	5.7	1.5					7.1	5.0	7.1
A9	Ŭ	0.48	0.62	2.56	1.24	1.58	20	2.0	4.0	850	1.8	5.7	2.5					6.5	5.0	6.5
DP7+DP8+A9	9	0.47	0.60	4.97	2.33	3.01		From DP7		190	0.5	4.9	0.6					13.0	5.0	13.0
A10		0.45	0.59	1.10	0.49	0.65	100	2.0	9.5	150	0.5	4.9	0.5					10.0	5.0	10.0
DP3+A10	10	0.44	0.59	2.57	1.13	1.52		From A10										10.0	5.0	10.0
DP6A+DP9+DP10	10A	0.46	0.60	15.18	6.97	9.14		From DP6A						240	0.5	5.8	0.7	15.0	5.0	15.0
A11		0.08	0.35	1.07	0.09	0.37	100	2.1	14.6	250	0.9	4.9	0.9					15.5	5.0	15.5
DP2+DP10A+A11	11	0.45	0.60	18.51	8.26	11.05		From DP3						5.5	1.0	5.8	0.02	6.6	5.0	6.6
A12	10	0.12	0.38	1.32	0.15	0.50	100	1.0	18.1	850	1.0	5.0	2.8					20.9	5.0	20.9
OSA+A12	12	0.20	0.44	17.94	3.56	7.84		From OSA		2500	1.5	5.2	8.0					27.3	5.0	27.3
A13	13	0.08	0.35	1.20	0.10	0.42	25	18.0	3.6	72	10.0	14.0	0.1					3.7	5.0 5.0	5.0
A14		0.08	0.35	0.61	0.05	0.21	25	2.1	7.3	250	3.0	5.8	0.7	-				8.0	5.0	8.0
B-BASINS																				
OSB1		0.88	0.95	0.83	0.74	0.79	40	2.0	2.0	100	1.0	5.0	0.3					2.4	5.0	5.0
OSB2		0.90	0.96	0.32	0.29	0.31	40	2.0	1.9	100	1.0	5.0	0.3					2.2	5.0	5.0
OSB3		0.90	0.96	0.56	0.50	0.54	40	2.0	1.9	150	1.0	5.0	0.5					2.4	5.0	5.0
B1		0.81	0.88	1.99	1.61	1.75	60	2.3	3.2	300	3.3	6.6	0.8					4.0	5.0	5.0
OSB1+B1	1	0.83	0.90	2.82	2.35	2.54		From OS1		300	3.3	6.6	0.8					5.8	5.0	5.8
B2		0.81	0.88	1.11	0.90	0.98	40	4.0	2.2	200	4.0	7.0	0.5					2.6	5.0	5.0
OSB2+B2	2	0.83	0.90	1.44	1.19	1.29		From OS2	4.0	200	4.0	7.0	0.5					5.5	5.0	5.5
B3	3	0.90	0.96	0.35	0.32	0.34	20	2.0	1.3	200	3.3	6.3	0.5					1.9	5.0	5.0
B4		0.81	0.88	1.53	1.24	1.35	50	3.5	2.5	280	2.0	5.5	0.8					3.4	5.0	5.0
OSB3+B4	4	0.83	0.90	2.09	1.75	1.89		From OS3		280	2.0	5.5	0.8					5.8	5.0	5.8
DP3+DP4	4A	0.84	0.91	2.44	2.06	2.22		From DP4						405	10	7.0	0.5	5.8	5.0	5.8
DP1+DP2+DP4A	4B	0.84	0.90	6.70	5.60	6.05		From DP1						195	1.0	7.2	0.5	6.2	5.0	6.2
B5	5	0.90	0.96	0.25	0.23	0.24	20	2.0	1.3	400	1.5	5.5	1.2					2.5	5.0	5.0
B6		0.90	0.96	0.37	0.33	0.36	20	2.0	1.3	340	1.5	5.5	1.0				_	2.4	5.0	5.0
DP5+B6			0.96	0.62	0.56	0.60		From DP5						30	1.0	7.2	0.1	5.1	5.0	5.1
	6	0.90																		
B7		0.81	0.88	1.97	1.59	1.73	40	2.0	2.7	310	2.3	5.9	0.9					3.6	5.0	5.0
B7 DP4B+DP6+B7	7			1.97 9.29		1.73 8.38	40	2.0 From DP4B	2.7	310		5.9		251	1.0	7.2	0.6	5.6	5.0	5.6
B7		0.81	0.88	1.97	1.59		40 40	-	2.7	310 210	2.3 2.8	5.9 6.1	0.9	251	1.0	7.2	0.6			
B7 DP4B+DP6+B7	7	0.81 0.83	0.88 0.90	1.97 9.29	1.59 7.75	8.38		From DP4B						251	1.0	7.2	0.6	5.6	5.0	5.6
B7 DP4B+DP6+B7 B8	7	0.81 0.83 0.81	0.88 0.90 0.88	1.97 9.29 1.52	1.59 7.75 1.23	8.38 1.34	40	From DP4B 1.0	3.4	210	2.8	6.1	0.6	251	1.0	7.2	0.6	5.6 4.0	5.0 5.0	5.6 5.0
B7 DP4B+DP6+B7 B8 B9	7 8	0.81 0.83 0.81 0.90	0.88 0.90 0.88 0.96	1.97 9.29 1.52 0.89	1.59 7.75 1.23 0.80	8.38 1.34 0.85	40	From DP4B 1.0 2.0	3.4	210	2.8	6.1	0.6					5.6 4.0 4.3 5.0	5.0 5.0 5.0	5.6 5.0 5.0
B7 DP48+DP6+B7 B8 B9 DP8+B9 B10	7 8 9	0.81 0.83 0.81 0.90 0.84 0.90	0.88 0.90 0.88 0.96 0.91 0.96	1.97 9.29 1.52 0.89 2.41 0.71	1.59 7.75 1.23 0.80 2.03 0.64	8.38 1.34 0.85 2.19 0.68	40 30	From DP4B 1.0 2.0 From DP8	3.4 1.6	210 800	2.8 1.5	6.1 5.0	0.6	20	1.0	7.2	0.0	5.6 4.0 4.3 5.0 3.4	5.0 5.0 5.0 5.0 5.0 5.0	5.6 5.0 5.0 5.0 5.0 5.0
B7 DP48+DP6+B7 B8 B9 DP8+B9 B10 DP9+B10	7 8 9 10	0.81 0.83 0.81 0.90 0.84 0.90 0.86	0.88 0.90 0.88 0.96 0.91 0.96 0.92	1.97 9.29 1.52 0.89 2.41 0.71 3.12	1.59 7.75 1.23 0.80 2.03 0.64 2.67	8.38 1.34 0.85 2.19 0.68 2.87	40 30	From DP4B 1.0 2.0 From DP8 2.0 From DP9	3.4 1.6	210 800	2.8 1.5	6.1 5.0	0.6	20	1.0	7.2	0.0	5.6 4.0 4.3 5.0 3.4 5.2	5.0 5.0 5.0 5.0 5.0 5.0 5.0	5.6 5.0 5.0 5.0 5.0 5.0 5.2
B7 DP48+DP6+B7 B8 B9 DP8+B9 B10 DP9+B10 DP7+DP10	7 8 9	0.81 0.83 0.81 0.90 0.84 0.90 0.86 0.84	0.88 0.90 0.88 0.96 0.91 0.96 0.92 0.91	1.97 9.29 1.52 0.89 2.41 0.71 3.12 12.41	1.59 7.75 1.23 0.80 2.03 0.64 2.67 10.42	8.38 1.34 0.85 2.19 0.68 2.87 11.25	40 30 30	From DP4B 1.0 2.0 From DP8 2.0 From DP9 From DP7	3.4 1.6 1.6	210 800 530	2.8 1.5 1.5	6.1 5.0 5.0	0.6 2.7 1.8	20	1.0	7.2	0.0	5.6 4.0 4.3 5.0 3.4 5.2 5.8	5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0	5.6 5.0 5.0 5.0 5.0 5.0 5.2 5.8
B7 DP48+DP6+87 B8 B9 DP8+89 B10 DP9+810	7 8 9 10	0.81 0.83 0.81 0.90 0.84 0.90 0.86	0.88 0.90 0.88 0.96 0.91 0.96 0.92	1.97 9.29 1.52 0.89 2.41 0.71 3.12	1.59 7.75 1.23 0.80 2.03 0.64 2.67	8.38 1.34 0.85 2.19 0.68 2.87	40 30	From DP4B 1.0 2.0 From DP8 2.0 From DP9	3.4 1.6	210 800	2.8 1.5	6.1 5.0	0.6	20	1.0	7.2	0.0	5.6 4.0 4.3 5.0 3.4 5.2	5.0 5.0 5.0 5.0 5.0 5.0 5.0	5.6 5.0 5.0 5.0 5.0 5.0 5.2



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Commons at Falcon Field 21604-00 KGV TDM El Paso County Preliminary 7/5/2024

RATIONAL METHOD CALCULATIONS FOR STORM WATER RUNOFF

DEVELOPED TIME OF CONCENTRATION

	5	SUB-BASI DATA	N				INITIAL/OVERLAND TIME (t _i)				TRAVEL (t _t)	TIME			PIPE TRA	VEL TIME		TIME OF CO	FINAL	
BASIN	DESIGN PT:	C ₅	C ₁₀₀	AREA	COMP		LENGTH	SLOPE	t,	LENGTH	SLOPE	VEL.	t	LENGTH	SLOPE	VEL.	t.	COMP.	MINIMUM	*0
· · · · ·		Ū	100	Ac			Ft	%	Min	Ft	%	FPS	Min	Ft	%	FPS	Min	tc	tc	Min
C-BASINS																				
OSC1		0.90	0.96	0.37	0.33	0.35	40	2.5	1.7	100	2.0	5.2	0.3					2.1	5.0	5.0
C1		0.90	0.96	0.25	0.23	0.24	40	2.5	1.7	193	2.0	5.2	0.6					2.4	5.0	5.0
OSC1+C1	1	0.90	0.96	0.62	0.56	0.59		From OSC1		185	2.0	5.2	0.5					5.5	5.0	5.5
C2		0.81	0.88	2.26	1.83	1.99	60	3.2	2.9	250	3.0	6.5	0.6					3.5	5.0	5.0
DP1+C2	2	0.83	0.90	2.88	2.39	2.58		From DP1						300	1.0	7.2	0.7	6.2	5.0	6.2
C3	3	0.81	0.88	1.15	0.93	1.01	70	2.6	3.3	300	2.0	5.2	1.0					4.3	5.0	5.0
OSC2		0.32	0.53	1.36	0.43	0.72	50	2.5	7.6	200	2.0	5.2	0.6					5.6	5.0	5.6
C4		0.81	0.88	1.41	1.14	1.24	50	2.5	2.8	350	4.7	7.5	0.8					3.6	5.0	5.0
OSC2+C4	4	0.57	0.71	2.78	1.58	1.96		From OS2		350	4.7	7.5	0.8					6.4	5.0	6.4
C5		0.90	0.96	0.17	0.16	0.17	20	2.0	1.3	450	2.0	5.2	1.4					2.8	5.0	5.0
DP3+C5	5	0.82	0.89	1.32	1.09	1.18		From DP3						20	1.0	7.2	0.0	5.0	5.0	5.0
C6		0.90	0.96	0.18	0.16	0.17	20	2.0	1.3	450	2.0	7.5	1.0					2.3	5.0	5.0
DP5+C6	6	0.83	0.90	1.50	1.25	1.35		From DP5						40	1.0	7.2	0.1	5.1	5.0	5.1
DP2+DP4+DP6	6A	0.73	0.60	7.16	5.21	4.32		From DP2						286	1.0	7.2	0.7	6.9	5.0	6.9
C7	7	0.90	0.96	0.88	0.79	0.85	40	2.0	1.9	750	2.0	5.2	2.4					4.3	5.0	5.0
C8	8	0.90	0.96	0.65	0.59	0.63	40	2.0	1.9	540	2.0	5.2	1.7					3.6	5.0	5.0
DP6A+DP7+DP8	8A	0.76	0.67	8.69	6.59	5.80		From DP6A						270	1.0	7.2	0.6	7.5	5.0	7.5
D-BASINS																				
D1	1	0.36	0.53	1.36	0.49	0.73	100	2.7	10.0	270	2.6	6.0	0.8				1	10.7	5.0	10.7
D2		0.38	0.54	1.95	0.73	1.06	100	2.7	9.7	370	1.2	5.0	1.2					10.9	5.0	10.9
DP1+D2	2	0.37	0.54	3.30	1.22	1.78		From DP1		370	1.2	5.0	1.2					11.9	5.0	11.9
D3	3	0.40	0.56	0.91	0.36	0.50	70	1.2	10.3	500	1.4	5.2	1.6					11.9	5.0	11.9
DP8A(C)+DP2+DP3	3A	0.63	0.63	12.90	8.17	8.08		From DP3						50	1.0	7.2	0.1	12.1	5.0	12.1
D4	4	0.39	0.55	2.75	1.07	1.52	100	2.3	10.2	320	3.3	8.8	0.6					10.8	5.0	10.8
D5		0.55	0.67	0.62	0.34	0.42	50	1.5	6.3	280	1.9	7.2	0.7					7.0	5.0	7.0
DP4+D5	5	0.42	0.58	3.37	1.41	1.94		From DP4		30	1.9	7.2	0.1					10.8	5.0	10.8
D6	6	0.45	0.59	2.68	1.21	1.58	100	2.0	9.6	850	3.2	6.3	2.2					11.9	5.0	11.9
D7		0.50	0.64	0.74	0.37	0.47	20	2.0	4.0	300	3.2	6.3	0.8					4.8	5.0	5.0
DP5+DP6+D7	7	0.44	0.59	6.79	2.99	4.00		From DP6		20	2.0	5.2	0.1					12.0	5.0	12.0
D8	8	0.45	0.59	0.44	0.20	0.26	80	1.5	9.5	150	1.5	5.0	0.5					10.0	5.0	10.0
D9	9	0.34	0.52	0.31	0.11	0.16	80	4.0	8.0	160	5.5	12.2	0.2					8.2	5.0	8.2
D10	10	0.35	0.52	1.34	0.46	0.70	100	2.0	11.2	300	4.5	11.6	0.4					11.6	5.0	11.6
D11		0.90	0.96	0.61	0.55	0.59	20	2.0	1.3	680	4.1	11.6	1.0					2.3	5.0	5.0
DP10+D11	11	0.52	0.66	1.95	1.01	1.29		From DP10		50	1.0	5.0	0.2					11.8	5.0	11.8
D12	10	0.08	0.35	1.51	0.12	0.53	80	25.0	5.8	166	2.0	6.0	0.5					6.3	5.0	6.3
DP3A+DP7+DP8+DP9+DP11+D12	12	0.53	0.60	23.91	12.60	14.32		From DP3A		100	2.0	6.0	0.3	200	1.0	7.2	0.5	12.8	5.0	12.8
OSD1	D1	0.08	0.35	2.70	0.22	0.94	40	2.5	8.9	165	2.0	5.8	0.5					9.4	5.0	9.4
D13	40	0.08	0.35	1.98	0.16	0.69	80	25.0	5.8	1080	2.0	5.8	3.1					8.9	5.0	8.9
DPD1+D13	13	0.08	0.35	4.68	0.37	1.64		From OSD1		330	2.0	6.0	0.9					9.9	5.0	9.9
D14		0.08	0.35	0.76	0.06	0.27	80	15.0	6.9	50	2.0	5.8	0.1					7.1	5.0	7.1



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DEVELOPED	RUNOFF		5	P1=	1.50		
			DIRECT RUNC	DFF			
BASIN (S)	DESIGN POINT	AREA (AC)	RUNOFF COEFF	t _c (MIN)	C * A	I (IN/HR)	Q (CFS)
		A-BASIN				-	
OSA		16.62	0.20	19.3	3.40	3.14	10.7
A1	1	0.74	0.87	5.0	0.65	5.17	3.3
A2		1.52	0.37	5.0	0.56	5.16	2.9
DP1+A2	2	2.27	0.53	5.2	1.21	5.11	6.2
A3	3	1.48	0.43	6.6	0.64	4.75	3.0
A4	4	2.87	0.43	6.3	1.24	4.81	6.0
A5		1.47	0.52	6.2	0.77	4.86	3.7
DP4+DP5	5	4.34	0.46	8.5	2.01	4.37	8.8
A6	6	3.30	0.46	14.3	1.50	3.60	5.4
DP5+DP6	6A	7.64	0.46	14.3	3.51	3.59	12.6
A7	7	1.76	0.45	12.3	0.79	3.81	3.0
A8	8	0.65	0.45	7.1	0.29	4.64	1.4
A9		2.56	0.48	6.5	1.24	4.78	5.9
DP7+DP8+A9	9	4.97	0.47	13.0	2.33	3.74	8.7
A10		1.10	0.45	10.0	0.49	4.13	2.0
DP3+A10	10	2.57	0.44	10.0	1.13	4.13	4.7
DP6A+DP9+DP10	10A	15.18	0.46	15.0	6.97	3.52	24.5
A11		1.07	0.08	15.5	0.09	3.48	0.3
DP2+DP10A+A11	11	18.51	0.45	6.6	8.26	4.75	39.2
A12		1.32	0.12	20.9	0.15	3.02	0.5
OSA+A12	12	17.94	0.20	27.3	3.56	2.62	9.3
A13	13	1.20	0.08	5.0	0.10	5.17	0.5
RET090 (DBPS)							36.0
A14		0.61	0.08	8.0	0.05	4.46	0.2
POND A OUTFALL							0.5
RET090+POND A+POND B+A14	14						37.2
B-BASINS							
OSB1		0.83	0.88	5.0	0.74	5.17	3.8
OSB2		0.32	0.90	5.0	0.29	5.17	1.5
OSB3		0.56	0.90	5.0	0.50	5.17	2.6
B1		1.99	0.81	5.0	1.61	5.17	8.3
OSB1+B1	1	2.82	0.83	5.8	2.35	4.96	11.6
B2		1.11	0.81	5.0	0.90	5.17	4.7
OSB2+B2	2	1.44	0.83	5.5	1.19	5.03	6.0

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DEVELOPED	RUNOFF			YR	STORM	P1=	1.50
			DIRECT RUNC	DFF			
BASIN (S)	DESIGN POINT	AREA (AC)	RUNOFF COEFF	t _c (MIN)	C * A	I (IN/HR)	Q (CFS)
B3	3	0.35	0.90	5.0	0.32	5.17	1.6
B4		1.53	0.81	5.0	1.24	5.17	6.4
OSB3+B4	4	2.09	0.83	5.8	1.75	4.93	8.6
DP3+DP4	4A	2.44	0.84	5.8	2.06	4.93	10.2
DP1+DP2+DP4A	4B	6.70	0.84	6.2	5.60	4.84	27.1
B5	5	0.25	0.90	5.0	0.23	5.17	1.2
B6		0.37	0.90	5.0	0.33	5.17	1.7
DP5+B6	6	0.62	0.90	5.1	0.56	5.15	2.9
B7		1.97	0.81	5.0	1.59	5.17	8.2
DP4B+DP6+B7	7	9.29	0.83	5.6	7.75	5.00	38.8
B8	8	1.52	0.81	5.0	1.23	5.17	6.4
B9		0.89	0.90	5.0	0.80	5.17	4.1
DP8+B9	9	2.41	0.84	5.0	2.03	5.16	10.5
B10		0.71	0.90	5.0	0.64	5.17	3.3
DP9+B10	10	3.12	0.86	5.2	2.67	5.12	13.7
DP7+DP10	10A	12.41	0.84	5.8	10.42	4.95	51.6
B11		1.14	0.08	5.0	0.09	5.17	0.5
DP10A+B11	11	13.55	0.78	6.0	10.51	4.90	51.6
POND B OUTFALL							0.5
C-BASINS	-		•			•	
OSC1		0.37	0.90	5.0	0.33	5.17	1.7
C1		0.25	0.90	5.0	0.23	5.17	1.2
OSC1+C1	1	0.62	0.90	5.5	0.56	5.03	2.8
C2		2.26	0.81	5.0	1.83	5.17	9.4
DP1+C2	2	2.88	0.83	6.2	2.39	4.85	11.6
C3	3	1.15	0.81	5.0	0.93	5.17	4.8
OSC2		1.36	0.32	5.6	0.43	4.99	2.2
C4		1.41	0.81	5.0	1.14	5.17	5.9
OSC2+C4	4	2.78	0.57	6.4	1.58	4.79	7.6
C5		0.17	0.90	5.0	0.16	5.17	0.8
DP3+C5	5	1.32	0.82	5.0	1.09	5.16	5.6
C6		0.18	0.90	5.0	0.16	5.17	0.8
DP5+C6	6	1.50	0.83	5.1	1.25	5.13	6.4
DP2+DP4+DP6	6A	7.16	0.73	6.9	5.21	4.70	24.5

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DEVELOPED	RUNOFF			5 YR		P1=	1.50	
			DIRECT RUNC	DFF				
BASIN (S)	DESIGN POINT	AREA (AC)	RUNOFF COEFF	t _c (MIN)	C * A	I (IN/HR)	Q (CFS)	
C7	7	0.88	0.90	5.0	0.79	5.17	4.1	
C8	8	0.65	0.90	5.0	0.59	5.17	3.0	
DP6A+DP7+DP8	8A	8.69	0.76	7.5	6.59	4.56	30.1	
D-BASINS								
D1	1	1.36	0.36	10.7	0.49	4.03	2.0	
D2		1.95	0.38	10.9	0.73	3.99	2.9	
DP1+D2	2	3.30	0.37	11.9	1.22	3.86	4.7	
D3	3	0.91	0.40	11.9	0.36	3.86	1.4	
DP8A(C)+DP2+DP3	3A	12.90	0.63	12.1	8.17	3.85	31.5	
D4	4	2.75	0.39	10.8	1.07	4.02	4.3	
D5		0.62	0.55	7.0	0.34	4.67	1.6	
DP4+D5	5	3.37	0.42	10.8	1.41	4.01	5.6	
D6	6	2.68	0.45	11.9	1.21	3.87	4.7	
D7		0.74	0.50	5.0	0.37	5.17	1.9	
DP5+DP6+D7	7	6.79	0.44	12.0	2.99	3.86	11.5	
D8	8	0.44	0.45	10.0	0.20	4.13	0.8	
D9	9	0.31	0.34	8.2	0.11	4.42	0.5	
D10	10	1.34	0.35	11.6	0.46	3.90	1.8	
D11		0.61	0.90	5.0	0.55	5.17	2.9	
DP10+D11	11	1.95	0.52	11.8	1.01	3.88	3.9	
D12		1.51	0.08	6.3	0.12	4.82	0.6	
DP3A+DP7+DP8+DP9+DP11+D12	12	23.91	0.53	12.8	12.60	3.76	47.4	
OSD1	D1	2.70	0.08	9.4	0.22	4.23	0.9	
D13		1.98	0.08	8.9	0.16	4.30	0.7	
DPD1+D13	13	4.68	0.08	9.9	0.37	4.15	1.6	
D14		0.76	0.08	7.1	0.06	4.65	0.3	
POND C OUTFALL							0.7	
POND C +D14	14						1.0	

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DEVELOPED	RUNOFF		100	YR	STORM	P1=	2.52
			DIRECT RUNC	DFF			
BASIN (S)	DESIGN POINT	AREA (AC)	RUNOFF COEFF	t _c (MIN)	C * A	I (IN/HR)	Q (CFS)
		A-BASI	NS				
OSA	0	16.62	0.44	19.3	7.35	5.28	38.8
A1	1	0.74	0.93	5.0	0.69	8.68	6.0
A2	0	1.52	0.56	5.0	0.85	8.66	7.4
DP1+A2	2	2.27	0.68	5.2	1.54	8.58	13.2
A3	3	1.48	0.59	6.6	0.87	7.98	7.0
A4	4	2.87	0.59	6.3	1.70	8.08	13.7
A5	0	1.47	0.65	6.2	0.95	8.16	7.8
DP4+DP5	5	4.34	0.61	8.5	2.65	7.34	19.5
A6	6	3.30	0.59	14.3	1.96	6.04	11.8
DP5+DP6	6A	7.64	0.60	14.3	4.61	6.03	27.8
A7	7	1.76	0.59	12.3	1.04	6.40	6.6
A8	8	0.65	0.59	7.1	0.38	7.79	3.0
A9	0	2.56	0.62	6.5	1.58	8.02	12.7
DP7+DP8+A9	9	4.97	0.60	13.0	3.01	6.27	18.9
A10	0	1.10	0.59	10.0	0.65	6.94	4.5
DP3+A10	10	2.57	0.59	10.0	1.52	6.94	10.6
DP6A+DP9+DP10	10A	15.18	0.60	15.0	9.14	5.91	54.0
A11	0	1.07	0.35	15.5	0.37	5.84	2.2
DP2+DP10A+A11	11	18.51	0.60	6.6	11.05	7.98	88.2
A12	0	1.32	0.38	20.9	0.50	5.08	2.5
OSA+A12	12	17.94	0.44	27.3	7.84	4.40	34.5
A13	13	1.20	0.35	5.0	0.42	8.68	3.6
RET090 (DBPS)							320.0
A14	0	0.61	0.35	8.0	0.21	7.49	1.6
POND A OUTFALL							12.7
RET090+POND A+POND B+A14	14						344.1
B-BASINS	<u> </u>		<u> </u>		_		
OSB1	0	0.83	0.95	5.0	0.79	8.68	6.8
OSB2	0	0.32	0.96	5.0	0.31	8.68	2.7
OSB3	0	0.56	0.96	5.0	0.54	8.68	4.7
B1	0	1.99	0.88	5.0	1.75	8.68	15.2
OSB1+B1	1	2.82	0.90	5.8	2.54	8.32	21.1
B2	0	1.11	0.88	5.0	0.98	8.68	8.5

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DEVELOPED	RUNOFF		100	YR	STORM	P1=	2.52	
			DIRECT RUNG	DFF				
BASIN (S)	DESIGN POINT	AREA (AC)	RUNOFF COEFF	t _c (MIN)	C * A	I (IN/HR)	Q (CFS)	
OSB2+B2	2	1.44	0.90	5.5	1.29	8.45	10.9	
B3	3	0.35	0.96	5.0	0.34	8.68	2.9	
B4	0	1.53	0.88	5.0	1.35	8.68	11.7	
OSB3+B4	4	2.09	0.90	5.8	1.89	8.28	15.6	
DP3+DP4	4A	2.44	0.91	5.8	2.22	8.28	18.4	
DP1+DP2+DP4A	4B	6.70	0.90	6.2	6.05	8.13	49.2	
B5	5	0.25	0.96	5.0	0.24	8.68	2.1	
B6	0	0.37	0.96	5.0	0.36	8.68	3.1	
DP5+B6	6	0.62	0.96	5.1	0.60	8.64	5.2	
B7	0	1.97	0.88	5.0	1.73	8.68	15.0	
DP4B+DP6+B7	7	9.29	0.90	5.6	8.38	8.40	70.4	
B8	8	1.52	0.88	5.0	1.34	8.68	11.6	
B9	0	0.89	0.96	5.0	0.85	8.68	7.4	
DP8+B9	9	2.41	0.91	5.0	2.19	8.66	19.0	
B10	0	0.71	0.96	5.0	0.68	8.68	5.9	
DP9+B10	10	3.12	0.92	5.2	2.87	8.60	24.7	
DP7+DP10	10A	12.41	0.91	5.8	11.25	8.31	93.5	
B11	0	1.14	0.35	5.0	0.40	8.68	3.5	
DP10A+B11	11	13.55	0.86	6.0	11.65	8.24	95.9	
POND B OUTFALL							9.8	
C-BASINS								
OSC1		0.37	0.96	5.0	0.35	8.68	3.1	
C1		0.25	0.96	5.0	0.24	8.68	2.1	
OSC1+C1	1	0.62	0.96	5.5	0.59	8.44	5.0	
C2		2.26	0.88	5.0	1.99	8.68	17.2	
DP1+C2	2	2.88	0.90	6.2	2.58	8.14	21.0	
C3	3	1.15	0.88	5.0	1.01	8.68	8.8	
OSC2		1.36	0.53	5.6	0.72	8.38	6.0	
C4		1.41	0.88	5.0	1.24	8.68	10.8	
OSC2+C4	4	2.78	0.71	6.4	1.96	8.05	15.8	
C5		0.17	0.96	5.0	0.17	8.68	1.5	
DP3+C5	5	1.32	0.89	5.0	1.18	8.66	10.2	
C6		0.18	0.96	5.0	0.17	8.68	1.5	

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DEVELOPED	RUNOFF		100 YR			P1=	2.52	
			DIRECT RUNC	DFF				
BASIN (S)	DESIGN POINT	AREA (AC)	RUNOFF COEFF	t _c (MIN)	C * A	I (IN/HR)	Q (CFS)	
DP5+C6	6	1.50	0.90	5.1	1.35	8.61	11.6	
DP2+DP4+DP6	6A	7.16	0.60	6.9	4.32	7.88	34.1	
C7	7	0.88	0.96	5.0	0.85	8.68	7.4	
C8	8	0.65	0.96	5.0	0.63	8.68	5.4	
DP6A+DP7+DP8	8A	8.69	0.67	7.5	5.80	7.66	44.4	
D-BASINS								
D1	1	1.36	0.53	10.7	0.73	6.76	4.9	
D2		1.95	0.54	10.9	1.06	6.71	7.1	
DP1+D2	2	3.30	0.54	11.9	1.78	6.48	11.6	
D3	3	0.91	0.56	11.9	0.50	6.48	3.3	
DP8A(C)+DP2+DP3	3A	12.90	0.63	12.1	8.08	6.46	52.2	
D4	4	2.75	0.55	10.8	1.52	6.74	10.3	
D5		0.62	0.67	7.0	0.42	7.84	3.3	
DP4+D5	5	3.37	0.58	10.8	1.94	6.73	13.1	
D6	6	2.68	0.59	11.9	1.58	6.49	10.3	
D7		0.74	0.64	5.0	0.47	8.68	4.1	
DP5+DP6+D7	7	6.79	0.59	12.0	4.00	6.48	25.9	
D8	8	0.44	0.59	10.0	0.26	6.93	1.8	
D9	9	0.31	0.52	8.2	0.16	7.42	1.2	
D10	10	1.34	0.52	11.6	0.70	6.55	4.6	
D11		0.61	0.96	5.0	0.59	8.68	5.1	
DP10+D11	11	1.95	0.66	11.8	1.29	6.52	8.4	
D12		1.51	0.35	6.3	0.53	8.10	4.3	
DP3A+DP7+DP8+DP9+DP11+D12	12	23.91	0.60	12.8	14.32	6.31	90.4	
OSD1	D1	2.70	0.35	9.4	0.94	7.10	6.7	
D13		1.98	0.35	8.9	0.69	7.22	5.0	
DPD1+D13	13	4.68	0.35	9.9	1.64	6.97	11.4	
D14		0.76	0.35	7.1	0.27	7.81	2.1	
POND C OUTFALL							21.1	
POND C +D14	14						23.2	

Hydraulic Calculations

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

	Project: The Commons at Falcon Field	
	Basin ID: Pond A	
	ZONE 3 2001 2 2001 2	
POOL	Example Zone Configuration (Retention Pond)	

Watershed Information

ceronea información		
Selected BMP Type =	EDB	
Watershed Area =	18.51	acres
Watershed Length =	1,191	ft
Watershed Length to Centroid =	550	ft
Watershed Slope =	0.025	ft/ft
Watershed Imperviousness =	59.00%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

	5		Optional L
Water Quality Capture Volume (WQCV) =	0.359	acre-feet	
Excess Urban Runoff Volume (EURV) =	1.319	acre-feet	
2-yr Runoff Volume (P1 = 1.19 in.) =	0.953	acre-feet	1.19
5-yr Runoff Volume (P1 = 1.5 in.) =	1.257	acre-feet	1.50
10-yr Runoff Volume (P1 = 1.75 in.) =	1.500	acre-feet	1.75
25-yr Runoff Volume (P1 = 2 in.) =	1.836	acre-feet	2.00
50-yr Runoff Volume (P1 = 2.25 in.) =	2.167	acre-feet	2.25
100-yr Runoff Volume (P1 = 2.52 in.) =	2.576	acre-feet	2.52
500-yr Runoff Volume (P1 = 3.49 in.) =	3.996	acre-feet	3.49
Approximate 2-yr Detention Volume =	0.854	acre-feet	
Approximate 5-yr Detention Volume =	1.120	acre-feet	
Approximate 10-yr Detention Volume =	1.356	acre-feet	
Approximate 25-yr Detention Volume =	1.642	acre-feet	
Approximate 50-yr Detention Volume =	1.817	acre-feet	
Approximate 100-yr Detention Volume =	2.010	acre-feet	

Define Zones and Basin Geometry

enne zones and basin deonned y		
Zone 1 Volume (WQCV) =	0.359	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.960	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.691	acre-feet
Total Detention Basin Volume =	2.010	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth $(H_{total}) =$	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S _{TC}) =	user	ft/ft
Slopes of Main Basin Sides (S _{main}) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	
Initial Surcharge Area $(A_{ISV}) =$	user	ft ²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor (W_{FLOOR}) =	user	ft
Area of Basin Floor (A _{FLOOR}) =	user	ft ²
Volume of Basin Floor (V_{FLOOR}) =	user	ft ³
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft ²
Volume of Main Basin (V_{MAIN}) =	user	ft ³
		1

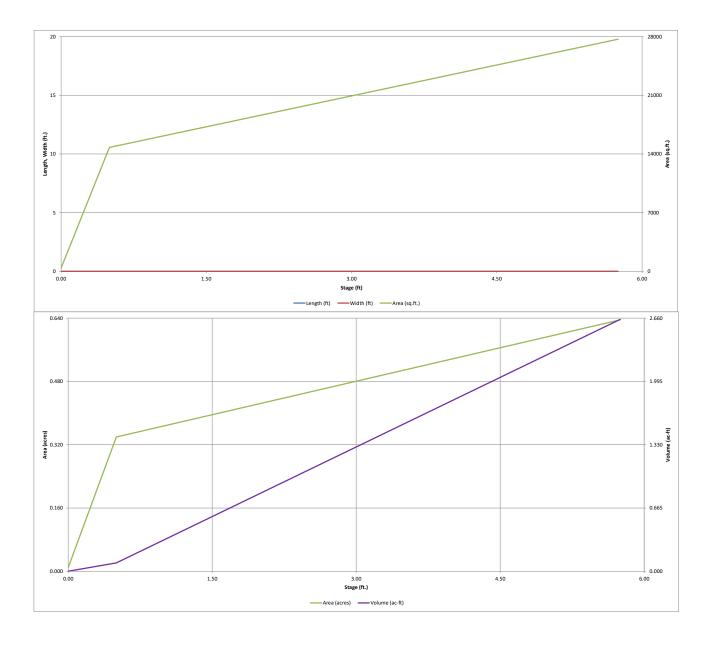
Calculated Total Basin Volume (V_{total}) = user

ft 2 ft³ acre-feet

		Optional				Optional			
Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
Description	(ft)	Stage (ft) 0.00	(ft)	(ft)	(ft ²)	Area (ft ²) 400	(acre) 0.009	(ft 3)	(ac-ft)
Top of Micropool								2 707	0.097
6828		0.50				14,788	0.339	3,797	0.087
6835.75		5.75				27,694	0.636	115,312	2.647
	-								
								1	
								<u> </u>	
								1	

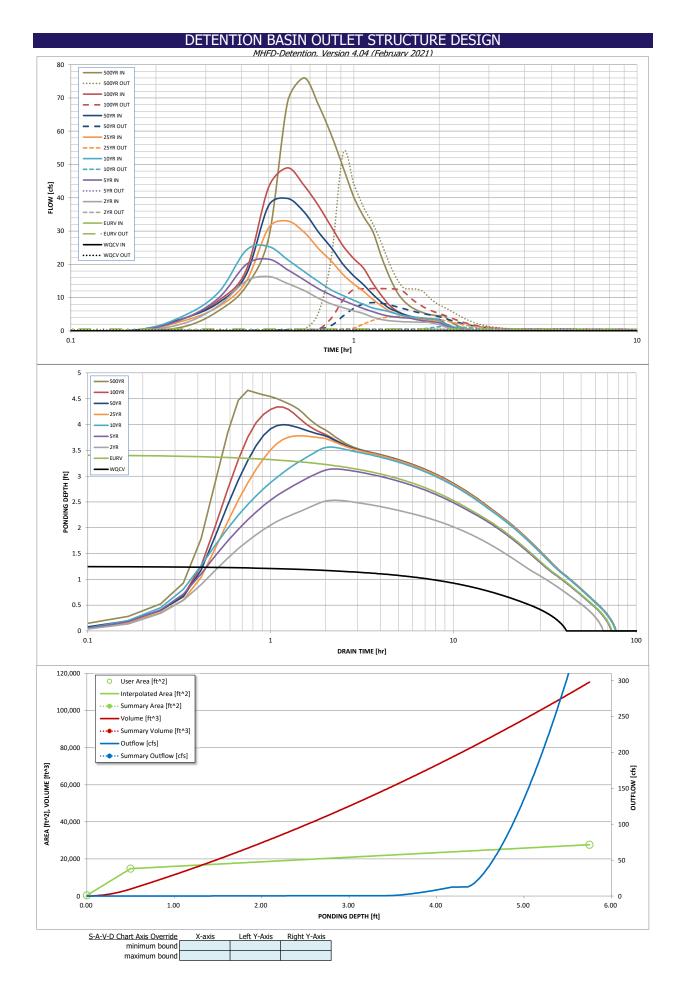
DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



DETENTION BASIN OUTLET STRUCTURE DESIGN

Description Description Secretion Secretion Secretion Secretion Description	Project:	The Commons at l		FD-Detention, Vers	sion 4.04 (Februar	ry 2021)				
Image: difference of the set of the difference of the differenc	-									
Image: Start and Start an	ZONE 3 ZONE 2 ZONE 1						Outlet Type			
Description Description <thdescription< th=""> <thdescription< th=""></thdescription<></thdescription<>				Zone 1 (WQCV)		, ,	1]		
Description Description <thdescription< th=""> <thdescription< th=""></thdescription<></thdescription<>		100-YEAR ORIFICE		Zone 2 (EURV)	3.42	0.960	Orifice Plate]		
Line Long. Line Long. Line Line Line Line Line Line Line Line	PERMANENT ORIFICES	Configuration (Re	tention Pond)	Zone 3 (100-year)			Weir&Pipe (Restrict)			
Understand on the function of basis Index does under basis Index does		•		MD)	Total (all zones)	2.010		Calculated Parame	ters for Underdrain	
Upper legit: Orfice Patte with eine or more stress or Illighted Streeweit busis bottom at Stage = 0 f) Upper at tig of 2 manage of the stress bottom at Stage = 0 f) Upper at tig of 2 manage of the stress bottom at Stage = 0 f) Upper at tig of 2 manage of the stress bottom at Stage = 0 f) Upper at tig of 2 manage of the stress bottom at Stage = 0 f) Upper at tig of 2 manage of the stress bottom at Stage = 0 f) Upper at tig of 2 manage of the stress bottom at Stage = 0 f) Upper at tig of 2 manage of the stress bottom at Stage = 0 f) Upper at tig of 2 manage of the stress bottom at Stage = 0 f) Upper at tig of 2 manage of the stress bottom at Stage = 0 f) Upper at tig of 2 manage of the stress bottom at Stage = 0 f) Upper at tig of 2 manage of the stress bottom at Stage = 0 f) Upper at tig of 2 manage of the stress bottom at Stage = 0 f) Upper at tig of 2 manage of the stress bottom at Stage = 0 f) Upper at tig of 2 manage of the stress bottom at Stage = 0 f) Vertical Office Areas refere Upper at tig of 2 manage of the stress bottom at Stage = 0 f) Vertical Office Areas refere Upper at tig of 2 manage of the stress bottom at Stage = 0 f) Vertical Office Areas refere Vertical Office Ar		í	i		surface)	Underd	drain Orifice Area =		1	
Inter of Locate Diffice 0.00 0 (1) (delate be bash lottion af Stage = 0.1) WD Office Area protect 278-50 1'r Diffice Area protecting Units Area protecting Starting - 1 3.36 ML, Include ML A Net Diffice Area protecting Units Area protecting Starting - 1 3.36 ML, Include Starting Area NL A Net Units Area protecting Ar	Underdrain Orifice Diameter =		inches			Underdrain	Orifice Centroid =		feet	
Inter of Locate Diffice 0.00 0 (1) (delate be bash lottion af Stage = 0.1) WD Office Area protect 278-50 1'r Diffice Area protecting Units Area protecting Starting - 1 3.36 ML, Include ML A Net Diffice Area protecting Units Area protecting Starting - 1 3.36 ML, Include Starting Area NL A Net Units Area protecting Ar	User Input: Orifice Plate with one or more orific	res or Elliptical Slot	Weir (typically used	to drain WOCV and	1/or FLIRV in a sed	imentation BMP)		Calculated Parame	ters for Plate	
Diffice Future Diffice Future NA Test Uptice Future Diffice Future NA Test Uptice Future Stage and Toda Asia of Each Office Rev 1 (spaces) Rev 5 (spaces) Rev 6 (spaces) Rev 7 (spaces) Rev 6 (spaces)			1				ice Area per Row =	C		
Other Piete: Other Area per Rov = 3.88 sp. inches (use rectangular openings) Bigiptal So Area = NA n° User Inndi: State and Tota Area of Each Orline Row (numbered from Isoveit to Registra) Rev 2 (optensi) Rev 7 (optensi) Rev 15 (optensi) Rev 16			+ `	<pre>bottom at Stage =</pre>	0 ft)				•	
List: The set of circle criteria (train from from from from from from from from			•	tangular openings)		•				
Bur Bur Stoppe of Online Area (day result) Box 3 (gatowa) Box 5 (gatowa) Box 5 (gatowa) Box 7 (gatowa) Box 6 (gatowa) Box 8 (gatowa) Box 16 (gatowa)	onnee Hate. Onnee Area per Now -	5.50	lad. menes (use ree			L		IN/A	lic	
Buge of Orline Centrol (No. 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0,										
Stoge of Online Control (b) 0.00 1.14 2.28 1.00 1.00 1.00 1.00 Stoge of Online Control (b) 569 1.08 3.08 1	User Input: Stage and Total Area of Each Orific				Row 4 (antional)	Dow E (optional)	Dow 6 (optional)	Dow 7 (optional)	Dow 9 (optional)	1
Onfor any Op. Install. 3.98 3.98 Image: 10 (distant) Rev: 12 (dis	Stage of Orifice Centroid (ft)				Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	
Stope of othic Carried (th) Instantion Instantion Instantion User Input: Vertical Office (Circular or Retrangular) Not Selected Selected Not Selected Not Selected Selected Not Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected S										
Stope of othic Carried (th) Instantion Instantion Instantion User Input: Vertical Office (Circular or Retrangular) Not Selected Selected Not Selected Not Selected Selected Not Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected Selected Not Selected S										1
Ortice Area (a, inches) Aussister User Input: Vertical Orfice (Crucier or Restance) No.4 No.4 <td< td=""><td>Chana of Ovifica Controld (A)</td><td></td><td>Row 10 (optional)</td><td>Row 11 (optional)</td><td>Row 12 (optional)</td><td>Row 13 (optional)</td><td>Row 14 (optional)</td><td>Row 15 (optional)</td><td>Row 16 (optional)</td><td></td></td<>	Chana of Ovifica Controld (A)		Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	
User Input: Vertical Onfree (Grader or Rectangular) Not Selected Not										
Insert of Vertical Orifice in the selected in the Selected in Na N			1	1		1	1	<u>.</u>	ł	
Linvert of Vertical Onfries N/A N/A<	User Input: Vertical Orifice (Circular or Rectang			1				r		fice
Depth at top of Zone using Vertical Onfice E NA N	Invert of Vertical Orifice –	-		ft (relative to basin	bottom at Stage -	-0ft) Ver	tical Orifice Area –			ft ²
Vertical Onfice Dameter N/A N/A N/A Inches User Input: Overflow Weir (Comptox with Flat or: Sogned Grate and Outlet Pipe OR Rectangular/Tragezoidal Weir (and No Outlet Pipe). Calculated Parameters for Overflow Weir Sone Edge Height, ho 2.06 N/A freet Overflow Weir Front Edge Height, ho 2.05 N/A freet 0.06 N/A freet Overflow Weir Front Edge Height, Ho 2.00 N/A freet 0.00 N/A freet Overflow Weir Grate Space 0.00 N/A freet 0.00 N/A freet Overflow Weir Grate Type : 0.00 N/A freet 0.00 N/A freet Overflow Grate Open Area (100-Profile Area is 2.00 N/A freet 0.00 N/A freet Overflow Grate Open Area (100-Profile Area is 0.00 N/A freet 0.00 N/A freet Outlet Pipe area 0.00 N/A freet 0.01 0.01 0.01 0.01 N/A freet Bept to Invert of Outlet Pipe area 0.000 N/A				•	-	,				1
Zoneflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Largth = Overflow Weir Front Edge Largth = Horiz, Largth of Wer Stele = 0.00 N/A freet feet Concertow Weir Stope Largth = Horiz, Largth of Wer Stele = 0.00 Zone 3 Weir NA Not Selected 3.00 N/A freet feet Overflow Weir Stope Largth = Horiz, Largth of Wer Stele = 0.00 Zone 3 Weir NA Not Selected 3.00 N/A freet feet Overflow Grate Open Area v/Debris = 0.20 Zone 3 Weir 4.53 N/A freet feet Overflow Grate Type = Horiz, Largth of Wer Stele = 0.00 N/A freet Overflow Grate Open Area v/Debris = 3.13 N/A freet Overflow Grate Type = Horiz, Largth of Wer Stele = 0.00 N/A freet Overflow Grate Open Area v/Debris = 3.13 N/A freet User Input: Outlet Pipe w/ Flow Restriction Plate, Circular Orffice, Restrictor Plate, or Sected 0.00 N/A freet Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate 2.03 N/A freet Base Induct The Weir Stape = 13.00 inches Half-Central Angle of Restrictor Plate on Pipe = 2.03 N/A freet Spliway Intert Stape Spliway Creat Length = Spliway Edsopes = 1.00 feet The Laser can override the default CLIPP hydrographs and numbri volume at Top of Freeboard = 2.61 2.61 acreft					j-			.,	.,	
Zoneflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Largth = Overflow Weir Front Edge Largth = Horiz, Largth of Wer Stele = 0.00 N/A freet feet Concertow Weir Stope Largth = Horiz, Largth of Wer Stele = 0.00 Zone 3 Weir NA Not Selected 3.00 N/A freet feet Overflow Weir Stope Largth = Horiz, Largth of Wer Stele = 0.00 Zone 3 Weir NA Not Selected 3.00 N/A freet feet Overflow Grate Open Area v/Debris = 0.20 Zone 3 Weir 4.53 N/A freet feet Overflow Grate Type = Horiz, Largth of Wer Stele = 0.00 N/A freet Overflow Grate Open Area v/Debris = 3.13 N/A freet Overflow Grate Type = Horiz, Largth of Wer Stele = 0.00 N/A freet Overflow Grate Open Area v/Debris = 3.13 N/A freet User Input: Outlet Pipe w/ Flow Restriction Plate, Circular Orffice, Restrictor Plate, or Sected 0.00 N/A freet Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate 2.03 N/A freet Base Induct The Weir Stape = 13.00 inches Half-Central Angle of Restrictor Plate on Pipe = 2.03 N/A freet Spliway Intert Stape Spliway Creat Length = Spliway Edsopes = 1.00 feet The Laser can override the default CLIPP hydrographs and numbri volume at Top of Freeboard = 2.61 2.61 acreft										
Zoneflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Largth = Overflow Weir Front Edge Largth = Horiz, Largth of Wer Stele = 0.00 N/A freet feet Concertow Weir Stope Largth = Horiz, Largth of Wer Stele = 0.00 Zone 3 Weir NA Not Selected 3.00 N/A freet feet Overflow Weir Stope Largth = Horiz, Largth of Wer Stele = 0.00 Zone 3 Weir NA Not Selected 3.00 N/A freet feet Overflow Grate Open Area v/Debris = 0.20 Zone 3 Weir 4.53 N/A freet feet Overflow Grate Type = Horiz, Largth of Wer Stele = 0.00 N/A freet Overflow Grate Open Area v/Debris = 3.13 N/A freet Overflow Grate Type = Horiz, Largth of Wer Stele = 0.00 N/A freet Overflow Grate Open Area v/Debris = 3.13 N/A freet User Input: Outlet Pipe w/ Flow Restriction Plate, Circular Orffice, Restrictor Plate, or Sected 0.00 N/A freet Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate 2.03 N/A freet Base Induct The Weir Stape = 13.00 inches Half-Central Angle of Restrictor Plate on Pipe = 2.03 N/A freet Spliway Intert Stape Spliway Creat Length = Spliway Edsopes = 1.00 feet The Laser can override the default CLIPP hydrographs and numbri volume at Top of Freeboard = 2.61 2.61 acreft										
Overflow Weir Front Edge Height, Ho 3.45 N/A ft relative to basin bottom at Stage = 0.1 Height of Grate Upper Edge, H ₌ 3.45 N/A feet Overflow Weir Front Edge Length = 3.00 N/A feet 3.00 N/A feet Overflow Weir Fort Edge Length = 3.00 N/A feet Overflow Grate Open Area / 100-/r Onfice Area 6.26 N/A feet Overflow Grate Digen Area 700 Press 50% N/A feet Overflow Grate Open Area / 100-/r Onfice Area 6.26 N/A feet Overflow Grate Digen Area 700 Overflow Grate Open Area // Debris 3.10 N/A feet Overflow Grate Digen Area 700 Overflow Grate Open Area // Debris 3.10 N/A feet Overflow Grate Digen Area 700 Feet Overflow Grate Open Area // Debris 2.01 N/A feet Debris Cloggin 9% 700 Feet Overflow Grate Dep Area 2.02 N/A feet Restrictor Plate Direct of Dife. Area 13.00 N/A feet Signitwary Design flow Dept	User Input: Overflow Weir (Dropbox with Flat o			<u>tangular/Trapezoid</u> 1	al Weir (and No Ou	<u>itlet Pipe)</u>		r		l <u>eir</u>
Overflow Weir Front Edge Length 3.00 NA feet Overflow Weir Stope Length 3.00 NA feet Overflow Weir Stope Length 3.00 N/A feet Overflow Weir Stope Length 4.58 N/A feet Overflow Grate Type 3.00 N/A feet Overflow Grate Open Area 100 / Overflow Grate Open Area 100 / Overflow Grate Open Area w/Debris 6.26 N/A ft ² User Input: Outlet Pipe w/ Flow Restricton Plate (Circular Orffice, Restrictor Plate, or Rectangular Orffice) Calculated Parameters for Outlet Pipe w/ Flow Restricton Plate 700 / 7	Overflow Weir Front Edge Height Ho -	-		ft (relative to basin h	ottom at Stage – 0 f	Height of Grate	e Upper Edge H. =			feet
Horz. Length of Weir Sides = Deris Cigning %=3.00N/A Type C Gratefeet N/A %Overflow Grate Open Area w/o Debris = 6.26 N/A n/A t^2 transmissionUser Input: Outlet Pipe w/ Flow Restriction Plate Deptis 10 rivert of Outlet Pipe aneter = 0.00 50% N/A N/A $\%$ 7 20% 7				1	ottom ut Stuge – o i					
Overflow Grate Type = Debris Clogging * Type C Grate N/A N/A User Input: Outlet Pipe w/ Flow Restriction Plate, Circular Orifice, Restrictor Plate, or Rectangular Orifice) Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate Zone 3 Restrictor NA nt User Input: Outlet Pipe w/ Flow Restriction Plate Cone 3 Restrictor Not Selected 0.00 NVA ft ² Detty to Invert of Outlet Pipe pameter = 0.00 NVA ft (distance below basin bottom at Stage = 0 ft) Outlet Orifice Area = 1.37 N/A ft ² Outlet Pipe w/ Flow Restrictor Plate to Stage = 1.30 inches Half-Central Angle of Restrictor Plate on Pipe = 2.03 N/A rdei User Input: Emergency Sollway (Rectangular or Trapezoidal) inches Fall-Central Angle of Restrictor Plate on Pipe = 0.03 N/A rdei Spillway Crest Length = 15.00 feet 75.00 feet 5.00 ect 5.00 feet 5.00 feet	Overflow Weir Grate Slope =	0.00	N/A	H:V	Gr	rate Open Area / 10	0-yr Orifice Area =	4.58	N/A	
Debris Clogging % =SomN/A%User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Onfice, Restrictor Not Selected)Calculated Parameters for Outlet Pipe w/ Flow Restriction PlateCone 3 Restrictor Not SelectedCalculated Parameters for Outlet Pipe w/ Flow Restriction PlateOutlet Pipe Diameter =Outlet Onfice, Restrictor Not SelectedCalculated Parameters for Outlet Pipe w/ Flow Restriction Plate Height Above Pipe Invert =Cane 3 Restrictor Not SelectedOutlet Onfice Centroid =Cone 3 Restrictor Not SelectedSelivay Intert Stage 1 A35ft (relative to basin bottom at Stage = 0 ft)Spilivay Design Flow DepterColspan="2">Colspan="2">Collated Parameters for SpilivaySpilivay Crest Length =Spilivay Inter Stage 1 Top of Freeboard =Spilivay Crest Length =Spilivay Crest Length =Spilivay Crest Centroid =Colspan= 500 YourCollated Hydrograph ResultThe user can override the default CUHP hydrographs and runoff volumes to pot Freeboard =Colspan= 500 YourCols	-		,	feet					,	
User Link Calculated Parameters for Outlet Pipe w/ How Restriction Plate Concent of Concent			-	0/	C	Overflow Grate Oper	n Area w/ Debris =	3.13	N/A	ft²
Depth to Invert of Outlet Pipe Outlet Pipe Diametre Restrictor Plate Height Above Pipe Invert = Zone 3 Restrictor 0.00 N/A ft (distance below basin bottom at Stage = 0 ft) 3.00 Outlet Orifice Centrol = 0.000 Zone 3 Restrictor N/A N/A ft (distance below basin bottom at Stage = 0 ft) 3.00 Outlet Orifice Centrol = 0.00 Zone 3 Restrictor N/A N/A ft (relative to basin bottom at Stage = 0 ft) Spillway Crest Length Spillway Crest Length Spillway Crest Length Spillway Crest Length Spillway Crest Length Spillway Crest Length Calculated Parameters for Spillway Education Spillway Crest Length Spillway Crest Length Spillway Crest Length Spillway Education Calculated Parameters for Spillway Education Spillway Crest Length Spillway Crest Length Spillway Crest Length Spillway Crest Length Spillway Crest Length Spillway Length Spillway Crest Spillway Crest Crest Spillway Crest Spillway Crest Spillway Crest Spillway Crest Spillway Crest Spillway Crest Spillway Crest Spillway Crest Crest Spillway Crest Spillway Crest Spillway Crest Spillway Cres	Debris clogging % =	50%	IN/A	90						
Depth to Invert of Outlet Pipe 0.00 N/A ft (distance below basin bottom at Stage = 0 ft) Outlet Orifice Area = 0.60 N/A ft ² Restrictor Plate Height Above Pipe Invert = 18.00 N/A inches Dullet Orifice Centrola 0.60 N/A feet User Input: Emergency Spillway (Rectangular or Trapezoidal) radians Calculated Parameters for Spillway radians Spillway Invert Stage= 4.35 ft (relative to basin bottom at Stage = 0 ft) Spillway Design Flow Depth 0.35 feet Spillway Crest Length = 75.00 feet Stage at Top of Freeboard = 0.63 arce-ft Routed Hydrograph Results The user can override the default CUMP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF). Design Storm Return Ferd = N/A N/A 1.50 1.75 2.00 2.25 2.576 3.996 OtHP Prodevelopment Peak Q (cfs) = N/A N/A 0.953 1.257 1.500 1.836 2.167 2.576 3.996 OtHP Prodevelopment Peak Q (cfs) = N/A N/A 0.21 0.42 <td< td=""><td>User Input: Outlet Pipe w/ Flow Restriction Plate</td><td>e (Circular Orifice, R</td><td>estrictor Plate, or R</td><td>ectangular Orifice)</td><td></td><td>Ca</td><td>lculated Parameter</td><td>s for Outlet Pipe w/</td><td>Flow Restriction Pl</td><td>ate</td></td<>	User Input: Outlet Pipe w/ Flow Restriction Plate	e (Circular Orifice, R	estrictor Plate, or R	ectangular Orifice)		Ca	lculated Parameter	s for Outlet Pipe w/	Flow Restriction Pl	ate
Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = 18.00 N/A inches Outlet Orifice Centroil = Half-Central Angle of Restrictor Plate on Pipe = 0.60 N/A feet User Input: Emergency Spillway (Rectangular or Trapezoidal) Spillway Crest Length Spillway Crest Cresth Spillway Crest Length Spillway Crest Length Spillwa										
Restrictor Plate Height Above Pipe Invert # 13.00 inches Half-Central Angle of Restrictor Plate on Pipe # 2.03 N/A radians User Input: Emergency Spillway (Rectangular or Trapezoidal) Calculated Parameters for Spillway Calculated Parameters for Spillway Spillway Invert Stage 4.35 ft (relative to basin bottom at Stage = 0 ft) Spillway Design Flow Depth= 0.35 feet Spillway End Slopes 4.00 H:V Basin Area at Top of Freeboard = 0.63 acres Freeboard above Max Water Surface = 1.00 feet Spillway Checkboard = 2.61 acres Mouted Hydrograph Results The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrograph table (Columns W through AF). 0.039 2.25 2.52 3.49 Ourher Narinfi Volume (acre-ft) 0.359 1.319 0.50 1.75 2.00 2.25 2.52 3.49 OPTIONAL Overlide Predevelopment Paka Q (Gi) N/A N/A 0.23 0.4 3.9 7.8 12.7 2.89 OPTIONAL Overlide Predevelopment Paka Q (Gi) N/A N/A 0.02				· ·	isin bottom at Stage	,				
User Input: Emergency Spillway (Rectangular or Trapezoidal)Calculated Parameters for SpillwaySpillway Invert Stage4.35ft (relative to basin bottom at Stage = 0 ft)Spillway Design Flow Depth=Spillway Crest Length75.00feetStage at Top of Freeboard =0.33feetSpillway End Slopes =4.00H:VBasin Area at Top of Freeboard =0.63acresFreeboard above Max Water Surface =1.00feetBasin Nolume at Top of Freeboard =2.61acresNote the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).Culter Runoff Volume (acrest)One-Hour Rainfall Depth (in) 0.259 1.3190.9531.2571.5001.8362.1672.5763.996OrtFONAL Override Predevelopment Pack Q (cfs)N/AN/A0.20.30.43.97.812.728.9OPTIONAL Override Predevelopment Pack Q (cfs)N/AN/A0.10.020.210.420.691.56Predevelopment Uter Pack Row Q (cfs)N/AN/A1.632.1525.333.039.849.076.0Pack Outflow Q (cfs)N/AN/AN/A1.632.1525.333.039.849.076.0N/AN/AN/AN/AN/A1.80.61.31.92.00.61.31.92.0OPTIONAL Overridow Q (cfs)N/A		-	N/A	1	Half Cont					
Spillway Invert Stage 4.35 ft (relative to basin bottom at Stage = 0 ft) Spillway Design Flow Depth= 0.35 feet Spillway Crest Length = 75.00 feet Stage at Top of Freeboard = 5.70 feet Spillway End Stopes = 4.00 H:V Basin Area at Top of Freeboard = 0.63 acres Routed Hydrograph Results The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF). Design Stom Return Perided N/A N/A 1.75 2.00 2.25 3.49 OutHP Runoff Volume (acreft) = N/A N/A 0.953 1.257 1.500 1.836 2.167 2.576 3.996 OUTIONAL Override Predevelopment Peak Q (cfs) = N/A N/A 0.2 0.3 0.4 3.9 7.8 12.7 28.9 Predevelopment Unit Peak (cfs) = N/A N/A 0.2 0.23 0.4 3.9 7.8 12.7 28.9 OPTIONAL Override Predevelopment Peak Q (cfs) = N/A N/A 0.2 0.2 0.2 0.2<	Restrictor Plate Height Above Pipe Invert =	15.00]	inches	nali-Celii	rai Angle of Restric	tor Plate on Pipe =	2.03	IN/A	raularis
Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = 75.00 H:V feet Stage at Top of Freeboard = Basin Area at Top of Freeboard = 0.63 Basin Area at Top of Freeboard = 2.61 feet 3.00 Routed Hydrograph Results Design Storm Return Period One-Hour Rainfall Depth (in) = UHP Runoff Volume (are-ft) = Inflow Hydrograph Volume (are-ft) = Inflow Hydrograph Volume (are-ft) = UHP Predevelopment Peak Q (cfs) = N/A The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF). CUHP Runoff Volume (are-ft) = Inflow Hydrograph Volume (are-ft) = Detextrice for edvelopment Peak Q (cfs) = Predevelopment Teak Q (cfs) = N/A N/A N/A 0.25 2.57 3.996 OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Q (cfs) = N/A N/A N/A 0.2 0.3 0.4 3.9 7.8 12.7 28.9 N/A N/A N/A N/A 0.2 0.3 0.4 3.9 7.8 12.7 28.9 OPTIONAL Override Predevelopment Peak Q (cfs) = Pack Utflow Q (cfs) = N/A N/A N/A 0.2 0.6 0.4 0.5 1.3 4.3 8.5 12.7 53.4 Ratio Peak Outflow to Predevelopment Q (cfs) = Pack Utflow Q (cfs) = N/A N/A	User Input: Emergency Spillway (Rectangular or	r Trapezoidal)	_					Calculated Parame	ters for Spillway	
Spillway End Slopes 4.00 H:V Basin Area at Top of Freeboard 0.63 acres Freeboard above Max Water Surface 1.00 feet Basin Volume at Top of Freeboard 0.63 acres Routed Hydrograph Results The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF). No NA N/A 1.19 1.50 1.75 2.00 2.25 2.52 3.49 One-Hour Rainfall Development Peak Q (cfs) = N/A N/A 1.19 1.50 1.75 2.00 2.25 2.52 3.49 OUHP predevelopment Peak Q (cfs) = N/A N/A 0.23 1.257 1.500 1.836 2.167 2.576 3.996 OPTIONAL Override Predevelopment Peak Q (cfs) = N/A N/A 0.2 0.3 0.4 3.9 7.8 12.7 28.9 Predevelopment Peak Q (cfs) = N/A N/A 0.01 0.02 0.02 0.21 0.42 0.69 1.56 Pak Inflow Q (cfs) = N/A N/A			+ `	n bottom at Stage =	0 ft)	. ,	5 1		1	
Basin Volume at Top of Freeboard = 2.61 acre-ft Routed Hydrograph Results The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF). Operation Return Period One-Hour Rainfall Depth (in) CUHP Runoff Volume (acre-ft) N/A N/A <td>. , -</td> <td></td> <td>-</td> <td></td> <td></td> <td>-</td> <td>•</td> <td></td> <td>•</td> <td></td>	. , -		-			-	•		•	
Mouted Hydrograph Results The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF). Design Storm Return Period main of the second			•				•			
Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Ranoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = N/A WQCV EURV 2 Year 5 Year 10 Year 25 Year 50 Year 100 Year 500 Year UHP Ranoff Volume (acre-ft) = CUHP predevelopment Peak Q (cfs) = Predevelopment Peak Q (cfs) = Predevelopment Peak Q (cfs) = Peak Nufflow Q (cfs) = Peak Outflow Q (cfs) = MA N/A N/A 0.953 1.257 1.500 1.836 2.167 2.576 3.996 OPTIONAL Override Predevelopment Peak Q (cfs) = Peak Nufflow Q (cfs) = Peak Outflow Q (cfs) = M/A N/A N/A 0.2 0.3 0.4 3.9 7.8 12.7 28.9 N/A N/A N/A 0.01 0.02 0.02 0.21 0.42 0.69 1.56 N/A N/A N/A 16.3 21.5 25.3 33.0 39.8 49.0 76.0 Peak Outflow to Predevelopment Q = Max Velocity through Grate 1 (fps) = Maxieure Controlling Flow = Time to Drain 97% of Inflow Volume (hours) = Maximum Ponding Depth (ft) = OXA N/A N/A N/A N/A N/A N/A N/A	Freebodru above Mdx Water Sufface =	1.00	licer			volume at 1 ווצאט	op or meenoard =	2.01		
Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Ranoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = N/A WQCV EURV 2 Year 5 Year 10 Year 25 Year 50 Year 100 Year 500 Year UHP Ranoff Volume (acre-ft) = CUHP predevelopment Peak Q (cfs) = Predevelopment Peak Q (cfs) = Predevelopment Peak Q (cfs) = Peak Nufflow Q (cfs) = Peak Outflow Q (cfs) = MA N/A N/A 0.953 1.257 1.500 1.836 2.167 2.576 3.996 OPTIONAL Override Predevelopment Peak Q (cfs) = Peak Nufflow Q (cfs) = Peak Outflow Q (cfs) = M/A N/A N/A 0.2 0.3 0.4 3.9 7.8 12.7 28.9 N/A N/A N/A 0.01 0.02 0.02 0.21 0.42 0.69 1.56 N/A N/A N/A 16.3 21.5 25.3 33.0 39.8 49.0 76.0 Peak Outflow to Predevelopment Q = Max Velocity through Grate 1 (fps) = Maxieure Controlling Flow = Time to Drain 97% of Inflow Volume (hours) = Maximum Ponding Depth (ft) = OXA N/A N/A N/A N/A N/A N/A N/A	D	7/								
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CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Predex Q (cfs) = Predevelopment Dit Peak D (cfs) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Peak Unflow Q (cfs) = N/A N/A N/A 0.2 0.3 0.4 3.96 3.96 N/A N/A 0.2 0.3 0.4 3.9 2.167 2.576 3.996 N/A N/A 0.2 0.3 0.4 3.9 7.8 12.7 28.9 N/A N/A N/A 0.01 0.02 0.02 0.21 0.42 0.69 1.56 N/A N/A N/A 16.3 21.5 25.3 33.0 38.8 49.0 76.0 Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Maxium Ponding Depth (fps) = Maxium Ponding Depth (ferce) = N/A N/A<										
CUHP Predevelopment Peak Q (cfs) = Predevelopment Data V (cfs) = Predevelopment Unit Peak Row, q (cfs/acre) = N/A N/A N/A 0.2 0.3 0.4 3.9 7.8 12.7 28.9 N/A N/	CUHP Runoff Volume (acre-ft) =	0.359	1.319	0.953	1.257	1.500	1.836	2.167	2.576	3.996
N/A N/A <td></td>										
Peak Inflow Q (cfs) Peak Outflow Q (cfs) Ratio Peak Outflow Q (cfs) Ratio Peak Outflow to Predevelopment Q = N/A N/A 16.3 21.5 25.3 33.0 39.8 49.0 76.0 Ratio Peak Outflow Q (cfs) Ratio Peak Outflow to Predevelopment Q = 0.2 0.6 0.4 0.5 1.3 4.3 8.5 12.7 53.4 Max Velocity through Grate 1 (fps) = N/A N/A N/A N/A 1.8 3.2 1.1 1.1 1.0 1.8 Max Velocity through Grate 1 (fps) = Plate Plate Plate Plate Overflow Weir 1 N/A N/A N/A Max Velocity through Grate 2 (fps) = N/A	OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Peak Outflow Q (cfs) = 0.2 0.6 0.4 0.5 1.3 4.3 8.5 12.7 53.4 Ratio Peak Outflow to Predevelopment Q = N/A N/A N/A N/A 1.8 3.2 1.1 1.1 1.0 1.8 Structure Controlling Flow = Plate Plate Plate Plate Plate Overflow Weir 1 N/A										
N/A N/A N/A N/A 1.8 3.2 1.1 1.1 1.0 1.8 Structure Controlling Flow = Plate Plate Plate Plate Plate Overflow Weir 1 N/A										
Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 99% of Inflow Volume (hours) = Maximum Ponding Depth (ft) = Area at Maximum Ponding Depth (arces) = N/A	Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	1.8	3.2	1.1	1.1	1.0	1.8
Max Velocity through Grate 2 (fps) = N/A										
Time to Drain 99% of Inflow Volume (hours) = 40 70 63 69 73 73 72 71 69 Maximum Ponding Depth (ft) = 1.26 3.42 2.53 3.14 3.56 3.78 4.00 4.34 4.66 Area at Maximum Ponding Depth (acres) = 0.38 0.50 0.45 0.49 0.51 0.52 0.54 0.56 0.57	Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Maximum Ponding Depth (ft) = 1.26 3.42 2.53 3.14 3.56 3.78 4.00 4.34 4.66 Area at Maximum Ponding Depth (acres) = 0.38 0.50 0.45 0.49 0.51 0.52 0.54 0.56 0.57										
Area at Maximum Ponding Depth (acres) = 0.38 0.50 0.45 0.49 0.51 0.52 0.54 0.56 0.57										
Maximum Volume Stored (acre-ft) = 0.361 1.319 0.893 1.175 1.390 1.504 1.616 1.807 1.988	Area at Maximum Ponding Depth (acres) =	0.38	0.50	0.45	0.49	0.51	0.52	0.54	0.56	0.57



DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

[SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	l in a separate pr CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]		25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	
	0:00:00									
5.00 min		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00 0:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.25	0.03	1.27
	0:20:00	0.00	0.00	2.25	3.65 9.94	4.53 11.67	3.05 7.34	8.51	3.72 9.18	6.09 13.41
·	0:25:00	0.00	0.00	15.01	19.95	24.24	14.88	16.95	18.26	28.04
	0:30:00	0.00	0.00	16.33	21.55	25.34	31.00	37.73	43.27	68.84
	0:35:00	0.00	0.00	14.22	18.37	21.41	33.00	39.78	48.96	76.02
	0:40:00	0.00	0.00	12.15	15.35	17.83	29.65	35.72	43.68	67.86
	0:45:00	0.00	0.00	9.80	12.66	14.79	24.72	29.66	37.57	58.73
	0:50:00	0.00	0.00	8.10	10.70	12.28	20.93	24.93	31.19	49.06
	0:55:00	0.00	0.00	6.96	9.13	10.61	16.88	19.94	25.50	40.12
	1:00:00	0.00	0.00	6.03	7.84	9.21	14.05	16.49	21.68	34.27
	1:05:00	0.00	0.00	5.18	6.69	7.93	11.85	13.82	18.74	29.81
	1:15:00	0.00	0.00	4.12 3.44	5.76 4.97	6.90 6.34	9.47 7.57	10.95 8.64	14.26 10.68	22.31 16.40
	1:20:00	0.00	0.00	3.08	4.45	5.76	6.04	6.84	7.78	11.83
	1:25:00	0.00	0.00	2.88	4.14	5.08	5.17	5.83	6.04	9.03
	1:30:00	0.00	0.00	2.76	3.94	4.61	4.42	4.97	5.00	7.33
·	1:35:00	0.00	0.00	2.70	3.80	4.28	3.92	4.40	4.34	6.25
	1:40:00	0.00	0.00	2.64	3.39	4.04	3.59	4.04	3.89	5.52
	1:45:00	0.00	0.00	2.60	3.08	3.88	3.37	3.79	3.59	5.03
	1:50:00	0.00	0.00	2.58	2.86	3.77	3.22	3.62	3.40	4.71
	1:55:00	0.00	0.00	2.20	2.71	3.57	3.13	3.52	3.31	4.59
	2:00:00	0.00	0.00	1.92	2.51	3.21	3.08	3.46	3.28	4.54
	2:05:00 2:10:00	0.00	0.00	1.35	1.76	2.25	2.16	2.42	2.30	3.18
	2:15:00	0.00	0.00	0.92	1.21 0.81	1.55	1.49 1.02	1.67 1.14	1.59	2.19
	2:20:00	0.00	0.00	0.03	0.53	0.69	0.67	0.75	0.72	0.98
	2:25:00	0.00	0.00	0.26	0.34	0.45	0.43	0.49	0.46	0.63
	2:30:00	0.00	0.00	0.15	0.21	0.27	0.27	0.31	0.29	0.39
	2:35:00	0.00	0.00	0.07	0.12	0.14	0.15	0.17	0.16	0.21
	2:40:00	0.00	0.00	0.03	0.05	0.06	0.06	0.07	0.07	0.09
	2:45:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00 3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
·	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ŀ	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
·	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
·	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ŀ	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
·	4:30:00 4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ľ	4:50:00 4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ŀ	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ŀ	5:40:00 5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.04 (February 2021) Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage [ft]	Area [ft ²]	Area [acres]	Volume [ft ³]	Volume [ac-ft]	Total Outflow [cfs]	
							For best results, include the
							stages of all grade slope changes (e.g. ISV and Floor) from the S-A-V table on
							changes (e.g. ISV and Floor)
							Sheet 'Basin'.
							Sheet Basin.
							Also include the inverts of al
							outlets (e.g. vertical orifice,
							overflow grate, and spillway,
						_	where applicable).
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DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

	Project: The Com	mons at Falcon Field
	Basin ID: Pond B	
	ZONE 1 AND 2 DOINE 1 AND 2 DOINE 1 AND 2	100-YEAR ORIFICE
POOL	Example Zone Configu	ration (Retention Pond)

Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	13.55	acres
Watershed Length =	915	ft
Watershed Length to Centroid =	450	ft
Watershed Slope =	0.030	ft/ft
Watershed Imperviousness =	89.00%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

	the embedded Colorado Urban Hydro	graph Procedu	ire.	Optional User	Ove
٧	Vater Quality Capture Volume (WQCV) =	0.444	acre-feet		acre
	Excess Urban Runoff Volume (EURV) =	1.634	acre-feet		acre
	2-yr Runoff Volume (P1 = 1.19 in.) =	1.106	acre-feet	1.19	inch
	5-yr Runoff Volume (P1 = 1.5 in.) =	1.426	acre-feet	1.50	inch
	10-yr Runoff Volume (P1 = 1.75 in.) =	1.684	acre-feet	1.75	inch
	25-yr Runoff Volume (P1 = 2 in.) =	1.967	acre-feet	2.00	inch
	50-yr Runoff Volume (P1 = 2.25 in.) =	2.243	acre-feet	2.25	inch
	100-yr Runoff Volume (P1 = 2.52 in.) =	2.554	acre-feet	2.52	inch
	500-yr Runoff Volume (P1 = 3.49 in.) =	3.652	acre-feet	3.49	inch
	Approximate 2-yr Detention Volume =	1.078	acre-feet		
	Approximate 5-yr Detention Volume =	1.398	acre-feet		
	Approximate 10-yr Detention Volume =	1.660	acre-feet		
	Approximate 25-yr Detention Volume =	1.958	acre-feet		
	Approximate 50-yr Detention Volume =	2.132	acre-feet		
,	Approximate 100-yr Detention Volume =	2.283	acre-feet		

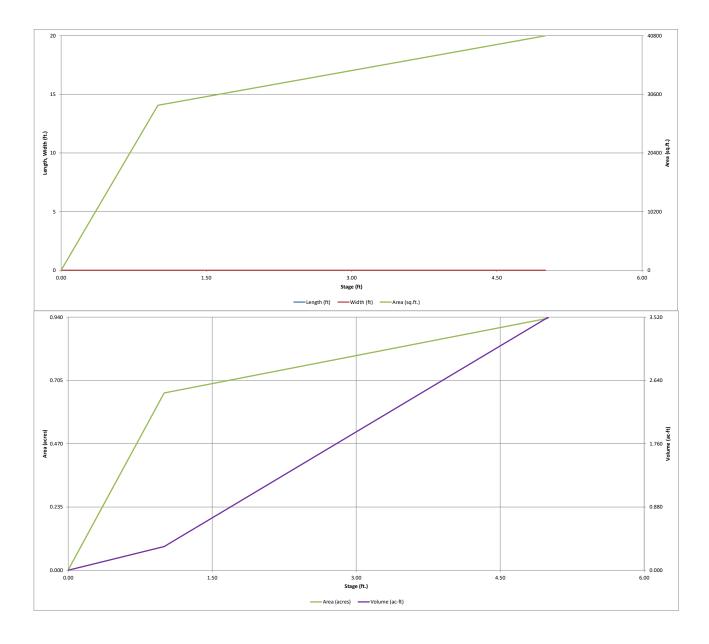
Define Zones and Basin Geometry

chine zones and basin deomedy		
Zone 1 Volume (WQCV) =	0.444	acre-feet
Zone 2 Volume (EURV - Zone 1) =	1.190	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.649	acre-feet
Total Detention Basin Volume =	2.283	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth $(H_{total}) =$	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S _{TC}) =	user	ft/ft
Slopes of Main Basin Sides (S _{main}) =	user	H:V
Basin Length-to-Width Ratio $(R_{L/W}) =$	user	
		_
Initial Surcharge Area $(A_{ISV}) =$	user	ft 2
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor (W_{FLOOR}) =	user	ft
Area of Basin Floor (A _{FLOOR}) =	user	ft ²
Volume of Basin Floor $(V_{FLOOR}) =$	user	ft ³
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft ²
Volume of Main Basin (V_{MAIN}) =	user	ft ³
Calculated Total Basin Volume (V_{total}) =	user	acre-feet

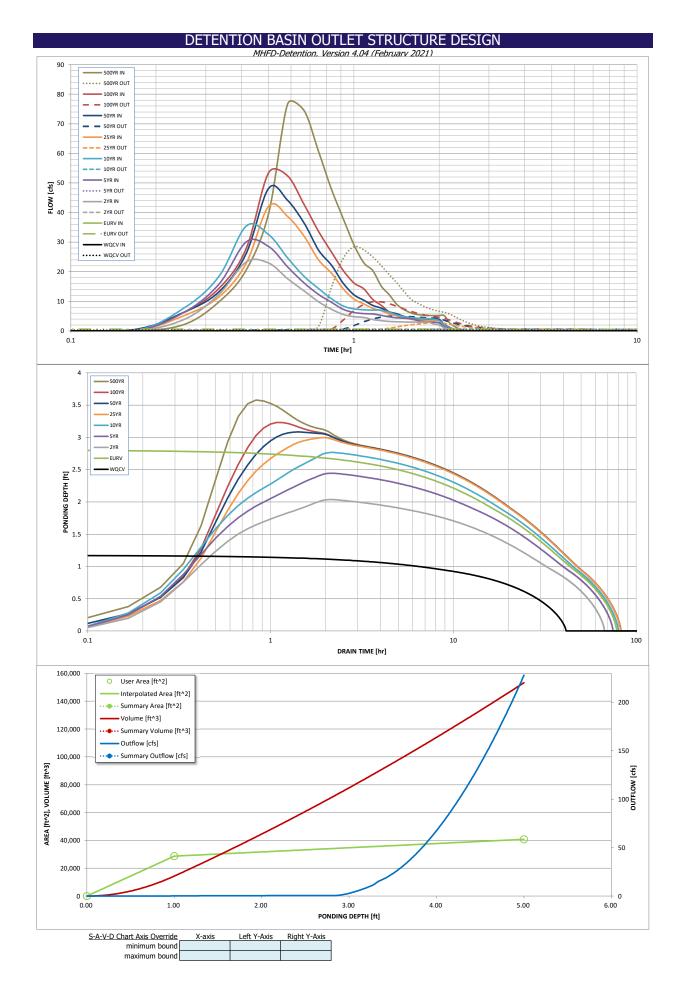
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	Top of Micropool							0.001			
	6832		1.00				28,695	0.659	14,367	0.330	
	6836		5.00				40,779	0.936	153,315	3.520	
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DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



Project:	The Commons at I		-D-Delention, vers	SION 4.04 (Februar	y 2021)				
Basin ID:	Pond B								
				Estimated	Estimated				
100-YR				Stage (ft)	Volume (ac-ft)	Outlet Type			
			Zone 1 (WQCV)	1.18	0.444	Orifice Plate			
i line	100-YEAR ORIFICE		Zone 2 (EURV)	2.81	1.190	Orifice Plate			
PERMANENT ZONE 1 AND 2 POOL ORIFICES			Zone 3 (100-year)	3.61	0.649	Weir&Pipe (Circular)			
Example Zone	Configuration (Re	tention Pond)		Total (all zones)	2.283				
User Input: Orifice at Underdrain Outlet (typicall	<u>y used to drain WC</u>	CV in a Filtration B	<u>MP)</u>			-	Calculated Parame	ters for Underdrain	
Underdrain Orifice Invert Depth =	N/A	ft (distance below	the filtration media	surface)	Underc	Irain Orifice Area =	N/A	ft ²	
Underdrain Orifice Diameter =	N/A	inches			Underdrair	Orifice Centroid =	N/A	feet	
User Input: Orifice Plate with one or more orific		1	-		,		Calculated Parame		
Invert of Lowest Orifice =	0.00		h bottom at Stage =		-	ce Area per Row =	3.132E-02	ft ²	
Depth at top of Zone using Orifice Plate = Orifice Plate: Orifice Vertical Spacing =	2.81	inches	bottom at Stage =	010)		ptical Half-Width = ical Slot Centroid =	N/A N/A	feet	
Orifice Plate: Orifice Area per Row =	4.51		tangular openings)			lliptical Slot Area =	N/A N/A	ft ²	
onnee hate. Onnee Area per Now -	1.51	lad. menea (uae ree			-		N/A	lic	
User Input: Stage and Total Area of Each Orifice	e Row (numbered f	rom lowest to high	est)						
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	
Stage of Orifice Centroid (ft)	0.00	0.94	1.87						
Orifice Area (sq. inches)	4.51	4.51	4.51						l
									1
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	
Stage of Orifice Centroid (ft)									
Orifice Area (sq. inches)	<u></u>								
User Input: Vertical Orifice (Circular or Rectange	ular)						Calculated Parame	eters for Vertical Orif	fice
oser input. Ventical onnee (encadar of Rectange	Not Selected	Not Selected	1				Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage =	= 0 ft) Ver	tical Orifice Area =	N/A		ft ²
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin	-	,	Orifice Centroid =	N/A		feet
Vertical Orifice Diameter =	N/A		inches	j	, ,		,	· · · ·	
		,							
User Input: Overflow Weir (Dropbox with Flat o	r Sloped Grate and	Outlet Pipe OR Rec	tangular/Trapezoid	al Weir (and No Ou	itlet Pipe)		Calculated Parame	ters for Overflow W	<u>eir</u>
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	2.85	N/A	ft (relative to basin b	oottom at Stage = 0 f		e Upper Edge, $H_t =$	2.85	· · · · ·	feet
Overflow Weir Front Edge Length =	6.00	N/A	feet	_		/eir Slope Length =	6.00		feet
Overflow Weir Grate Slope =	0.00	N/A	H:V		ate Open Area / 10	•	14.18	N/A	- 2
Horiz. Length of Weir Sides =	6.00	N/A	feet		verflow Grate Open		25.06		ft ² ft ²
Overflow Grate Type = Debris Clogging % =	Type C Grate 50%	N/A N/A	%	(Overflow Grate Ope	n Area w/ Debris =	12.53	N/A	,tt-
Debris Clogging % =	50%	IN/A	90						
User Input: Outlet Pipe w/ Flow Restriction Plate	(Circular Orifice, R	estrictor Plate, or R	ectangular Orifice)		Ca	lculated Parameter	s for Outlet Pipe w/	Flow Restriction Pla	ate
	Zone 3 Circular	Not Selected			<u></u>		Zone 3 Circular	Not Selected	<u></u>
Depth to Invert of Outlet Pipe =	0.00	N/A	ft (distance below ba	sin bottom at Stage	= 0 ft) O	utlet Orifice Area =	1.77		ft ²
Circular Orifice Diameter =	18.00	N/A	inches	5	-	Orifice Centroid =	0.75		feet
			1	Half-Cent	ral Angle of Restric	tor Plate on Pipe =	N/A	N/A	radians
User Input: Emergency Spillway (Rectangular or		1					Calculated Parame		
Spillway Invert Stage=	3.26	ft (relative to basir	bottom at Stage =	• 0 ft)		esign Flow Depth=	0.74	feet	
Spillway Crest Length =	25.00	feet			-	Top of Freeboard =	5.00	feet	
Spillway End Slopes =	4.00	H:V				Top of Freeboard =	0.94	acres	
Freeboard above Max Water Surface =	1.00	feet			Basin Volume at I	op of Freeboard =	3.52	acre-ft	
Routed Hydrograph Results	The user can over	ride the default CUI	HP hydrographs and	d runoff volumes by	v entering new valu	es in the Inflow Hy	drographs table (Co	olumns W through A	1 <i>F).</i>
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) =	N/A 0.444	N/A 1.634	1.19 1.106	1.50 1.426	1.75 1.684	2.00 1.967	2.25 2.243	2.52 2.554	3.49 3.652
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	1.106	1.426	1.684	1.907	2.243	2.554	3.652
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.1	0.3	0.4	3.1	6.2	10.2	23.1
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A	0.01	0.02	0.02	0.02	0.45	0.75	4.74
Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) =	N/A N/A	N/A N/A	0.01 23.3	0.02 30.1	0.03 35.4	0.23 42.2	0.46 48.2	0.75 53.5	1.71 76.7
Peak Outflow Q (cfs) =	0.2	0.6	0.4	0.5	0.6	2.8	5.1	9.8	28.4
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	2.1	1.7	0.9	0.8	1.0	1.2
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Spillway
Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) =	N/A N/A	N/A N/A	N/A N/A	N/A N/A	N/A N/A	0.1 N/A	0.2 N/A	0.4 N/A	0.5 N/A
Time to Drain 97% of Inflow Volume (hours) =	38	70	61	67	71	73	72	71	67
Time to Drain 99% of Inflow Volume (hours) =	40	75	64	71	76	78	78	77	76
Maximum Ponding Depth (ft) =	1.18	2.81	2.04	2.44	2.77	3.00	3.09	3.23	3.58
Area at Maximum Ponding Depth (acres) = Maximum Volume Stored (acre-ft) =	0.67 0.450	0.78 1.636	0.73 1.045	0.76 1.350	0.78	0.80	0.80 1.850	0.81 1.971	0.84 2.252
maximum volume stored (dtle-it) =	0.130	1 1.000	L TIDI	1.000	1.337	1.1.10	1 1.000	1 1.7/1	2.232



Outflow Hydrograph Workbook Filename:

[SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.43	0.04	2.11
-	0:15:00	0.00	0.00	3.79	6.16	7.62	5.11	6.23	6.20	9.78
	0:20:00	0.00	0.00	12.31	15.76	18.36	11.47	13.20	14.32	20.58
-	0:25:00	0.00	0.00	23.33	30.09	35.44	22.89	26.19	27.85	39.87
-	0:30:00	0.00	0.00	22.91 17.62	28.50 21.64	32.50 24.68	42.20 38.67	48.24 44.10	53.54 52.38	76.66 74.47
-	0:40:00	0.00	0.00	17.62	16.22	18.46	31.99	36.46	42.74	60.68
-	0:45:00	0.00	0.00	9.83	12.34	14.32	24.00	27.31	33.64	47.83
	0:50:00	0.00	0.00	7.33	9.68	10.85	19.54	22.21	26.65	37.98
	0:55:00	0.00	0.00	5.58	7.29	8.43	14.21	16.14	20.47	29.12
	1:00:00	0.00	0.00	4.82	6.24	7.44	10.76	12.21	16.20	23.06
	1:05:00	0.00	0.00	4.55	5.86	7.14	9.15	10.38	14.25	20.34
	1:15:00	0.00	0.00	3.83 3.45	5.71 5.25	7.03	7.60 6.81	8.60 7.69	10.60 8.60	15.09 12.23
-	1:20:00	0.00	0.00	3.22	4.75	6.34	5.71	6.44	6.38	9.00
-	1:25:00	0.00	0.00	3.10	4.46	5.40	5.16	5.81	5.19	7.27
	1:30:00	0.00	0.00	3.02	4.29	4.84	4.39	4.94	4.42	6.16
	1:35:00	0.00	0.00	2.97	4.19	4.51	3.95	4.45	4.01	5.56
	1:40:00	0.00	0.00	2.97	3.58	4.31	3.71	4.17	3.85	5.33
	1:45:00 1:50:00	0.00	0.00	2.97	3.23	4.19	3.58	4.03	3.78	5.23
	1:55:00	0.00	0.00	2.97 2.34	3.03 2.92	4.15 3.96	3.52 3.49	3.96 3.93	3.77 3.77	5.22
-	2:00:00	0.00	0.00	1.97	2.69	3.48	3.49	3.93	3.77	5.22
-	2:05:00	0.00	0.00	1.11	1.52	1.99	2.00	2.25	2.16	2.99
-	2:10:00	0.00	0.00	0.62	0.86	1.12	1.14	1.28	1.23	1.70
	2:15:00	0.00	0.00	0.30	0.45	0.58	0.60	0.67	0.65	0.89
	2:20:00	0.00	0.00	0.14	0.23	0.28	0.31	0.35	0.33	0.46
	2:25:00 2:30:00	0.00	0.00	0.05	0.08	0.09	0.11	0.13	0.12	0.16
	2:35:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
	2:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	3:05:00 3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	3:40:00 3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00 4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	4:35:00 4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	4:50:00 4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	5:10:00 5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00 5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00 5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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MHFD-Detention, Version 4.04 (February 2021) Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage [ft]	Area [ft ²]	Area [acres]	Volume [ft ³]	Volume [ac-ft]	Total Outflow [cfs]	
							For best results, include the
							stages of all grade slope changes (e.g. ISV and Floor) from the S-A-V table on
							changes (e.g. ISV and Floor)
							Sheet 'Basin'.
							Sheet Basin.
							Also include the inverts of all
							outlets (e.g. vertical orifice,
							overflow grate, and spillway,
							where applicable).
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DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

	Project:	The Commons a	at Falcon Field
	Basin ID:	Pond C	
		1 AND 2	100-YEAR ORIFICE
POOL	Example Zone	Configuration (Retention Pond)

Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	26.61	acres
Watershed Length =	1,500	ft
Watershed Length to Centroid =	650	ft
Watershed Slope =	0.050	ft/ft
Watershed Imperviousness =	58.00%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Urban Hydro	graph Procedu	re.	Optional User	Ove
Water Quality Capture Volume (WQCV) =	0.509	acre-feet		acri
Excess Urban Runoff Volume (EURV) =	1.855	acre-feet		acri
2-yr Runoff Volume (P1 = 1.19 in.) =	1.339	acre-feet	1.19	inch
5-yr Runoff Volume (P1 = 1.5 in.) =	1.767	acre-feet	1.50	inch
10-yr Runoff Volume (P1 = 1.75 in.) =	2.110	acre-feet	1.75	inch
25-yr Runoff Volume (P1 = 2 in.) =	2.592	acre-feet	2.00	inch
50-yr Runoff Volume (P1 = 2.25 in.) =	3.065	acre-feet	2.25	inch
100-yr Runoff Volume (P1 = 2.52 in.) =	3.652	acre-feet	2.52	inch
500-yr Runoff Volume (P1 = 3.49 in.) =	5.688	acre-feet	3.49	inch
Approximate 2-yr Detention Volume =	1.201	acre-feet		
Approximate 5-yr Detention Volume =	1.575	acre-feet		
Approximate 10-yr Detention Volume =	1.908	acre-feet		
Approximate 25-yr Detention Volume =	2.313	acre-feet		
Approximate 50-yr Detention Volume =	2.561	acre-feet		
Approximate 100-yr Detention Volume =	2.839	acre-feet		

Define Zones and Basin Geometry

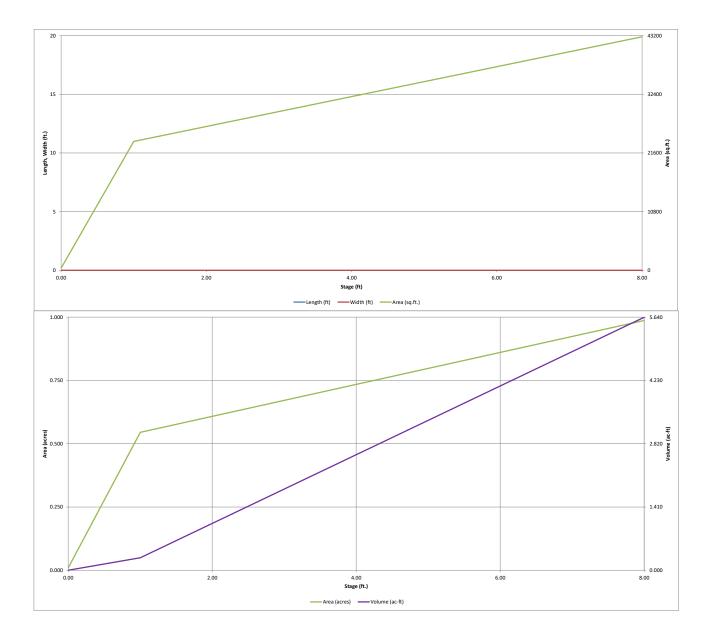
chine zones and basin deomedy		
Zone 1 Volume (WQCV) =	0.509	acre-feet
Zone 2 Volume (EURV - Zone 1) =	1.346	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.984	acre-feet
Total Detention Basin Volume =	2.839	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth $(H_{total}) =$	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S _{TC}) =	user	ft/ft
Slopes of Main Basin Sides (S _{main}) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	
		_
Initial Surcharge Area $(A_{ISV}) =$	user	ft ²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor (W_{FLOOR}) =	user	ft
Area of Basin Floor (A _{FLOOR}) =	user	ft ²
Volume of Basin Floor $(V_{FLOOR}) =$	user	ft ³
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin (A _{MAIN}) =	user	ft 2
Volume of Main Basin (V_{MAIN}) =	user	ft ³
		1

 $\begin{array}{c|c} Volume of Main Basin (V_{MAIN}) = & user & ft^{3} \\ \hline Calculated Total Basin Volume (V_{total}) = & user & acre-feet \\ \end{array}$

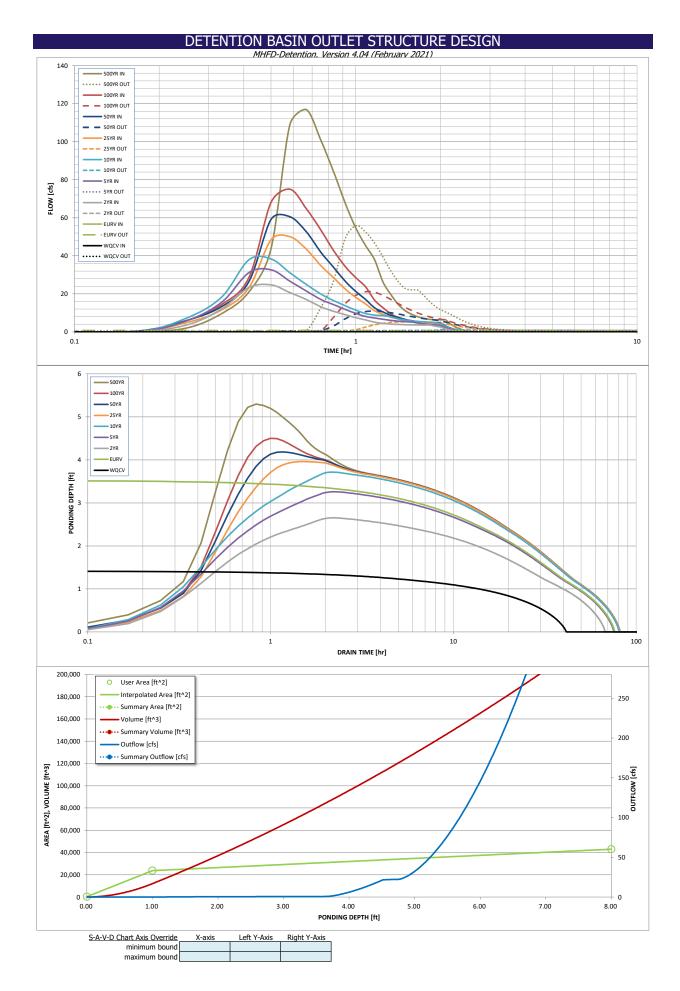
Depth Increment =		ft Optional			4	Optional		Mahama	
Stage - Storage Description	Stage (ft)	Override Stage (ft)	Length (ft)	Width (ft)	Area (ft ²)	Override Area (ft ²)	Area (acre)	Volume (ft ³)	Volum (ac-ft
Top of Micropool		0.00				400	0.009		
6805		1.00				23,745	0.545	12,072	0.277
6812		8.00				42,990	0.987	245,645	5.639
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DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



			FD-Detention, Vers	sion 4.04 (Februar	ry 2021)				
Project: Basin ID:	The Commons at I	Falcon Field							
ZONE 3	Pona C			Estimated	Estimated				
				Stage (ft)	Volume (ac-ft)	Outlet Type			
	1		Zone 1 (WQCV)	1.42	0.509	Orifice Plate]		
	100-YEAR ORIFICE		Zone 2 (EURV)	3.53	1.346	Orifice Plate	1		
PERMANENT ORIFICES	ORIFICE		Zone 3 (100-year)	4.85	0.984	Weir&Pipe (Circular)	1		
POOL Example Zone	Configuration (Re	tention Pond)		Total (all zones)	2.839		1		
User Input: Orifice at Underdrain Outlet (typicall	<u>y used to drain WC</u>	CV in a Filtration B	<u>MP)</u>			-	Calculated Parame	eters for Underdrain	
Underdrain Orifice Invert Depth =		ft (distance below	the filtration media	surface)	Underc	Irain Orifice Area =		ft ²	
Underdrain Orifice Diameter =		inches			Underdrair	Orifice Centroid =		feet	
User Input: Orifice Plate with one or more orific	es er Elliptical Clat	Mair (typically year	te drain WOCV and	d/or ELID\/ in a cod	imontation RMD)				
Invert of Lowest Orifice =	0.00	1	n bottom at Stage =			ce Area per Row =	Calculated Parame 3.396E-02	ft ²	
Depth at top of Zone using Orifice Plate =	3.53	+ `	bottom at Stage =			ptical Half-Width =	N/A	feet	
Orifice Plate: Orifice Vertical Spacing =	14.10	inches	5	,		ical Slot Centroid =	N/A	feet	
Orifice Plate: Orifice Area per Row =	4.89	sq. inches (use rec	tangular openings)		E	lliptical Slot Area =	N/A	ft ²	
User Input: Stage and Total Area of Each Orific									
Chara - 6 (2016) - (2016) - (11/0)	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	
Stage of Orifice Centroid (ft) Orifice Area (sq. inches)		1.18 4.89	2.35 4.89						
Office Area (sq. IICHES)	1.05	1.05	1.05						I
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	
Stage of Orifice Centroid (ft)									
Orifice Area (sq. inches)									
							<u></u>		c
User Input: Vertical Orifice (Circular or Rectange	ular) Not Selected	Not Selected	1				Calculated Parame	eters for Vertical Ori Not Selected	rice
Invert of Vertical Orifice =	Not Selected	Not Selected	ft (relative to basin	bottom at Stage -	-0ft) Ver	tical Orifice Area =	Not Selected	Not Selected	ft ²
Depth at top of Zone using Vertical Orifice =	N/A	N/A N/A	ft (relative to basin	-		I Orifice Centroid =	N/A	N/A N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches	bottom at otage				.,,,	
	,	,							
User Input: Overflow Weir (Dropbox with Flat o	r Sloped Grate and	Outlet Pipe OR Rec	tangular/Trapezoid	al Weir (and No Ou	itlet Pipe)		Calculated Parame	eters for Overflow W	/eir
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	3.65	N/A	ft (relative to basin b	oottom at Stage = 0 f	-	e Upper Edge, $H_t =$	3.65	N/A	feet
Overflow Weir Front Edge Length =	4.00	N/A	feet			/eir Slope Length =	4.00	N/A	feet
Overflow Weir Grate Slope =	0.00 4.00	N/A N/A	H:V feet		ate Open Area / 10	•	6.30 11.14	N/A N/A	ft ²
Horiz. Length of Weir Sides = Overflow Grate Type =	Type C Grate	N/A N/A	leet		verflow Grate Open Overflow Grate Ope		5.57	N/A N/A	ft ²
Debris Clogging % =	50%	N/A	%			TAICO W/ DEDIIS -	5.57	N/A	lir
			1						
User Input: Outlet Pipe w/ Flow Restriction Plate	e (Circular Orifice, R	estrictor Plate, or R	ectangular Orifice)		Ca	Iculated Parameter	s for Outlet Pipe w	/ Flow Restriction Pl	ate
	Zone 3 Circular	Not Selected					Zone 3 Circular	Not Selected	
Depth to Invert of Outlet Pipe =	2.83	N/A	ft (distance below ba	asin bottom at Stage		utlet Orifice Area =	1.77	N/A	ft ²
Circular Orifice Diameter =	18.00	N/A	inches			Orifice Centroid =	0.75	N/A	feet
				Half-Cent	ral Angle of Restric	tor Plate on Pipe =	N/A	N/A	radians
User Input: Emergency Spillway (Rectangular or	Tranezoidal)						Calculated Parame	aters for Snillway	
Spillway Invert Stage=		ft (relative to basin	n bottom at Stage =	: 0 ft)	Snillway D	esign Flow Depth=		feet	
Spillway Crest Length =	25.00	feet	strom at stuge -	,		Top of Freeboard =	6.67	feet	
Spillway End Slopes =	-	H:V			-	Top of Freeboard =	0.90	acres	
Freeboard above Max Water Surface =	1.00	feet			Basin Volume at 1	op of Freeboard =	4.38	acre-ft	
Routed Hydrograph Results	The user can over	ride the default (11	HP hydroaranhs and	d runoff volumes h	v enterina new valu	es in the Inflow Hu	drographs table (C	olumns W through ,	4 <i>F).</i>
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52	3.49
CUHP Runoff Volume (acre-ft) =	0.509	1.855	1.339	1.767	2.110	2.592	3.065	3.652	5.688
Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) =	N/A N/A	N/A N/A	1.339 0.3	1.767 0.5	2.110 0.7	2.592 6.3	3.065	3.652 20.4	5.688 46.3
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.02	0.03	0.24	0.47	0.77	1.74
Peak Inflow Q (cfs) = Peak Outflow Q (cfs) =	N/A 0.3	N/A 0.7	24.7 0.6	32.7 0.7	38.4	50.1 5.3	60.5 10.9	75.0	116.9 55.8
Ratio Peak Outflow to Predevelopment $Q =$	N/A	N/A	N/A	1.4	1.7	0.8	0.9	1.0	1.2
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Spillway
Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) =	N/A N/A	N/A N/A	N/A N/A	N/A N/A	0.0 N/A	0.4 N/A	0.9 N/A	1.8 N/A	2.0 N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	61	67	72	71	69	68	62
Time to Drain 99% of Inflow Volume (hours) =	40	73	65	72	77	77	76	75	73
Maximum Ponding Depth (ft) = Area at Maximum Ponding Depth (acres) =	1.42 0.57	3.53 0.70	2.65 0.65	3.26 0.69	3.72 0.72	3.96 0.73	4.19 0.75	4.50 0.77	5.30 0.82
Area at Maximum Ponding Depth (acres) = Maximum Volume Stored (acre-ft) =	0.57	1.858	1.262	1.663	1.986	2.167	2.330	2.572	3.196



DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

o<mark>hs</mark> ide the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program The user can over

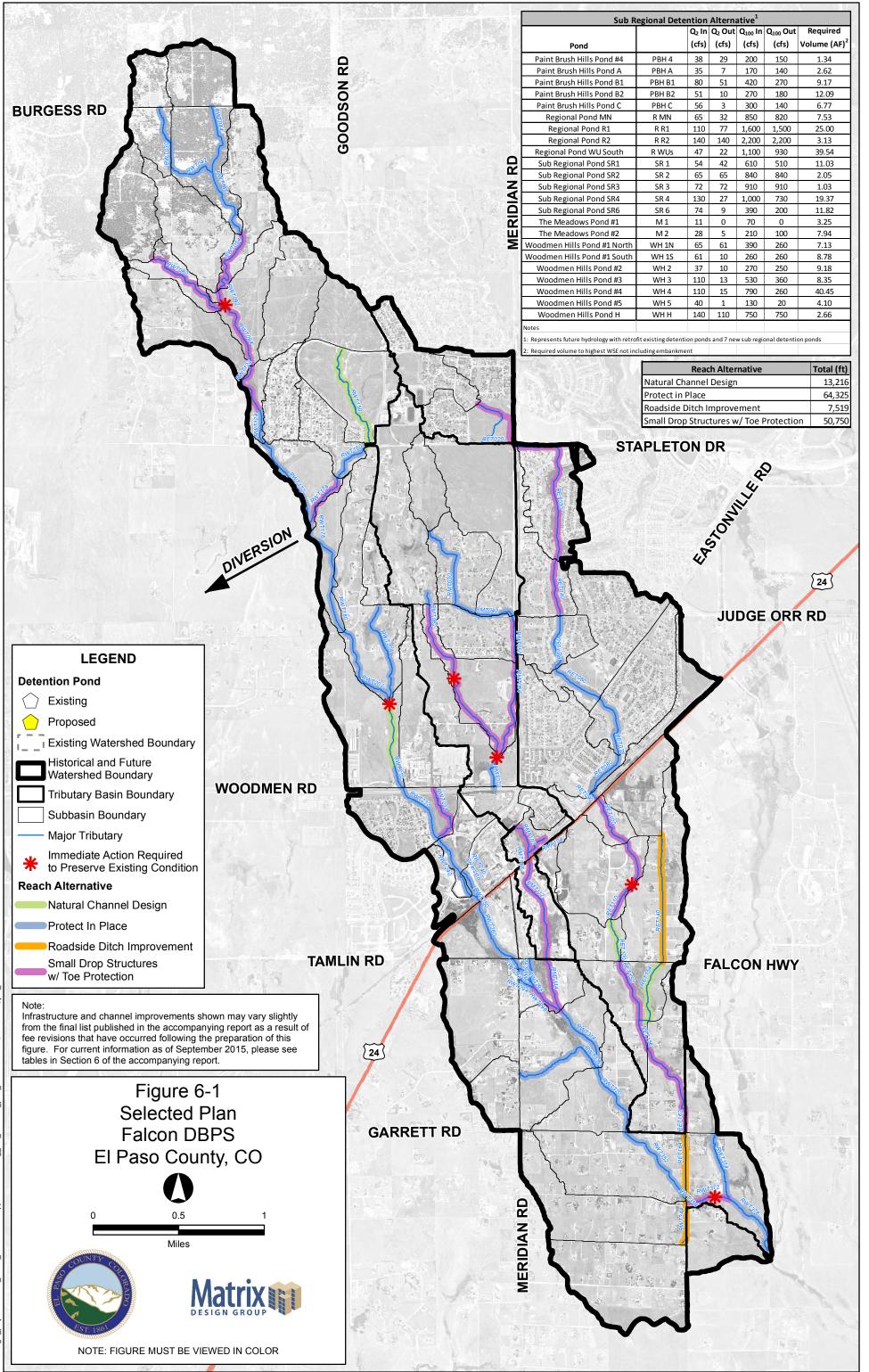
Time Interval TIME WQCV [cfs] EURV [cfs] 2 Year [cfs] 5 Year [cfs] 10 Year 5.00 min 0:00:00 0.00 0.00 0.00 0.00 0.00 0.00 0:05:00 0.00 <td< th=""><th>JHP CUHP var [cfs] 25 Year [cfs] .00 0.00 .00 0.00 .00 0.00 .00 0.00 .00 0.00 .00 1.04 .22 4.86 .328 11.49 .337 48.40 1.09 50.08 .496 43.60 .00 34.95</th><th>CUHP 50 Year [cfs] 0.00 0.41 5.99 13.30 26.30 59.17</th><th>CUHP 100 Year [cfs] 0.00 0.00 0.04 5.93 14.38</th><th>0.00 0.00 2.03 9.62</th></td<>	JHP CUHP var [cfs] 25 Year [cfs] .00 0.00 .00 0.00 .00 0.00 .00 0.00 .00 0.00 .00 1.04 .22 4.86 .328 11.49 .337 48.40 1.09 50.08 .496 43.60 .00 34.95	CUHP 50 Year [cfs] 0.00 0.41 5.99 13.30 26.30 59.17	CUHP 100 Year [cfs] 0.00 0.00 0.04 5.93 14.38	0.00 0.00 2.03 9.62
5.00 min 0:00:00 0.00	.00 0.00 .00 0.00 .00 0.00 .22 4.86 3.28 11.49 7.85 23.12 3.37 48.40 1.09 50.08 4.96 43.60	0.00 0.00 0.41 5.99 13.30 26.30	0.00 0.00 0.04 5.93 14.38	0.00 0.00 2.03 9.62
0:05:00 0:00	.00 0.00 .00 0.00 .22 4.86 8.28 11.49 7.85 23.12 3.37 48.40 1.09 50.08 4.96 43.60	0.00 0.41 5.99 13.30 26.30	0.00 0.04 5.93 14.38	0.00 2.03 9.62
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0:10:00 0.00 0.00 0.00 0.00 0.00 0:15:00 0.00 0.00 3.58 5.82 7. 0:20:00 0.00 0.00 12.06 15.59 18 0:25:00 0.00 0.00 23.32 31.10 37 0:30:00 0.00 0.00 24.74 32.66 38 0:35:00 0.00 0.00 20.71 26.69 31 0:40:00 0.00 0.00 17.07 21.50 24 0:45:00 0.00 0.00 13.27 17.12 20 0:50:00 0.00 0.00 10.85 14.39 16	.00 0.00 .22 4.86 3.28 11.49 7.85 23.12 3.37 48.40 1.09 50.08 4.96 43.60	0.41 5.99 13.30 26.30	0.04 5.93 14.38	2.03 9.62
0:20:00 0.00 0.00 12.06 15.59 18 0:25:00 0.00 0.00 23.32 31.10 37 0:30:00 0.00 0.00 24.74 32.66 38 0:35:00 0.00 0.00 20.71 26.69 31 0:40:00 0.00 0.00 17.07 21.50 24 0:45:00 0.00 0.00 13.27 17.12 20 0:50:00 0.00 0.00 10.85 14.39 16	3.28 11.49 7.85 23.12 3.37 48.40 1.09 50.08 4.96 43.60	13.30 26.30	14.38	
0:25:00 0.00 0.00 23.32 31.10 37 0:30:00 0.00 0.00 24.74 32.66 38 0:35:00 0.00 0.00 20.71 26.69 31 0:40:00 0.00 0.00 17.07 21.50 24 0:45:00 0.00 0.00 13.27 17.12 20 0:50:00 0.00 0.00 10.85 14.39 16	7.85 23.12 8.37 48.40 1.09 50.08 4.96 43.60	26.30		
0:30:00 0.00 0.00 24.74 32.66 38 0:35:00 0.00 0.00 20.71 26.69 31 0:40:00 0.00 0.00 17.07 21.50 24 0:45:00 0.00 0.00 13.27 17.12 20 0:50:00 0.00 0.00 10.85 14.39 16	3.37 48.40 1.09 50.08 4.96 43.60			20.92
0:35:00 0.00 0.00 20.71 26.69 31 0:40:00 0.00 0.00 17.07 21.50 24 0:45:00 0.00 0.00 13.27 17.12 20 0:50:00 0.00 0.00 10.85 14.39 16	1.09 50.08 4.96 43.60	59.17	28.45	43.77
0:40:00 0.00 0.00 17.07 21.50 24 0:45:00 0.00 0.00 13.27 17.12 20 0:50:00 0.00 0.00 10.85 14.39 16	4.96 43.60		68.08	108.88
0:45:00 0.00 0.00 13.27 17.12 20 0:50:00 0.00 0.00 10.85 14.39 16		60.54	75.04	116.90
0:50:00 0.00 0.00 10.85 14.39 16	0.00 34.95	52.71	64.82	101.09
	C 40 20 E0	42.02	53.79	84.41
	5.48 28.59 3.77 22.60	34.04 26.72	42.90 34.46	67.88 54.68
	1.45 18.19	21.31	28.56	45.45
	.66 14.72	17.09	23.76	38.02
	.87 11.15	12.73	16.76	26.22
	.63 9.27	10.52	12.74	19.67
1:20:00 0.00 0.00 4.13 6.05 7.	.92 7.71	8.71	9.54	14.46
1:25:00 0.00 0.00 3.92 5.66 6.	.93 6.79	7.65	7.53	11.14
	.26 5.83	6.56	6.37	9.23
	.81 5.22	5.87	5.58	7.94
	4.82	5.42	5.07	7.10
	.32 4.56 .17 4.41	5.12 4.96	4.76 4.65	6.59 6.44
	.17 4.41 .91 4.32	4.96	4.60	6.36
	.40 4.28	4.80	4.60	6.36
	.92 2.84	3.19	3.05	4.22
	.89 1.85	2.07	1.98	2.73
	.20 1.18	1.32	1.26	1.73
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	.21 0.23	0.25	0.24	0.32
	.08 0.08	0.09	0.09	0.11
	.01 0.01	0.01	0.01	0.00
	.00 0.00	0.00	0.00	0.00
	.00 0.00	0.00	0.00	0.00
	0.00 0.00	0.00	0.00	0.00
	.00 0.00	0.00	0.00	0.00
	.00 0.00	0.00	0.00	0.00
	.00 0.00	0.00	0.00	0.00
3:20:00 0.00 0.00 0.00 0.00 0.	.00 0.00	0.00	0.00	0.00
3:25:00 0.00 0.00 0.00 0.00 0.	.00 0.00	0.00	0.00	0.00
	.00 0.00	0.00	0.00	0.00
	.00 0.00	0.00	0.00	0.00
	.00 0.00	0.00	0.00	0.00
	.00 0.00	0.00	0.00	0.00
	.00 0.00	0.00	0.00	0.00
	0.00 0.00	0.00	0.00	0.00
	.00 0.00	0.00	0.00	0.00
4:10:00 0.00 0.00 0.00 0.00 0.00	.00 0.00	0.00	0.00	0.00
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	0.00 0.00	0.00	0.00	0.00
4:35:00 0.00 0.00 0.00 0.00 0.00	.00 0.00	0.00	0.00	0.00
	.00 0.00	0.00	0.00	0.00
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MHFD-Detention, Version 4.04 (February 2021) Summary Stage-Area-Volume-Discharge Relationships

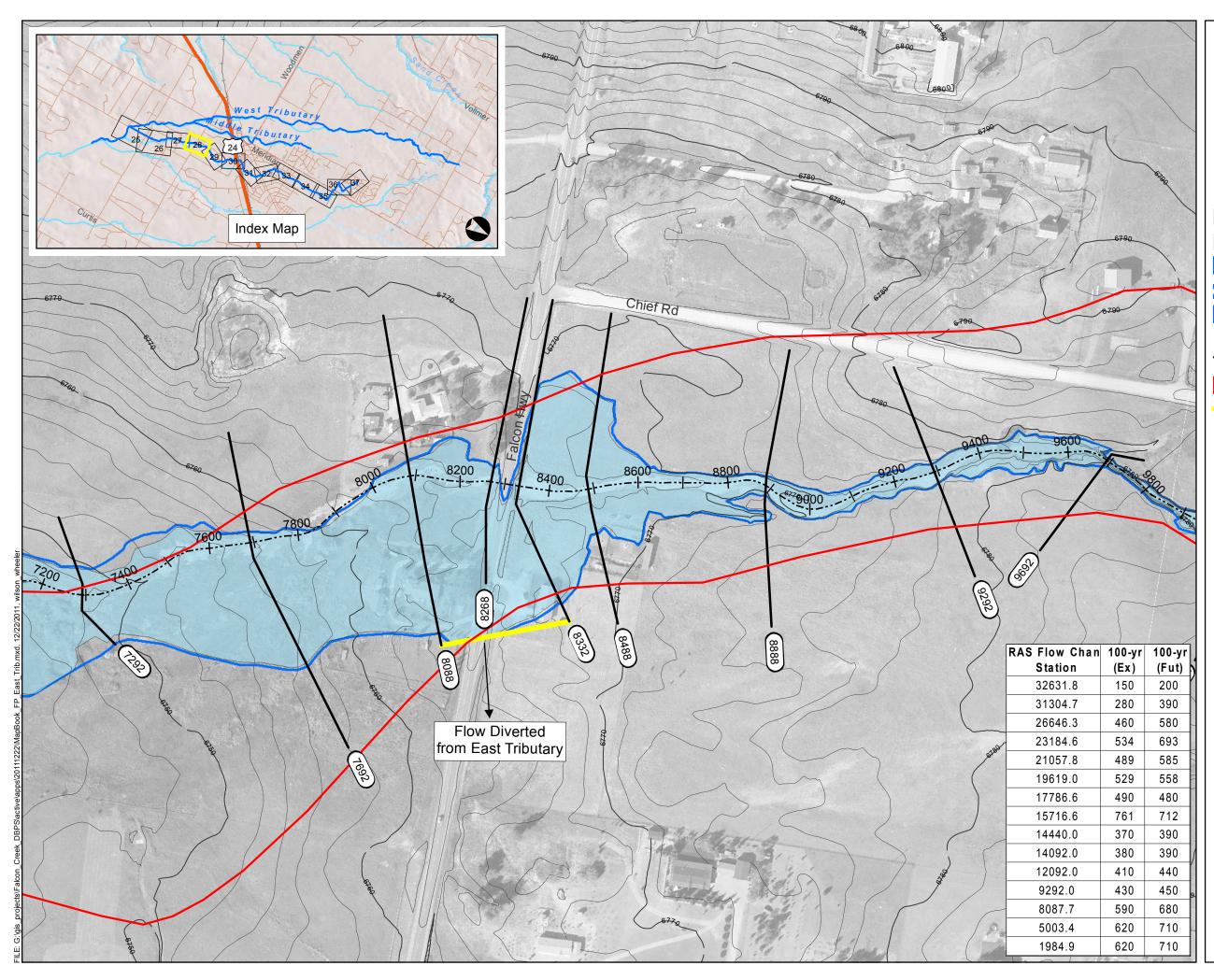
The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage [ft]	Area [ft ²]	Area [acres]	Volume [ft ³]	Volume [ac-ft]	Total Outflow [cfs]	
							For best results, include the
							stages of all grade slope
							changes (e.g. ISV and Floor from the S-A-V table on
							Sheet 'Basin'.
							Also include the inverts of a
							outlets (e.g. vertical orifice.
							overflow grate, and spillwa where applicable).
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DBPS Excerpts



clonts



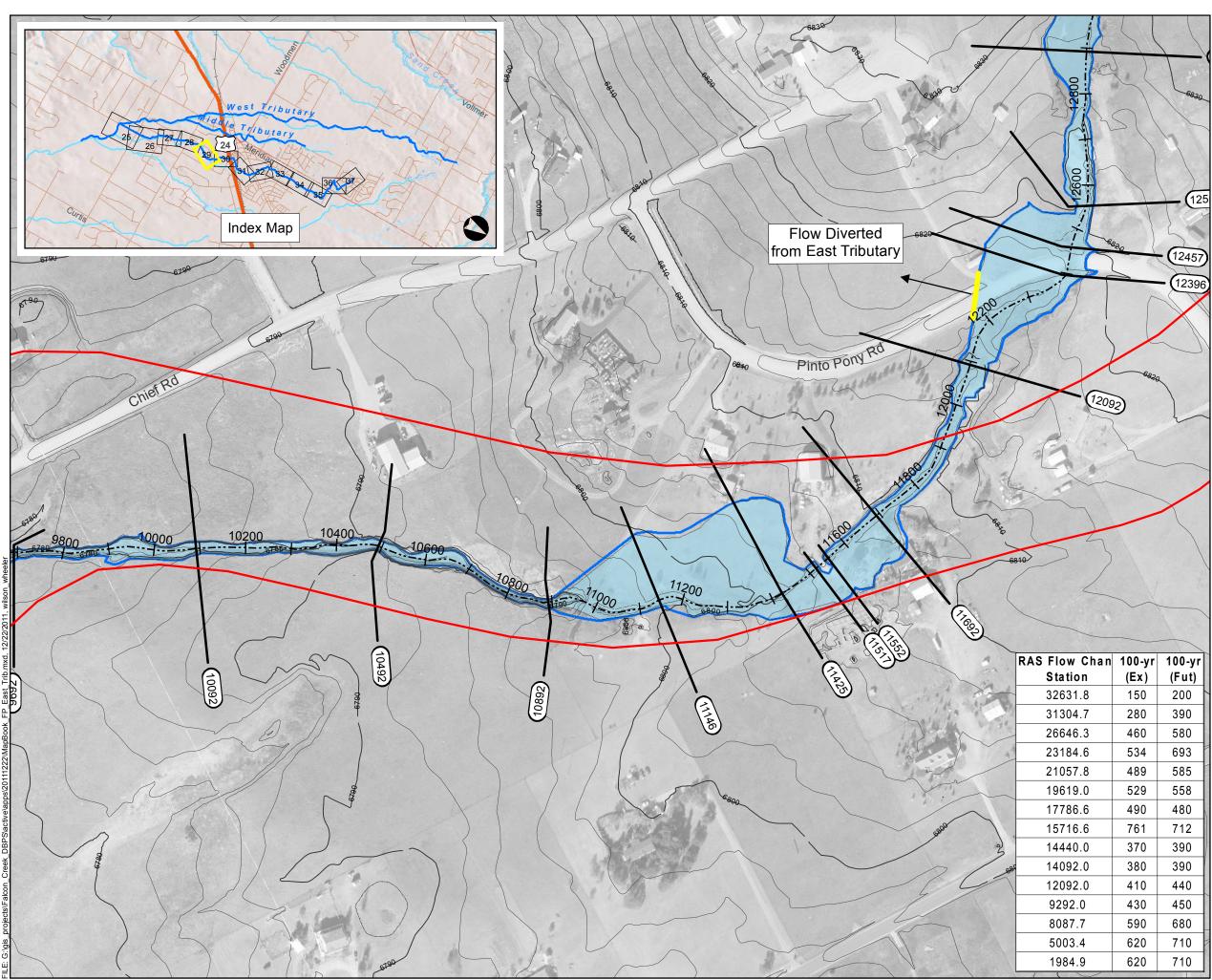
Sheet 4-28

East Tributary Floodplain Falcon DBPS El Paso County, CO

Legend



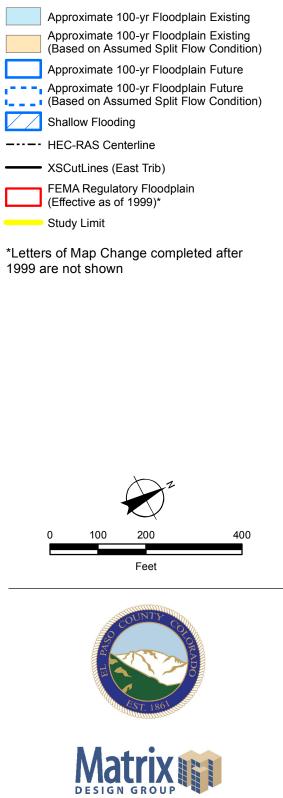


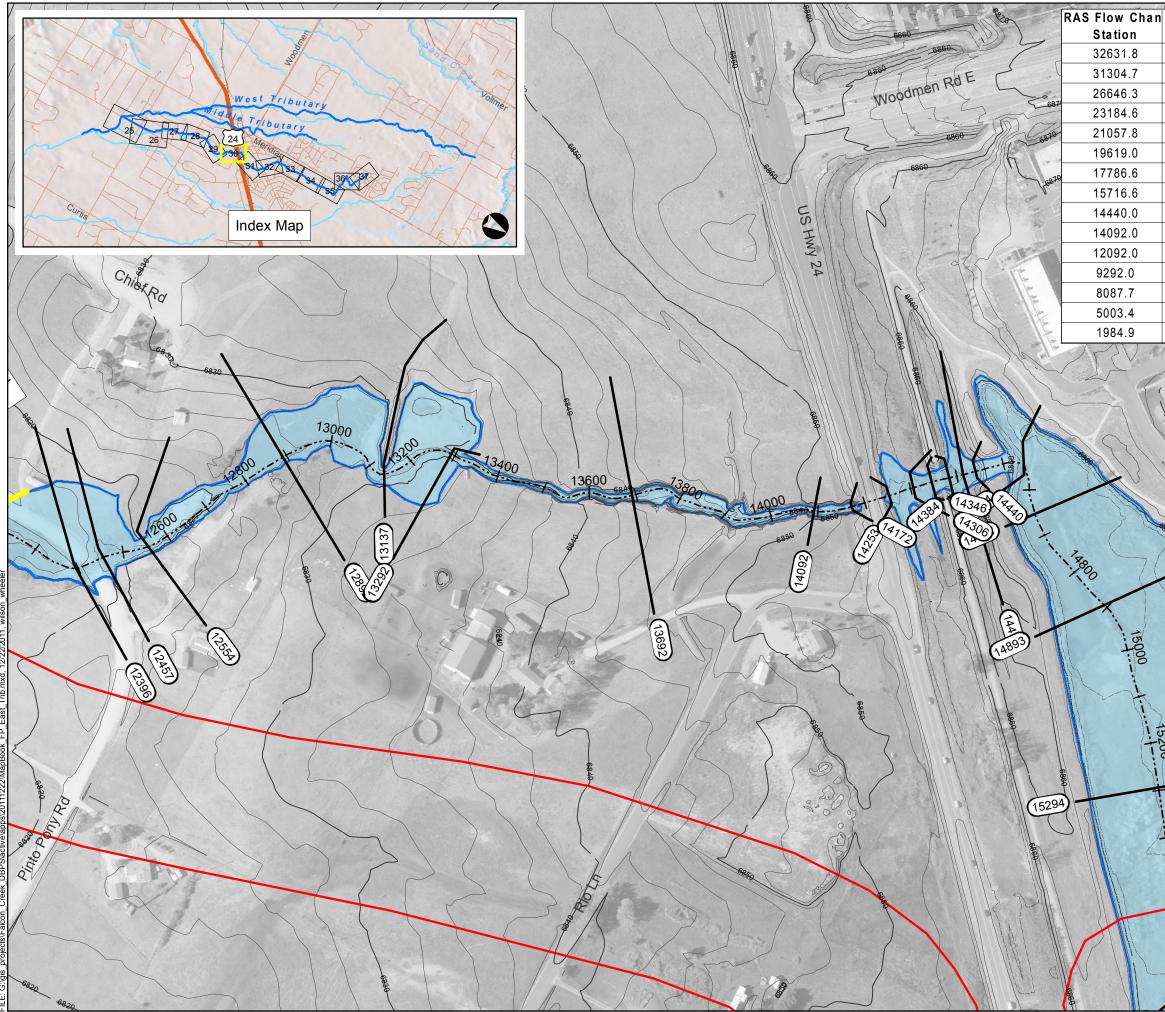


Sheet 4-29

East Tributary Floodplain Falcon DBPS El Paso County, CO

Legend





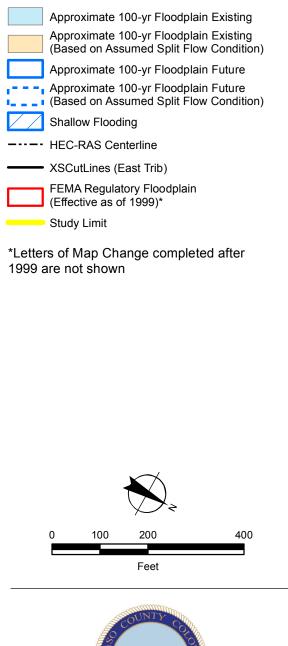
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534	693
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Sheet 4-30

East Tributary Floodplain Falcon DBPS El Paso County, CO

Legend



Matrix III

CLOMR Excerpts

REQUEST FOR CONDITIONAL LETTER OF MAP REVISION UNNAMED TRIBUTARY TO BLACK SQUIRREL CREEK FALCON FIELD

1.0 INTRODUCTION

1.1 Background

The following report and supporting documentation are being submitted to FEMA for the purpose of requesting a Conditional Letter of Map Revision (CLOMR) for a portion of the Unnamed Tributary to Black Squirrel Creek (UTBSC) in El Paso County, Colorado.

Falcon Field consists of approximately 57 acres adjacent to and southeast of Highway 24 near Rio Lane as shown in **Figure 1**. The UTBSC flows southeast across the property and is proposed to be contained within an 8'x4' box culvert and open channel that will discharge into the existing tributary. A general site layout of the Falcon Field development is shown in the construction drawings included in **Appendix 1**.

The improvements associated with Falcon Field are in general conformance with the Falcon Basin, Drainage Basin Planning Study (Falcon DBPS), prepared by El Paso County in 2015. The hydrologic analysis completed for the Falcon DBPS was used as the basis for the current CLOMR.

The Effective FEMA Flood Insurance Rate Map (FIRM) Numbers 08041C0553G and 08041C0561G in **Appendix 5** show the UTBSC 100-year Zone A floodplain across the center of the Falcon Field. This report includes detailed hydraulic models showing that the proposed 100-year floodplain will be contained within a proposed box culvert and open channel.

It is the Owner/Developer's intent to comply with all floodplain regulations.

1.2 General Location and Project Description

This CLOMR is limited to the 57-acre parcel located at the southwest corner of Highway 24 and Rio Lane, in the east half of Section 7, Township 13 South, Range 64 West of the 6th P.M. in El Paso County, Colorado. The subject property will be developed with a mixed-use commercial and residential development (Falcon Field).

The Falcon Field development includes regrading the site and containing the UTBSC across the site. Approximately 1024 feet of the tributary will be impacted by the development, which intercepts the existing creek south of Highway 24 and conveys it via an 8'x4' box culvert and open channel to the existing creek downstream. The box culvert and open channel are designed to convey the full 100-year discharge.

REQUEST FOR CONDITIONAL LETTER OF MAP REVISION UNNAMED TRIBUTARY TO BLACK SQUIRREL CREEK, FALCON FIELD



Figure 1 – Vicinity Map

1.3 Regulatory Floodplain

The Effective Zone A limits for the UTBSC on the Falcon Field site are defined on Map Numbers 8041C0553G and 08041C0561G dated December 7, 2018. No flow rates, floodway data or flood profiles were defined for this section of UTBSC in the effective FIS for El Paso County, Colorado, Revised December 7, 2018.

2.0 PREVIOUS STUDIES

El Paso County completed hydrologic and hydraulic analyses summarized in a report titled Falcon Basin, Drainage Basin Planning Study, Selected Plan Report, Final, September 2015 (Falcon DBPS). The Falcon DBPS encompasses three unnamed tributaries to Black Squirrel Creek, including the "East Tributary" which flows across the subject property. Select output from the Falcon DBPS is included in **Appendix 2**.

3.0 HYDROLOGIC ANALYSIS

The Falcon DBPS completed hydrologic analysis for the Falcon Basin Watershed, using HEC-HMS v3.5 software, for historical, existing, and future land use conditions by applying a 24-hour storm event with 2-, 5-, 10-, 25-, 50-, and 100-year recurrence intervals and current drainage infrastructure. Chapter 3 and Appendix A of the Falcon DBPS include a detailed discussion of the hydrologic analysis. An electronic copy of the HEC-HMS model (File: Aug15_Working_Falcon_DBPS_S.hms) is also provided.

El Paso County requires regional drainage infrastructure to be sized for future land use conditions. Therefore, peak discharges with existing drainage infrastructure and future land use conditions near Falcon Field are summarized in Table 3-1.

Last Hibatary, Falcon DDFS			
Model Location	Physical Location	Proximity to Falcon Field	Q100 (cfs)
JET090	Highway 24	Upstream of	390

Pinto Pony

Road

Table 3-1. Future Land Use Conditions Peak Discharges near Falcon Field on theEast Tributary, Falcon DBPS

Site

Downstream

of Site

390

4.0 HYDRAULIC ANALYSIS

JET100

4.1 General

The effective FIRM identifies an approximate Zone A floodplain across the Falcon Field property with no flood profiles, discharges, or BFE's defined. The Falcon Field development includes filling and regrading the site and rerouting the UTBSC through a box culvert and open channel across the site.

4.2 Vertical Datum

The effective FIRM is on the North American Vertical Datum of 1988 (NAVD88). The survey completed for the site, the design and construction drawings, and the hydraulic analysis completed for this CLOMR are all on the NAVD88. The Falcon DBPS was completed on the NGVD29.

4.3 Horizontal Datum

The field survey, design, construction drawings and hydraulic modeling for the Falcon Field project were completed on the North American Datum of 1983 (NAD83), Colorado State Plane coordinate system, Central Zone.

4.4 Box Culvert Hydraulic Analysis

Under existing conditions, the UTBSC discharges to an open channel through the site from 2-12'H x 4.83'W box culverts under Highway 24. The Falcon Field property limits are approximately 46 feet downstream of the Highway 24 box culvert exit. There is an 8-foot concrete vertical wall/drop immediately downstream of the culvert, then a short riprap channel section (shown in the photo below), before the open channel returns to a vegetated

REQUEST FOR CONDITIONAL LETTER OF MAP REVISION UNNAMED TRIBUTARY TO BLACK SQUIRREL CREEK, FALCON FIELD

section through the site. This section of the tributary was realigned with the construction of the upstream railroad and highway and does not follow the historic flow path.



Existing 2-12'H x 4.83' W box culverts under Highway 24

The proposed 8' x 4' box culvert will begin at the upstream property boundary (approximately the fence line shown in the photo above) at a headwall and convey the tributary flows 750 feet downstream to a proposed open channel. StormCAD was used to evaluate the hydraulic performance of the box culvert. The profile and output for the 100-year storm event is included in **Appendix 3**, and the model files are provided.

4.5 Open Channel Hydraulic Analysis

The proposed box culvert discharges to a proposed open channel via a headwall. The proposed open channel conveys the UTBSC 275 feet downstream to the existing creek, and will be vegetated with mowable short grasses. The open channel has a 20-foot bottom width in a v-shape with two 10-foot sections set at a 2% slope to the invert. The side slopes above the v-shape bottom are set at a 3H:1V slope. HEC-RAS version 6.2 was used to model the proposed open channel and existing creek downstream. The profile and output for the 100-year storm event is included in **Appendix 3**, and the model files are provided.

The proposed geometry includes six cross sections over a modeled reach of 400 feet. Roughness coefficients (n-values) of 0.04 and 0.08 were used for the proposed and existing channel, respectively. The model was computed in a subcritical flow regime for the design flow of 390 cfs, with a normal depth starting water surface elevation.

5.0 NFIP REGULATION COMPLIANCE

5.1 Floodplain Work Map and Annotated FIRM

The effective Zone A 100-year floodplain delineation for the UTBSC begins downstream of Highway 24. The 100-year flood discharge will be contained in the proposed box culvert. The proposed floodplain for the on-site open channel is delineated on the Floodplain Work Map and Annotated FIRM in **Appendix 5**. The proposed Zone AE floodplain ties into the effective Zone A floodplain approximately 225 feet downstream of the Falcon Field downstream property limits.

5.2 Forms and Notifications

The appropriate FEMA forms are located in **Appendix 4**. Modifications to 100-year floodplain elevations and delineations are limited to the Falcon Field development. Furthermore, there are no proposed increases to the BFE's or floodplain extents. Therefore, individual legal notices are not required for this CLOMR submittal.

5.3 Compliance with Section 65.12

Although there are no increases to BFE's due to the proposed project, an alternatives evaluation was performed to evaluate options for closed conduit and open channel conveyance of the UTBSC. The alternatives evaluation can be provided upon request.

Furthermore, no structures are located in areas that would be impacted by the floodplain modifications proposed by this CLOMR.

5.4 Endangered Species Act (ESA)

ESA Compliance information is provided in Appendix 6.

6.0 CONCLUSIONS

The Falcon Field development will relocate a portion of an Unnamed Tributary to Black Squirrel Creek (East Tributary). This report and supporting documentation are being submitted to FEMA for the purpose of requesting a CLOMR to conditionally change the floodplain in accordance with NFIP regulations.

7.0 **REFERENCES**

Bentley (formerly Haestad Methods, Inc.), StormCAD v4.1.1.

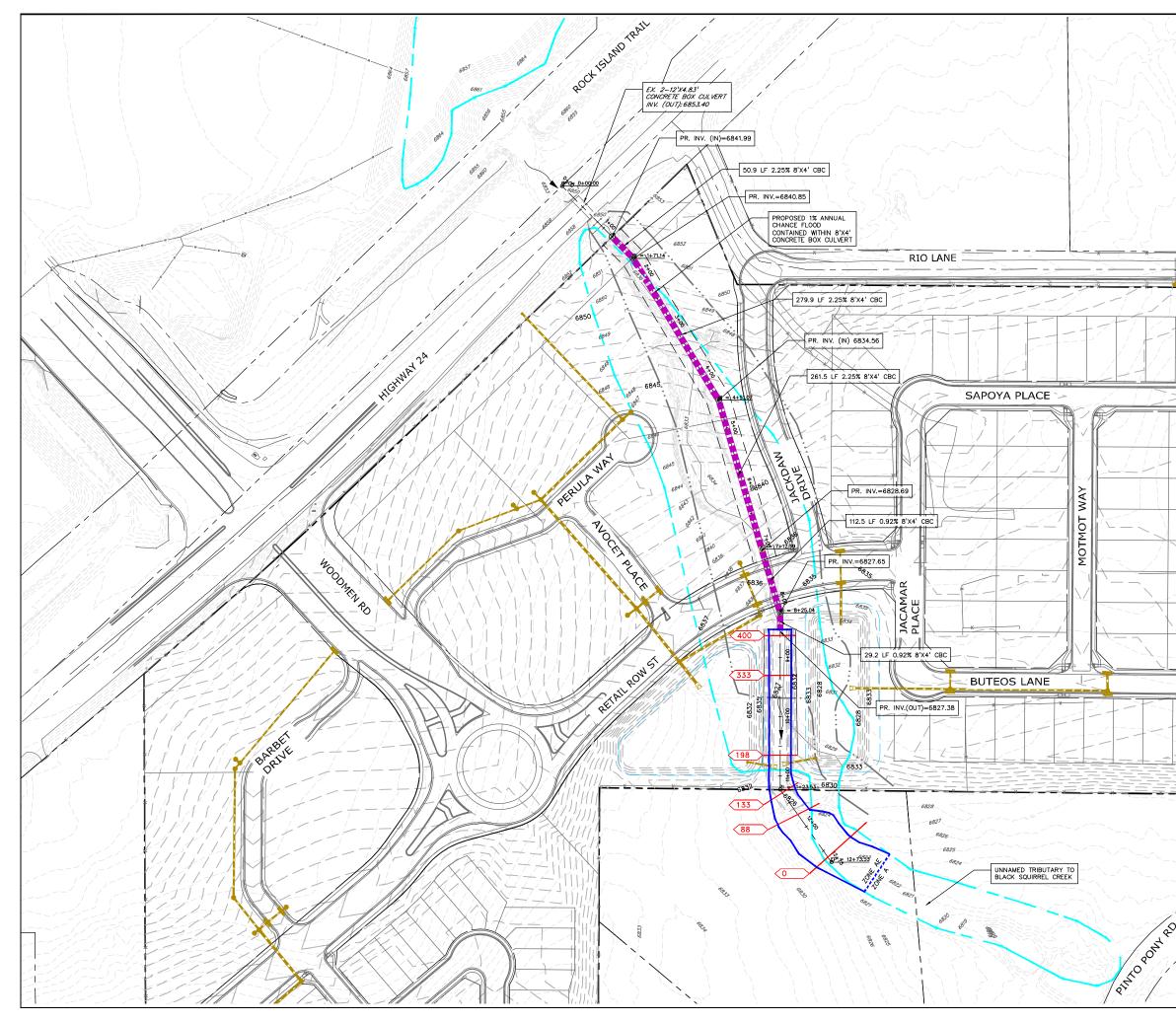
El Paso County, Drainage Criteria Manual, October 2018.

FEMA, FIRM Numbers 08041C0553G and 08041C0561G, El Paso County, Colorado and Incorporated Areas, Revised December 7, 2018.

FEMA, FIS Number 08041CV001A, El Paso County, Colorado and Incorporated Areas, Revised December 7, 2018.

Matrix Design Group, Falcon Drainage Basin Planning Study, Selected Plan Report, Final, September 2015.

USACE, Hydrologic Engineering Center River Analysis System (HEC-RAS), Version 6.2, March 2022.



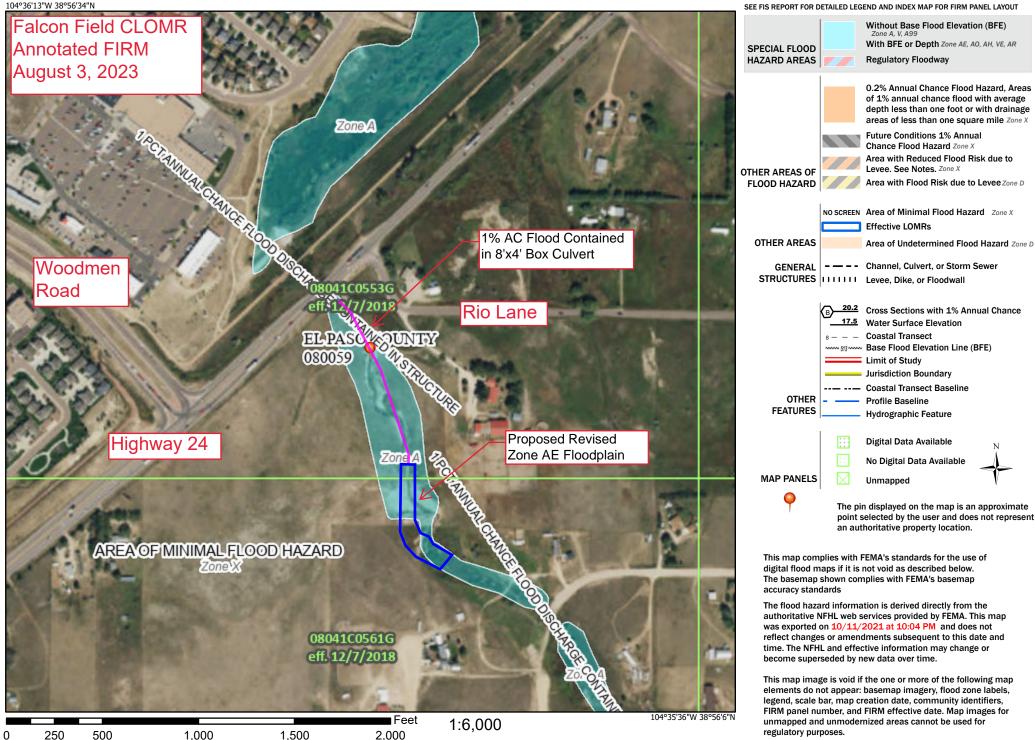
/			PREPARED) BY:
	LEGEND EX. CONTOUR PR. CONTOUR EX. STORM SEWER OR PR. CBC STORM SEWER PR. ON-SITE STORM DRAIN EFFECTIVE FEMA FLOODPLAN (ZONE A) PROPOSED FLOODPLAIN (ZONE AE) CROSS SECTION CROSS SECTION LABEL FLOW DIRECTION		PREPARED BY: DREXEI, BATTEII & Co. Treasel, Barrell & Co. Engineers •Surveyors 1376 MINERS DRIVE, STE 107 LAFAYETTE, COLORADO SOROZÓ CONTACT: MICHELLE IBLINGS, P.E. (303) 442-4338 LAFAYETTE COLORADO SPRINGS OWNER/CLIENT: PJ ANDERSON FALCON FIELD, LLC 3230 ELECTRA DR. N COLORADO SPRINGS, CO 80906	
	PR. ON-SITE DETENTION PR. EASEMENT PR. LOT EX. PROPERTY LINE PR. SITE BOUNDARY PROPOSED CURB LINE & SIDEWALK NOTES 1. SPATIAL PROJECTION IS STATE PLANE, CENTRAL			
>	2. VERTICAL DATUM IS NAV		EXHIBIT FOR: FALCON FIELI	FALCON, COLORADO
			ISSUE EXHIBIT	DATE 8/3/23
			DESIGNED BY: DRAWN BY: CHECKED BY: FILE NAME: 2170: RADO L/ OCCUPATION OF A 43515	
	80 40 C	ALE IN FEET	DRAWING SI HORIZONTAL: VERTICAL: CLOM FLOODP WORK M PROJECT:21705 DRAWING NO.	SEE PLAN N/A R LAIN MAP 5-00BLWR

National Flood Hazard Layer FIRMette



Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020



DEPARTMENT OF THE ARMY CORPS OF ENGINEERS, ALBUQUERQUE DISTRICT SOUTHERN COLORADO REGULATORY BRANCH 201 WEST 8TH STREET, SUITE 350 PUEBLO, COLORADO 81003

August 26, 2022

Regulatory Division

SUBJECT: Jurisdictional Determination - Action No. SPA-2021-00180, Falcon Field

P. J. Anderson Falcon Field, LLC 31 North Tejon Street, Suite 516 Colorado Springs, CO 80903 pja5713@gmail.com

Dear P.J. Anderson:

This letter responds to your request for a jurisdictional determination (JD) for property located at latitude 38.936555635255, longitude -104.600429740897, in El Paso County, Colorado. We have assigned Action No. SPA-2021-00180 to your request. Please reference this number in all future correspondence concerning the site.

Based on the information provided, we have determined that the site does not contain waters of the United States that are subject to regulation under Section 404 of the Clean Water Act. The attached JD form describes the area that was evaluated and determined to contain no waters of the United States. If you intend to conduct work that could result in a discharge of dredged or fill material into waters of the United States, please contact this office for a determination of Department of the Army permit requirements and refer to Action No. SPA-2021-00180.

The basis for this approved JD (attached) is that the project site contains isolated wetlands and/or other waters. Wetland 1 through 5 are intrastate, isolated waters that do not flow into a traditional navigable waterway (attached). A copy of this JD is also available at <u>http://www.spa.usace.army.mil/reg/JD</u>. This approved JD is valid for 5 years unless new information warrants revision of the determination before the expiration date.

You may accept or appeal this approved JD or provide new information in accordance with the attached Notification of Administration Appeal Options and Process and Request for Appeal. If you elect to appeal this approved JD, you must complete Section II of the form and return it to the Army Engineer Division, South Pacific, CESPD-PDS-O, Attn: Travis Morse, Administrative Appeal Review Officer, P.O. Box 36023, 450 Golden Gate Avenue, San Francisco, CA 94102 within 60 days of the date of this notice. Failure to notify the Corps within 60 days of the date of this notice means that you accept the approved JD in its entirety and waive all rights to appeal the approved JD.

If you have any questions, please contact Kraig Jashinsky at (719) 439-7281 or by email at Kraig.A.Jashinsky@usace.army.mil. At your convenience, please complete a Customer Service Survey online at <u>https://regulatory.ops.usace.army.mil/customer-service-survey/</u>.

Sincerely,

Kara A. Hellige Chief, Southern Colorado Regulatory Branch

CC:

Daniel Maynard, Bristlecone Ecology, LLC, <u>dmaynard@bristleconeecology.com</u>

APPROVED JURISDICTIONAL DETERMINATION FORM U.S. Army Corps of Engineers

This form should be completed by following the instructions provided in Section IV of the JD Form Instructional Guidebook.

SECTION I: BACKGROUND INFORMATION

A. REPORT COMPLETION DATE FOR APPROVED JURISDICTIONAL DETERMINATION (JD): August 26, 2022

B. DISTRICT OFFICE, FILE NAME, AND NUMBER: Albuquerque District, Falcon Field AJD Request, SPA-2021-00180

C. PROJECT LOCATION AND BACKGROUND INFORMATION:

State: Colorado County/parish/borough: El Paso County City:

Center coordinates of site (lat/long in degree decimal format): Lat. 38.936555635255°, Long. -104.600429740897°

Universal Transverse Mercator: 13 534630.43 4309812.02

Name of nearest waterbody: Jimmy Camp Creek

Name of nearest Traditional Navigable Water (TNW) into which the aquatic resource flows:

Name of watershed or Hydrologic Unit Code (HUC): Chico, 11020004

Check if map/diagram of review area and/or potential jurisdictional areas is/are available upon request.

Check if other sites (e.g., offsite mitigation sites, disposal sites, etc...) are associated with this action and are recorded on a different JD form:

D. REVIEW PERFORMED FOR SITE EVALUATION (CHECK ALL THAT APPLY):

Office (Desk) Determination. Date: July 14, 2022

Field Determination. Date(s): June 28, 2022

SECTION II: SUMMARY OF FINDINGS

A. RHA SECTION 10 DETERMINATION OF JURISDICTION.

There Are no "navigable waters of the U.S." within Rivers and Harbors Act (RHA) jurisdiction (as defined by 33 CFR part 329) in the review area. [Required]

Waters subject to the ebb and flow of the tide.

Waters are presently used, or have been used in the past, or may be susceptible for use to transport interstate or foreign commerce. Explain:

B. CWA SECTION 404 DETERMINATION OF JURISDICTION.

There Are no "waters of the U.S." within Clean Water Act (CWA) jurisdiction (as defined by 33 CFR part 328) in the review area. [Required]

1. Waters of the U.S.

- a. Indicate presence of waters of U.S. in review area (check all that apply): ¹
 - TNWs, including territorial seas
 - Wetlands adjacent to TNWs
 - Relatively permanent waters² (RPWs) that flow directly or indirectly into TNWs
 - Non-RPWs that flow directly or indirectly into TNWs
 - Wetlands directly abutting RPWs that flow directly or indirectly into TNWs
 - Wetlands adjacent to but not directly abutting RPWs that flow directly or indirectly into TNWs
 - Wetlands adjacent to non-RPWs that flow directly or indirectly into TNWs
 - Impoundments of jurisdictional waters
 - Isolated (interstate or intrastate) waters, including isolated wetlands
- b. Identify (estimate) size of waters of the U.S. in the review area:
 - Non-wetland waters: linear feet, wide, and/or acres. Wetlands: acres.
- c. Limits (boundaries) of jurisdiction based on: Pick List Elevation of established OHWM (if known):
- 2. Non-regulated waters/wetlands (check if applicable):³

Potentially jurisdictional waters and/or wetlands were assessed within the review area and determined to be not jurisdictional. Explain: The review area contains five wetlands totalling 7.15 acres. A review of the downstream connectivity of the associated wetlands found there to be a lack of a connection to downstream waters. The drainage features and associated wetlands presented a southward flow path until reaching E. Blaney Road. The flow path consisting of a varying degree of broken stream channel and connected wetlands terminated across a portion of flat terrain with not apparent wetland vegetation. Flow does not appear to reach any downstream waters via the nearby roadside ditch. Flow also does not cross E. Blaney Road due to the lack of culverts and a slight elevation rise. Due to a lack of downstream connectivity, the drainage features and associated wetlands under review are found to be isolated.

¹ Boxes checked below shall be supported by completing the appropriate sections in Section III below.

² For purposes of this form, an RPW is defined as a tributary that is not a TNW and that typically flows year-round or has continuous flow at least "seasonally" (e.g., typically 3 months).

³ Supporting documentation is presented in Section III.F.

SECTION III: CWA ANALYSIS

A. TNWs AND WETLANDS ADJACENT TO TNWs

The agencies will assert jurisdiction over TNWs and wetlands adjacent to TNWs. If the aquatic resource is a TNW, complete Section III.A.1 and Section III.D.1. only; if the aquatic resource is a wetland adjacent to a TNW, complete Sections III.A.1 and 2 and Section III.D.1.; otherwise, see Section III.B below.

1. TNW

Identify TNW:

Summarize rationale supporting determination:

2. Wetland adjacent to TNW

Summarize rationale supporting conclusion that wetland is "adjacent":

B. CHARACTERISTICS OF TRIBUTARY (THAT IS NOT A TNW) AND ITS ADJACENT WETLANDS (IF ANY):

This section summarizes information regarding characteristics of the tributary and its adjacent wetlands, if any, and it helps determine whether or not the standards for jurisdiction established under *Rapanos* have been met.

The agencies will assert jurisdiction over non-navigable tributaries of TNWs where the tributaries are "relatively permanent waters" (RPWs), i.e. tributaries that typically flow year-round or have continuous flow at least seasonally (e.g., typically 3 months). A wetland that directly abuts an RPW is also jurisdictional. If the aquatic resource is not a TNW, but has year-round (perennial) flow, skip to Section III.D.2. If the aquatic resource is a wetland directly abutting a tributary with perennial flow, skip to Section III.D.4.

A wetland that is adjacent to but that does not directly abut an RPW requires a significant nexus evaluation. Corps districts and EPA regions will include in the record any available information that documents the existence of a significant nexus between a relatively permanent tributary that is not perennial (and its adjacent wetlands if any) and a traditional navigable water, even though a significant nexus finding is not required as a matter of law.

If the waterbody⁴ is not an RPW, or a wetland directly abutting an RPW, a JD will require additional data to determine if the waterbody has a significant nexus with a TNW. If the tributary has adjacent wetlands, the significant nexus evaluation must consider the tributary in combination with all of its adjacent wetlands. This significant nexus evaluation that combines, for analytical purposes, the tributary and all of its adjacent wetlands is used whether the review area identified in the JD request is the tributary, or its adjacent wetlands, or both. If the JD covers a tributary with adjacent wetlands, complete Section III.B.1 for the tributary, Section III.B.2 for any onsite wetlands, and Section III.B.3 for all wetlands adjacent to that tributary, both onsite and offsite. The determination whether a significant nexus exists is determined in Section III.C below.

1. Characteristics of non-TNWs that flow directly or indirectly into TNW

(i) General Area Conditions:

Watershed size:	Pick List	
Drainage area:	Pick List	
Average annual rain	nfall: inches	
Average annual sno	owfall: inches	s

(ii) Physical Characteristics:

(a) <u>Relationship with TNW:</u>
 ☐ Tributary flows directly into TNW.
 ☐ Tributary flows through **Pick List** tributaries before entering TNW.

Project waters are Pick List river miles from TNW.
Project waters are Pick List river miles from RPW.
Project waters are Pick List aerial (straight) miles from TNW.
Project waters are Pick List aerial (straight) miles from RPW.
Project waters cross or serve as state boundaries. Explain:

Identify flow route to TNW⁵: Tributary stream order, if known:

⁴ Note that the Instructional Guidebook contains additional information regarding swales, ditches, washes, and erosional features generally and in the arid West.

⁵ Flow route can be described by identifying, e.g., tributary a, which flows through the review area, to flow into tributary b, which then flows into TNW.

- 3 -	
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	(b)	General Tributary Characteristics (check all that apply): Tributary is: Natural Artificial (man-made). Explain: Manipulated (man-altered). Explain:
		Tributary properties with respect to top of bank (estimate): Average width: feet Average depth: feet Average side slopes: Pick List.
		Primary tributary substrate composition (check all that apply):
		Tributary condition/stability [e.g., highly eroding, sloughing banks]. Explain: Presence of run/riffle/pool complexes. Explain: Tributary geometry: Pick List Tributary gradient (approximate average slope): %
	(c)	<u>Flow:</u> Tributary provides for: Pick List Estimate average number of flow events in review area/year: Pick List Describe flow regime: Other information on duration and volume:
		Surface flow is: Pick List. Characteristics:
		Subsurface flow: Pick List. Explain findings: Dye (or other) test performed:
		Tributary has (check all that apply): Bed and banks OHWM ⁶ (check all indicators that apply): the presence of litter and debris clear, natural line impressed on the bank the presence of litter and debris changes in the character of soil destruction of terrestrial vegetation shelving the presence of wrack line vegetation matted down, bent, or absent sediment sorting leaf litter disturbed or washed away scour sediment deposition multiple observed or predicted flow events water staining abrupt change in plant community other (list): Discontinuous OHWM. ⁷ Explain:
		If factors other than the OHWM were used to determine lateral extent of CWA jurisdiction (check all that apply): High Tide Line indicated by: Mean High Water Mark indicated by: oil or scum line along shore objects survey to available datum; fine shell or debris deposits (foreshore) physical markings/characteristics tidal gauges other (list):
(iii)	Cha E	e mical Characteristics: aracterize tributary (e.g., water color is clear, discolored, oily film; water quality; general watershed characteristics, etc.). Explain: ntify specific pollutants, if known:
(iv)	Bio	logical Characteristics. Channel supports (check all that apply): Riparian corridor. Characteristics (type, average width): Wetland fringe. Characteristics: Habitat for:

⁶A natural or man-made discontinuity in the OHWM does not necessarily sever jurisdiction (e.g., where the stream temporarily flows underground, or where the OHWM has been removed by development or agricultural practices). Where there is a break in the OHWM that is unrelated to the waterbody's flow regime (e.g., flow over a rock outcrop or through a culvert), the agencies will look for indicators of flow above and below the break. ⁷Ibid.

Federally Listed species. Explain findings:

Fish/spawn areas. Explain findings:

Other environmentally-sensitive species. Explain findings:

Aquatic/wildlife diversity. Explain findings:

2. Characteristics of wetlands adjacent to non-TNW that flow directly or indirectly into TNW

(i) Physical Characteristics:

- (a) <u>General Wetland Characteristics:</u> Properties: Wetland size: acres Wetland type. Explain: Wetland quality. Explain: Project wetlands cross or serve as state boundaries. Explain:
- (b) <u>General Flow Relationship with Non-TNW</u>: Flow is: **Pick List**. Explain:

Surface flow is: Pick List Characteristics:

Subsurface flow: **Pick List**. Explain findings: Dye (or other) test performed:

(c) <u>Wetland Adjacency Determination with Non-TNW:</u>

Directly abutting

□ Not directly abutting

Discrete wetland hydrologic connection. Explain:

- Ecological connection. Explain:
- Separated by berm/barrier. Explain:

(d) <u>Proximity (Relationship) to TNW</u>

Project wetlands are Pick List river miles from TNW.
Project waters are Pick List aerial (straight) miles from TNW.
Flow is from: Pick List.
Estimate approximate location of wetland as within the Pick List floodplain.

(ii) Chemical Characteristics:

Characterize wetland system (e.g., water color is clear, brown, oil film on surface; water quality; general watershed characteristics; etc.). Explain:

Identify specific pollutants, if known:

(iii) Biological Characteristics. Wetland supports (check all that apply):

- Riparian buffer. Characteristics (type, average width):
- Vegetation type/percent cover. Explain:

Habitat for:

- Federally Listed species. Explain findings:
- Fish/spawn areas. Explain findings:
- Other environmentally-sensitive species. Explain findings:
- Aquatic/wildlife diversity. Explain findings:

3. Characteristics of all wetlands adjacent to the tributary (if any)

All wetland(s) being considered in the cumulative analysis: **Pick List** Approximately acres in total are being considered in the cumulative analysis.

For each wetland, specify the following:

Directly abuts? (Y/N) Size (in acres)

Directly abuts? (Y/N)

Size (in acres)

Summarize overall biological, chemical and physical functions being performed:

A significant nexus analysis will assess the flow characteristics and functions of the tributary itself and the functions performed by any wetlands adjacent to the tributary to determine if they significantly affect the chemical, physical, and biological integrity of a TNW. For each of the following situations, a significant nexus exists if the tributary, in combination with all of its adjacent wetlands, has more than a speculative or insubstantial effect on the chemical, physical and/or biological integrity of a TNW. Considerations when evaluating significant nexus include, but are not limited to the volume, duration, and frequency of the flow of water in the tributary and its proximity to a TNW, and the functions performed by the tributary and all its adjacent wetlands. It is not appropriate to determine significant nexus based solely on any specific threshold of distance (e.g. between a tributary and its adjacent wetland or between a tributary and the TNW). Similarly, the fact an adjacent wetland lies within or outside of a floodplain is not solely determinative of significant nexus.

Draw connections between the features documented and the effects on the TNW, as identified in the *Rapanos* Guidance and discussed in the Instructional Guidebook. Factors to consider include, for example:

- Does the tributary, in combination with its adjacent wetlands (if any), have the capacity to carry pollutants or flood waters to TNWs, or to reduce the amount of pollutants or flood waters reaching a TNW?
- Does the tributary, in combination with its adjacent wetlands (if any), provide habitat and lifecycle support functions for fish and other species, such as feeding, nesting, spawning, or rearing young for species that are present in the TNW?
- Does the tributary, in combination with its adjacent wetlands (if any), have the capacity to transfer nutrients and organic carbon that support downstream foodwebs?
- Does the tributary, in combination with its adjacent wetlands (if any), have other relationships to the physical, chemical, or biological integrity of the TNW?

Note: the above list of considerations is not inclusive and other functions observed or known to occur should be documented below:

- 1. Significant nexus findings for non-RPW that has no adjacent wetlands and flows directly or indirectly into TNWs. Explain findings of presence or absence of significant nexus below, based on the tributary itself, then go to Section III.D:
- 2. Significant nexus findings for non-RPW and its adjacent wetlands, where the non-RPW flows directly or indirectly into TNWs. Explain findings of presence or absence of significant nexus below, based on the tributary in combination with all of its adjacent wetlands, then go to Section III.D:
- **3.** Significant nexus findings for wetlands adjacent to an RPW but that do not directly abut the RPW. Explain findings of presence or absence of significant nexus below, based on the tributary in combination with all of its adjacent wetlands, then go to Section III.D:

D. DETERMINATIONS OF JURISDICTIONAL FINDINGS. THE SUBJECT WATERS/WETLANDS ARE (CHECK ALL THAT APPLY):

- TNWs and Adjacent Wetlands. Check all that apply and provide size estimates in review area:

 TNWs:
 linear feet,
 wide, Or
 acres.

 Wetlands adjacent to TNWs:
 acres.
- 2. RPWs that flow directly or indirectly into TNWs.
 - Tributaries of TNWs where tributaries typically flow year-round are jurisdictional. Provide data and rationale indicating that tributary is perennial:
 - Tributaries of TNW where tributaries have continuous flow "seasonally" (e.g., typically three months each year) are jurisdictional. Data supporting this conclusion is provided at Section III.B. Provide rationale indicating that tributary flows seasonally:

Provide estimates for jurisdictional waters in the review area (check all that apply):

- Tributary waters: linear feet wide.
- Other non-wetland waters: acres.

Identify type(s) of waters:

3. Non-RPWs⁸ that flow directly or indirectly into TNWs.

Ukaterbody that is not a TNW or an RPW, but flows directly or indirectly into a TNW, and it has a significant nexus with a TNW is jurisdictional. Data supporting this conclusion is provided at Section III.C.

Provide estimates for jurisdictional waters within the review area (check all that apply):

 Tributary waters: linear feet, wide.
 Other non-wetland waters: acres. Identify type(s) of waters:

- 5 -

Wetlands directly abutting an RPW that flow directly or indirectly into TNWs. 4.

Wetlands directly abut RPW and thus are jurisdictional as adjacent wetlands.

- Use Wetlands directly abutting an RPW where tributaries typically flow year-round. Provide data and rationale indicating that tributary is perennial in Section III.D.2, above. Provide rationale indicating that wetland is directly abutting an RPW:
- Wetlands directly abutting an RPW where tributaries typically flow "seasonally." Provide data indicating that tributary is seasonal in Section III.B and rationale in Section III.D.2, above. Provide rationale indicating that wetland is directly abutting an RPW:

Provide acreage estimates for jurisdictional wetlands in the review area: acres.

5. Wetlands adjacent to but not directly abutting an RPW that flow directly or indirectly into TNWs.

Wetlands that do not directly abut an RPW, but when considered in combination with the tributary to which they are adjacent and with similarly situated adjacent wetlands, have a significant nexus with a TNW are jurisidictional. Data supporting this conclusion is provided at Section III.C.

Provide acreage estimates for jurisdictional wetlands in the review area: acres.

Wetlands adjacent to non-RPWs that flow directly or indirectly into TNWs. 6.

Wetlands adjacent to such waters, and have when considered in combination with the tributary to which they are adjacent and with similarly situated adjacent wetlands, have a significant nexus with a TNW are jurisdictional. Data supporting this conclusion is provided at Section III.C.

Provide estimates for jurisdictional wetlands in the review area: acres.

Impoundments of jurisdictional waters.9 7.

- As a general rule, the impoundment of a jurisdictional tributary remains jurisdictional.
- Demonstrate that impoundment was created from "waters of the U.S.," or
- Demonstrate that water meets the criteria for one of the categories presented above (1-6), or

Demonstrate that water is isolated with a nexus to commerce (see E below).

E. ISOLATED [INTERSTATE OR INTRA-STATE] WATERS, INCLUDING ISOLATED WETLANDS, THE USE, DEGRADATION OR DESTRUCTION OF WHICH COULD AFFECT INTERSTATE COMMERCE, INCLUDING ANY SUCH WATERS (CHECK ALL THAT APPLY):10

which are or could be used by interstate or foreign travelers for recreational or other purposes.

- from which fish or shellfish are or could be taken and sold in interstate or foreign commerce.
- which are or could be used for industrial purposes by industries in interstate commerce.
- Interstate isolated waters. Explain:
- Other factors. Explain:

Identify water body and summarize rationale supporting determination:

Provide estimates for jurisdictional waters in the review area (check all that apply):

- Tributary waters: linear feet, wide. acres.
- Other non-wetland waters:
- Identify type(s) of waters:
- Wetlands: acres.

NON-JURISDICTIONAL WATERS, INCLUDING WETLANDS (CHECK ALL THAT APPLY): F.

- If potential wetlands were assessed within the review area, these areas did not meet the criteria in the 1987 Corps of Engineers Wetland Delineation Manual and/or appropriate Regional Supplements.
- Review area included isolated waters with no substantial nexus to interstate (or foreign) commerce.
 - Prior to the Jan 2001 Supreme Court decision in "SWANCC," the review area would have been regulated based solely on the "Migratory Bird Rule" (MBR).
- Waters do not meet the "Significant Nexus" standard, where such a finding is required for jurisdiction. Explain: Other: (explain, if not covered above):

⁹ To complete the analysis refer to the key in Section III.D.6 of the Instructional Guidebook.

¹⁰ Prior to asserting or declining CWA jurisdiction based solely on this category, Corps Districts will elevate the action to Corps and EPA HQ for review consistent with the process described in the Corps/EPA Memorandum Regarding CWA Act Jurisdiction Following Rapanos.

Provide acreage estimates for non-jurisdictional waters in the review area, where the <u>sole</u> potential basis of jurisdiction is the MBR factors (i.e., presence of migratory birds, presence of endangered species, use of water for irrigated agriculture), using best professional judgment (check all that apply):

Non-wetland waters (i.e., rivers, streams): linear feet, wide.

Lakes/ponds: acres.

 \boxtimes Other non-wetland waters: acres. List type of aquatic resource:

Wetlands: 7.15 acres.

Provide acreage estimates for non-jurisdictional waters in the review area that do not meet the "Significant Nexus" standard, where such a finding is required for jurisdiction (check all that apply):

Non-wetland waters (i.e., rivers, streams): linear feet, wide.

Lakes/ponds: acres.

- Other non-wetland waters: acres. List type of aquatic resource:
- Wetlands: acres.

SECTION IV: DATA SOURCES.

- A. SUPPORTING DATA. Data reviewed for JD (check all that apply checked items shall be included in case file and, where checked and requested, appropriately reference sources below):
 - Maps, plans, plots or plat submitted by or on behalf of the applicant/consultant: 2021-180 Falcon Field AJD Request 12-15-2020 29-Nov-21.pdf
 - Data sheets prepared/submitted by or on behalf of the applicant/consultant. Office concurs with data sheets/delineation report. Office does not concur with data sheets/delineation report. Data sheets prepared by the Corps: Corps navigable waters' study: U.S. Geological Survey Hydrologic Atlas: USGS NHD data. USGS 8 and 12 digit HUC maps. U.S. Geological Survey map(s). Cite scale & quad name: 1:24K; Falcon USDA Natural Resources Conservation Service Soil Survey. Citation: 2021-180 Soil Map National wetlands inventory map(s). Cite name: 2021-180 NWI Map State/Local wetland inventory map(s): FEMA/FIRM maps: 100-year Floodplain Elevation is: (National Geodectic Vertical Datum of 1929) Photographs: Aerial (Name & Date): 2021-180 Aerial - May 2020 or Other (Name & Date): Previous determination(s). File no. and date of response letter: Applicable/supporting case law: Applicable/supporting scientific literature: \boxtimes Other information (please specify): 2021-180 EPA Watershed Report, 2021-180 Flow Path and Pictures, 2021-180 Inspection

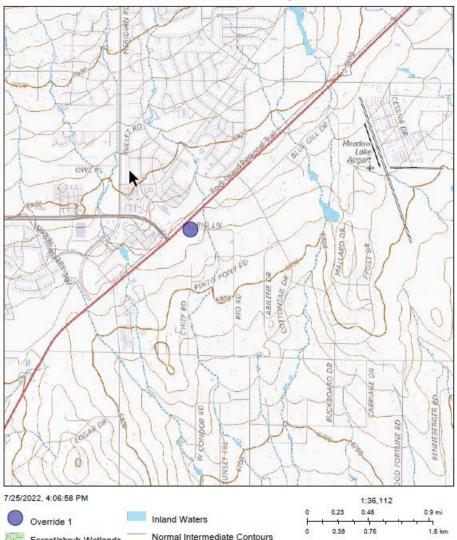
Report - June 2022, 2021-180 NE Stream StreamStats, 2021-180 SW Stream StreamStats, 2021-180 USGS Topo

ADDITIONAL COMMENTS TO SUPPORT JD:

B.

A review of the downstream connectivity of the associated wetlands found there to be a lack of a connection to downstream waters. The drainage features and associated wetlands presented a southward flow path until reaching E. Blaney Road. The flow path consisting of a varying degree of broken stream channel and connected wetlands terminated across a portion of flat terrain with not apparent wetland vegetation. Flow does not appear to reach any downstream waters via the nearby roadside ditch. Flow also does not cross E. Blaney Road due to the lack of culverts and a slight elevation rise. Due to a lack of downstream connectivity, the drainage features and associated wetlands under review are found to be isolated.

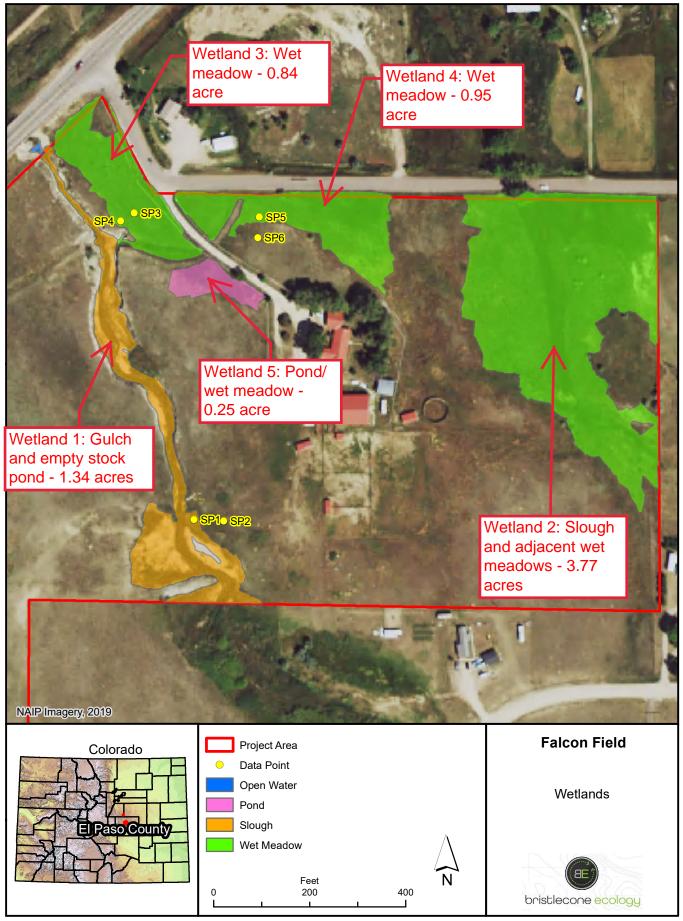
2021-180 USGS Topo



Normal Index Contours

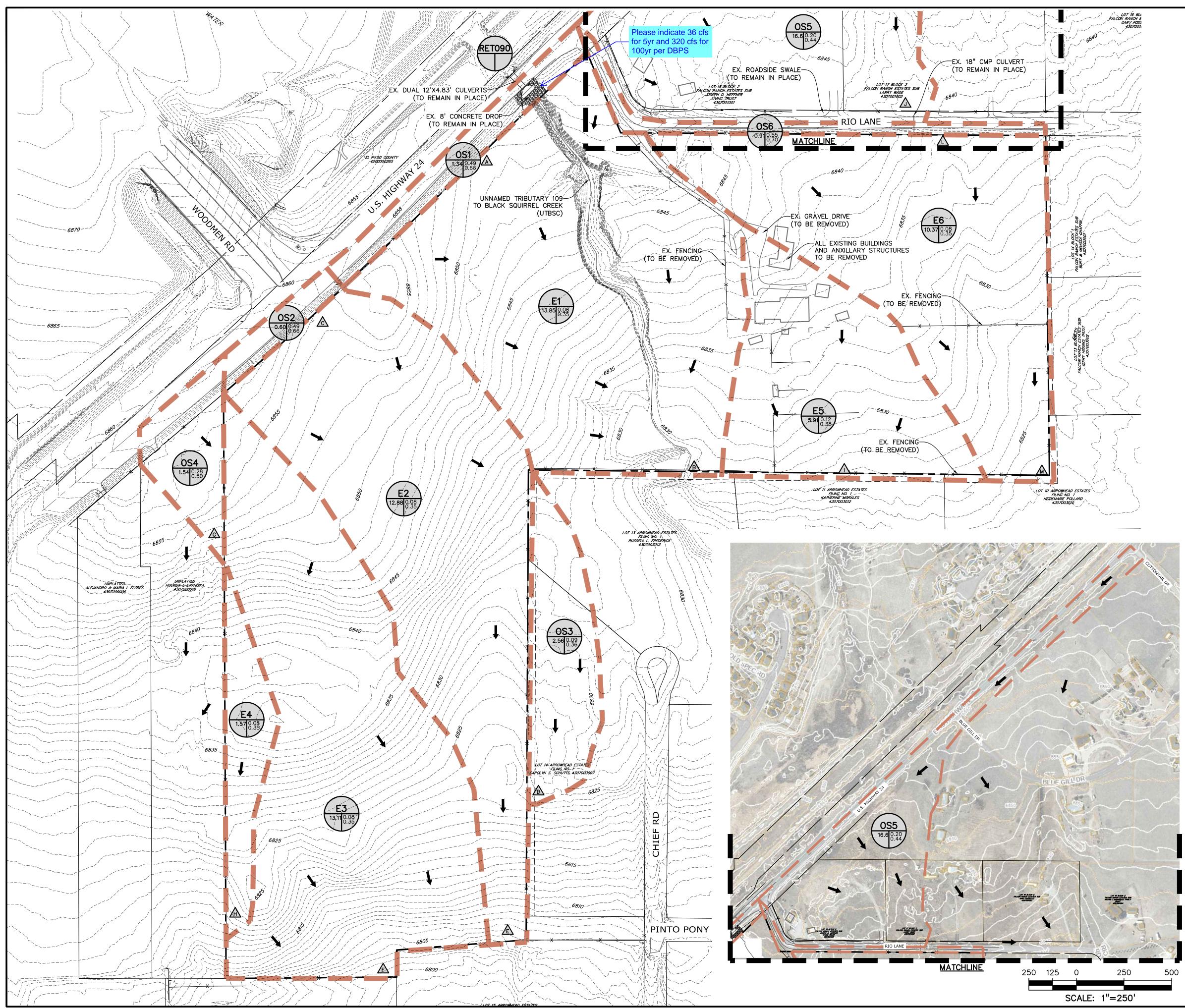
Forest/shrub Wetlands

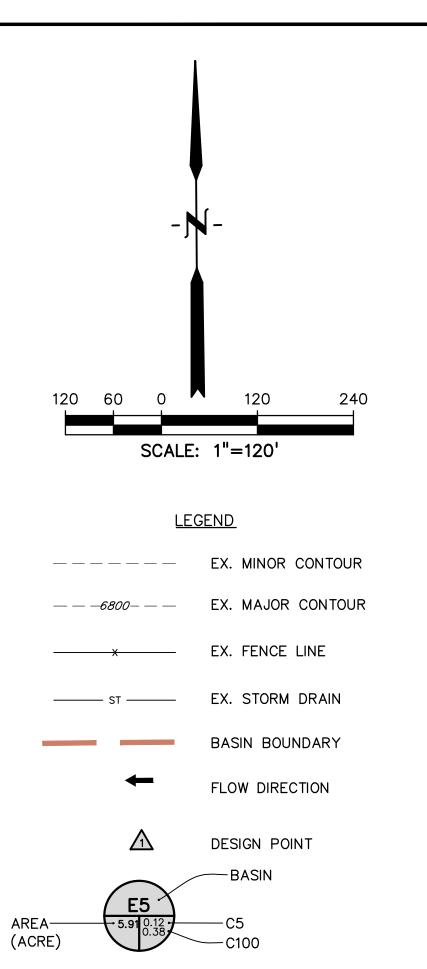
USOS The National Map: National Boundaries Dataset, 30EP Elevation Program, Geographic Natives Information System, National Hydrography Dataset, National Land Cover Database, National Structures Dataset, and National Transportation Databaset, USOS Global Ecosystems; U.S. Census

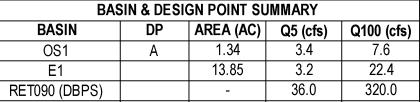


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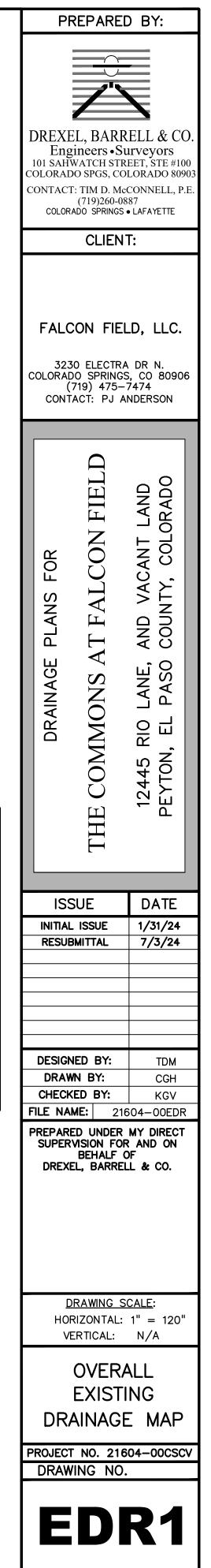
Drainage Maps



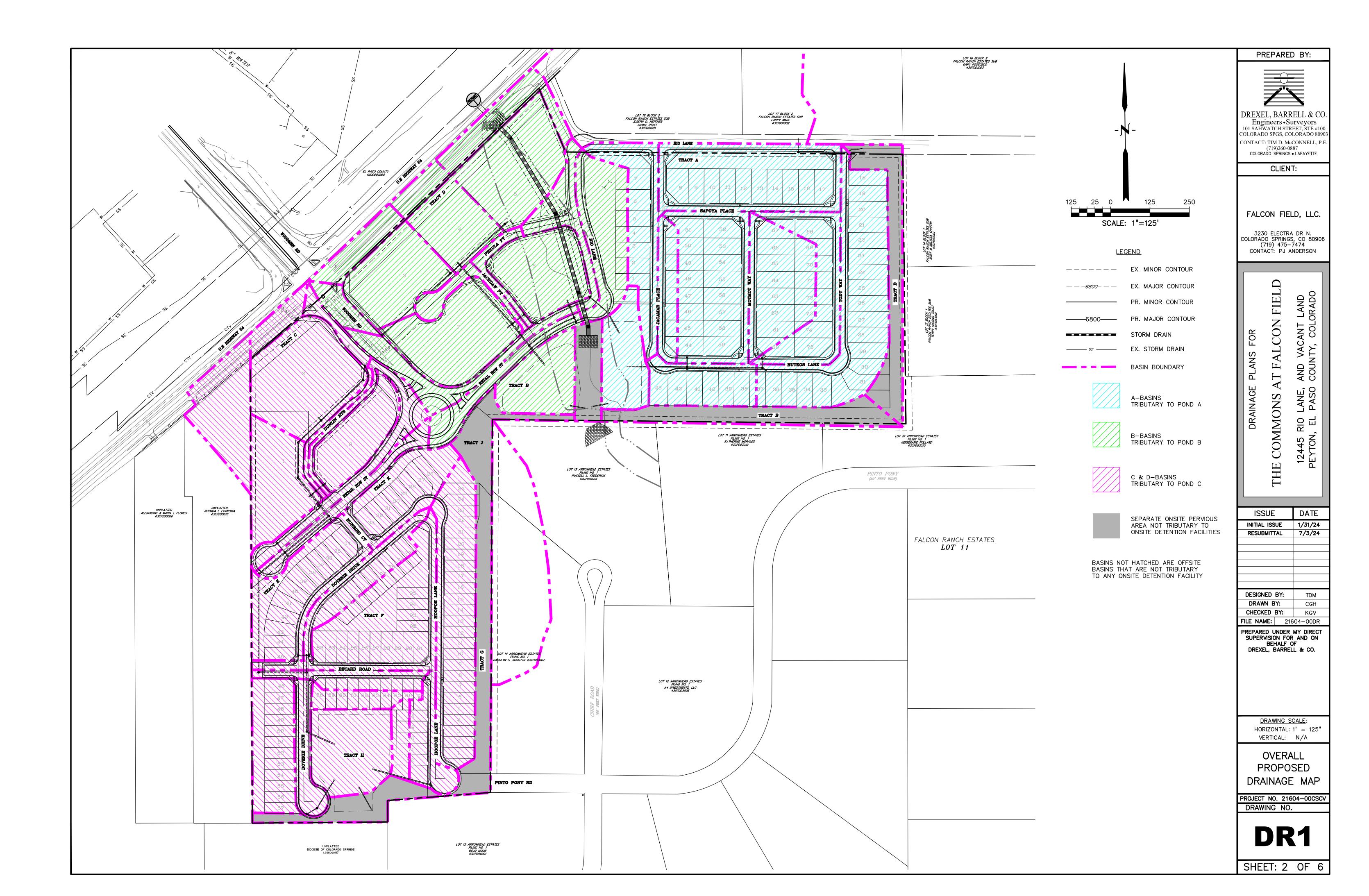


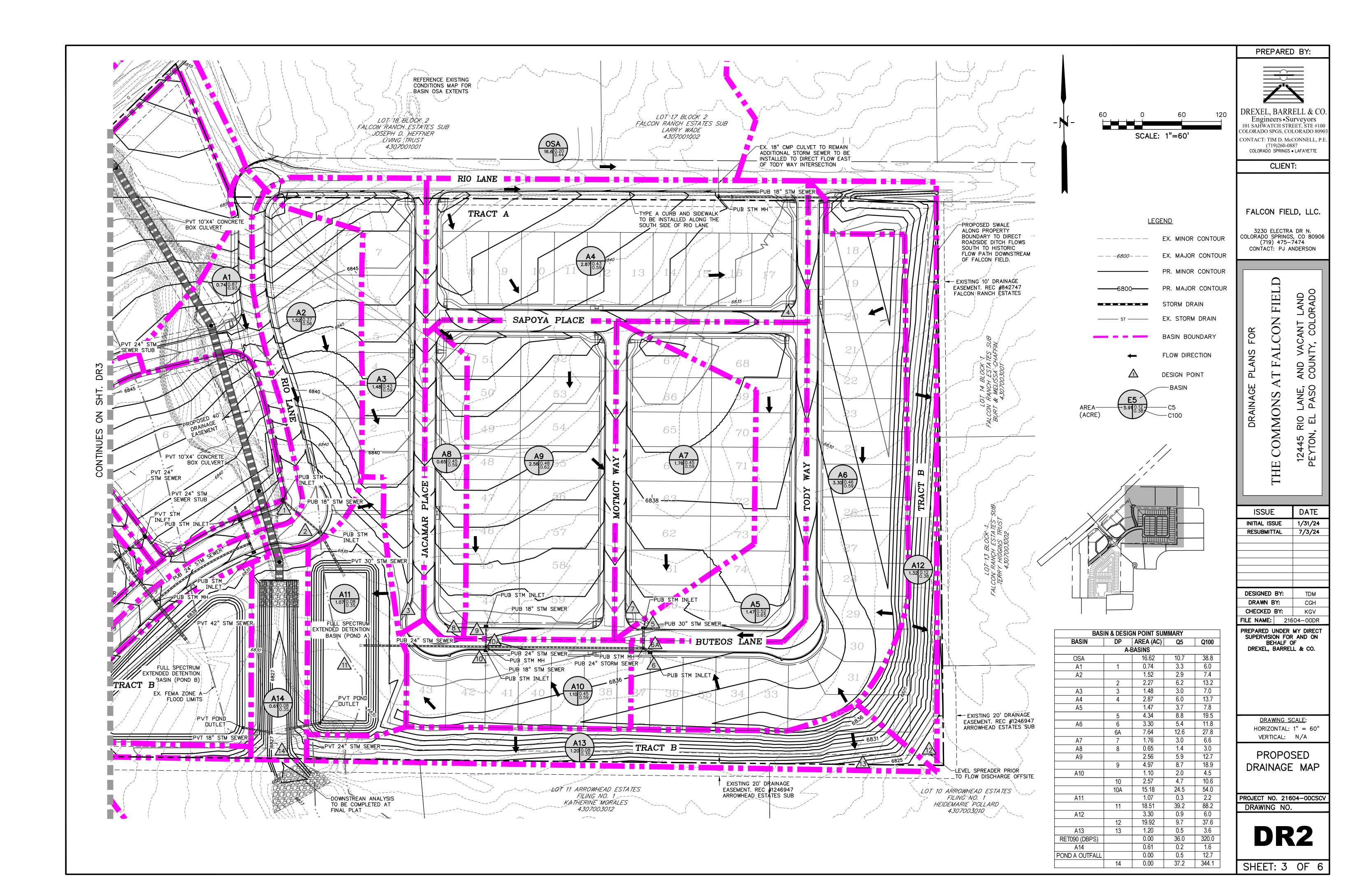


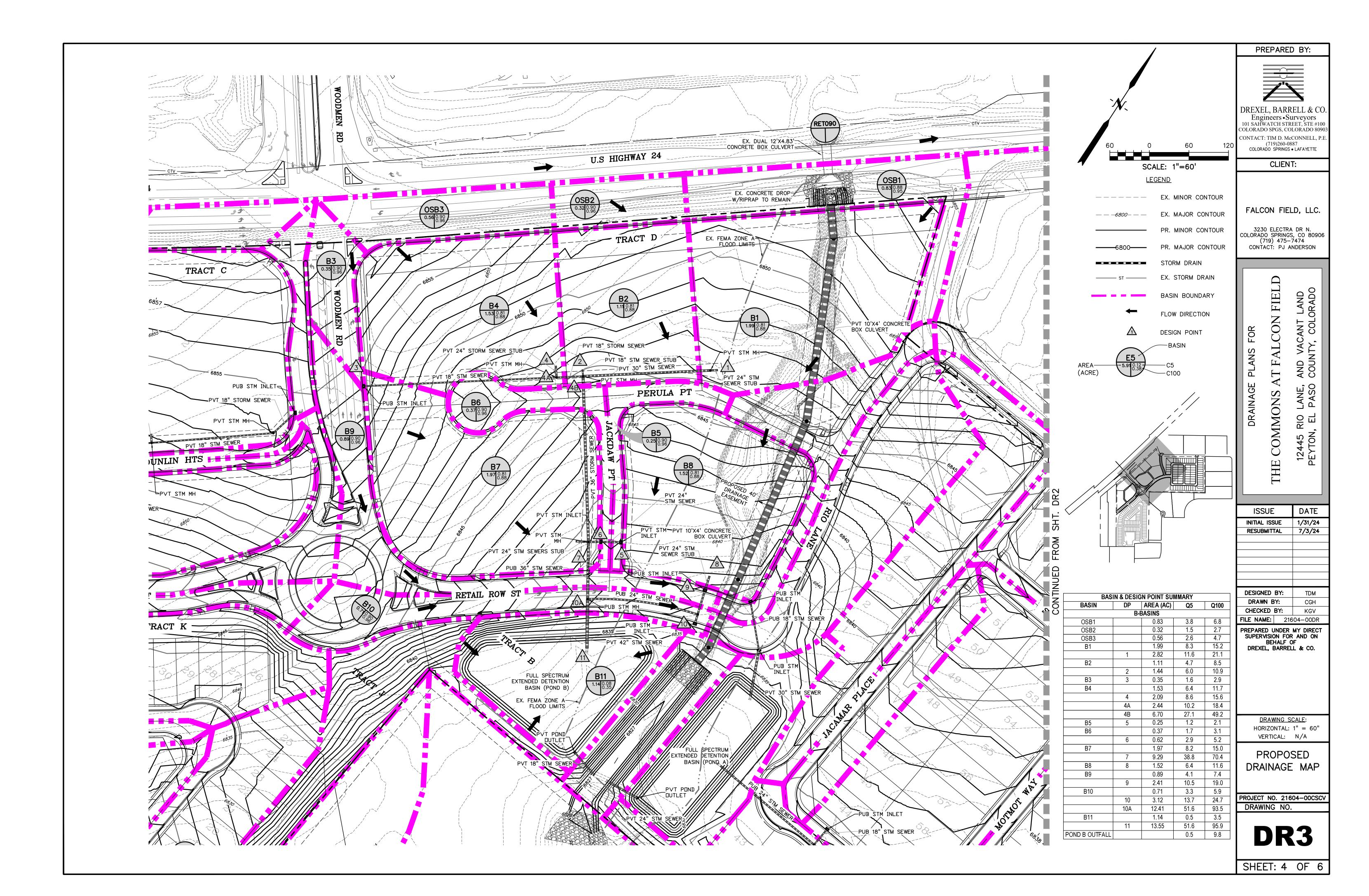
E1		13.85	3.2	22.4
RET090 (DBPS)		-	36.0	320.0
DPA+E1+RET090	В	15.19	41.0	346.4
OS2	С	0.60	1.4	3.2
OS3	D	2.56	0.7	4.5
E2		12.88	2.5	18.6
DPC+DPD+E2	E	16.04	3.8	23.9
E3	F	13.11	2.7	19.6
OS4	G	1.54	1.6	4.8
E4		1.57	0.3	2.6
DPG+E4	Н	3.11	1.5	6.1
E5		5.91	2.2	11.7
OS5	J	16.62	6.2	22.6
OS6	L	0.91	2.6	5.5
E6		10.37	1.7	12.5
DPJ+DPL+E6	М	27.89	7.4	30.7

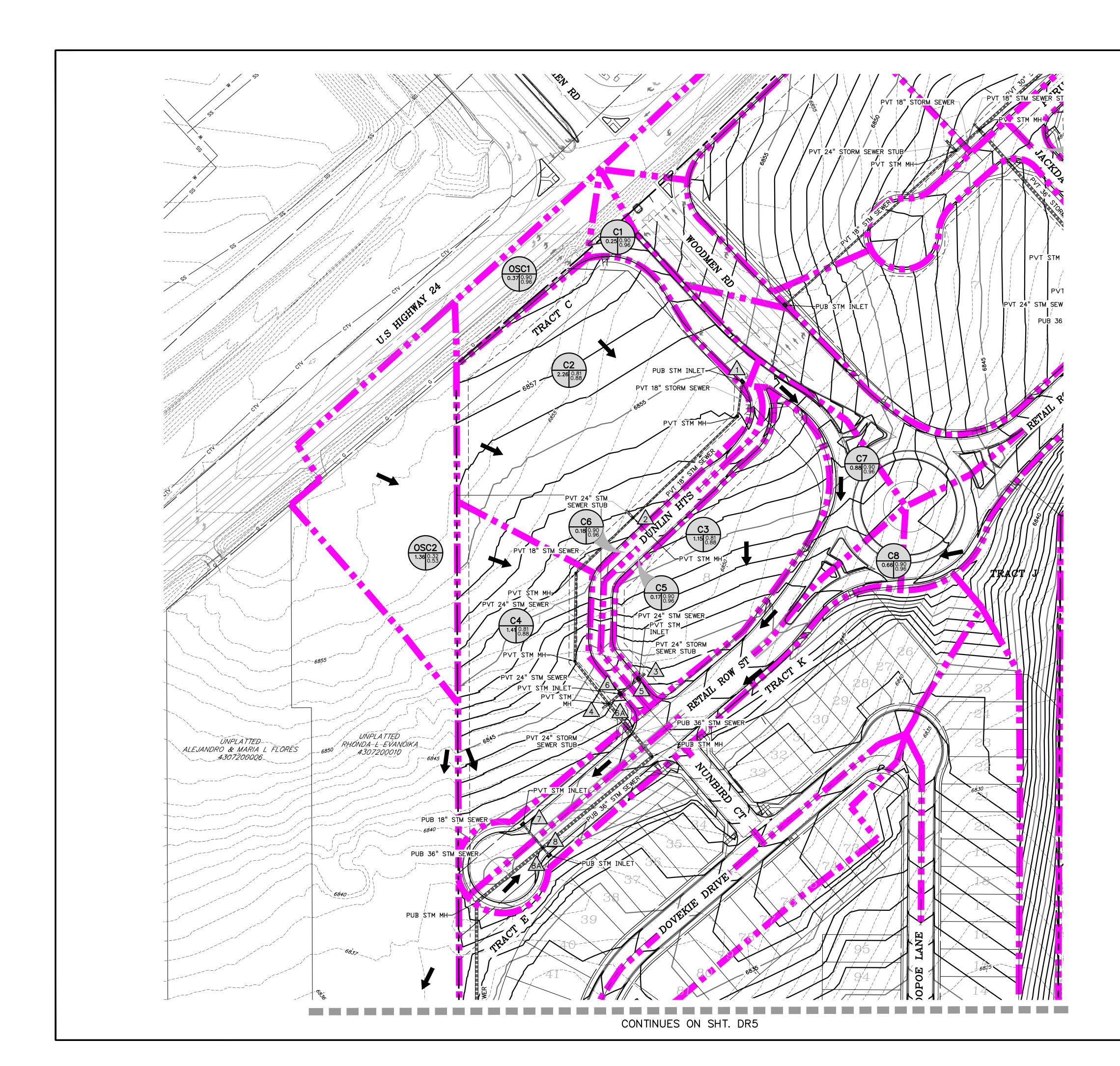


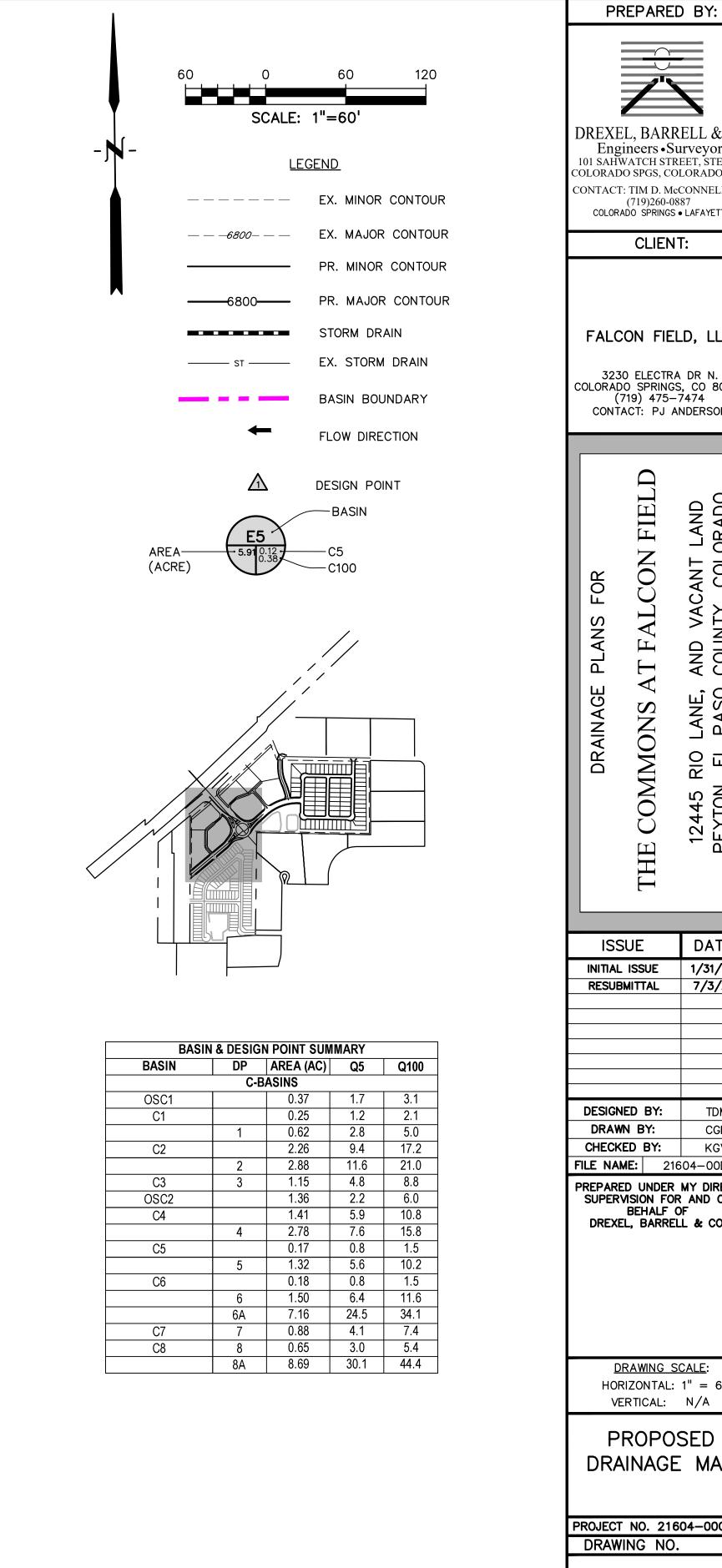
SHEET: 1 OF 6











DREXEL, BARRELL & CO Engineers •Surveyors 101 SAHWATCH STREET, STE #100 COLORADO SPGS, COLORADO 80902 CONTACT: TIM D. McCONNELL, P.E (719)260-0887 COLORADO SPRINGS • LAFAYETTE CLIENT: FALCON FIELD, LLC. 3230 ELECTRA DR N. COLORADO SPRINGS, CO 80906 (719) 475–7474 CONTACT: PJ ANDERSON LAND ORADO ANT COL Ű A Y ND AN CO LANE, PASO RIO EL Z ß 1244 EYT(DATE 1/31/24 RESUBMITTAL 7/3/24 TDM CGH CHECKED BY: KGV FILE NAME: 21604-00DR PREPARED UNDER MY DIRECT SUPERVISION FOR AND ON BEHALF OF DREXEL, BARRELL & CO. DRAWING SCALE: HORIZONTAL: 1'' = 60''VERTICAL: N/A PROPOSED DRAINAGE MAP PROJECT NO. 21604-00CSCV DRAWING NO. DR4 SHEET: 5 OF 6

