## MASTER DEVELOPMENT DRAINAGE PLAN

**FOR** 

Tract C

# CLAREMONT COMMERCIAL SUBDIVISION FILING NO. 2 A RESUBDIVISON OF TRACT OF CLAREMONT BUSINESS PARK FILING NO. 2

# EL PASO COUNTY, COLORADO

**NOVEMBER 2019** 

Prepared for:

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&

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Prepared by:



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> Project #44-037 PCD - SP-XX-XXX

# MASTER DEVELOPMENT DRAINAGE PLAN FOR CLAREMONT COMMERCIAL SUBDIVISION FILING NO. 2 A RESUBDIVISION OF TRACT C OF CLAREMONT BUSINESS PARK FILING NO.2 EL PASO COUNTY COLORADO

#### DRAINAGE PLAN STATEMENTS

#### **ENGINEERS STATEMENT**

The attached drainage plan and report was prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

		caused by any negligent acts, errors or omission
Virgil A. Sanchez, For and on Behalf o	P.E. #37160 f M&S Civil Consultants, Inc	
DEVELOPER'S ST.	<u>ATEMENT</u>	
I, the developer(s) h report and plan.	ave read and will comply with all	the requirements specified in this drainage
BY:	В	Y:
TITLE: DATE:		TITLE: DATE:
ADDRESS:	Lena Gail Case 2432 Parkview Lane Colorado Springs, CO 80903	Hammers Construction, Inc. 1411 Woosley Heights Colorado Springs, CO 80906
EL PASO COUNTY	Y'S STATEMENT	
	with the requirements of El Paso of lumes 1 and 2, and the Engineering	County Land Development Code, Drainage ag Manual, as amended.
Jennif	D Fer Irvin, P.E. ty Engineer / ECM Administrator	ATE:
CONDITIONS	, ,	

#### CONDITIONS:

## MASTER DEVELOPMENT DRAINAGE PLAN FOR CLAREMONT COMMERCIAL SUBDIVISION FILING NO. 2 A RESUBDIVISION OF TRACT C OF CLAREMONT BUSINESS PARK FILING NO.2 EL PASO COUNTY COLORADO

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### **APPENDIX**

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Proposed Drainage Map

## MASTER DEVELOPMENT DRAINAGE PLAN FOR

## **CLAREMONT COMMERCIAL SUBDIVISION FILING NO. 2**

### A RESUBDIVISION OF TRACT C OF CLAREMONT BUSINESS PARK FILING NO.2 EL PASO COUNTY COLORADO

Previous report was approved in December of 2018

#### **PURPOSE**

This document is intended to serve as the Master Development Drainage Plan for Claremont Commercial Subdivision Filing No. 2 and will effectively <u>supersede</u> the previously approved Preliminary Drainage Report for Claremont Commercial Subdivision Fil No. 2, A Resubdivision of Tract C of Claremont Buisness (sic) Park Filing No. 2, El Paso County, Colorado previously approved in March of 2018. The purpose of this document is to identify and analyze the onsite drainage patterns and to ensure that post development runoff is routed through the site safely and in a manner that satisfies the requirements set forth by the El Paso County and City of Colorado Springs Drainage Criteria Manual. The proposed principal use for the site will be neighborhood commercial and light industrial. The parcel is zoned by El Paso County for commercial service as CS. This is the preliminary drainage report; a final drainage report shall be required with the final plat. A drainage letter will be required with the development of the individual lots, provided that no significant changes from the approved final drainage report are being proposed.

#### GENERAL LOCATION AND DESCRIPTION

Claremont Commercial Subdivision Filing No. 2 is located in the Northeast ¼ of the Northeast ¼ of Section 8, and the Southeast ¼ of the Southeast ¼ of Section 5, Township 14 South, Range 65 West of the 6th P.M. in El Paso County, Colorado. The site is bordered to the southeast by U.S. Highway 24 and to the northeast by N. Marksheffel Road, to the north and west by Meadowbrook Parkway, and to the south by a vacant, undeveloped lot. The site lies within the Sand Creek Drainage Basin. Flows from this site are tributary to Sand Creek.

The site consists of 13.7 acres which is currently vacant land with a relatively new roadway infrastructure for Meadowbrook Parkway and associated utilities services directly adjacent to the site. Vegetation is sparse, consisting of native grasses and weeds. Existing site terrain generally slopes from north to southwest at grade rates that vary between 1.2% and 2%. A soil retention wall runs along the eastside of the proposed site, next to U.S. Highway 24 and N. Marksheffel Road, and borders a large portion of the back of the proposed lots. The Claremont Commercial site is currently zoned "CS" and the proposed principal use for the site will be neighborhood commercial and light industrial.

Two sand filter basins will provide water quality treatment for the proposed development. The outlet structures of the proposed water quality ponds will tie into an existing storm sewer system near Meadowbrook Parkway, which routes the treated runoff southwest into Sand Creek. See Appendix for details.

#### **SOILS**

Soils for this project are delineated by the map in the appendix as Ellicott Loamy Course Sand (28), Blendon Sandy Loam (10) and Blakeland Loamy Sand (8) and have been characterized as Hydrologic Soil Types "A" & "B". Soils in the study area are shown as mapped by S.C.S. in the "Soils Survey of El Paso County Area". See Appendix for soils report.

#### HYDROLOGIC CALCULATIONS

Hydrologic calculations were performed using the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual and where applicable the Urban Storm Drainage Criteria Manual. The Rational Method was used to estimate stormwater runoff anticipated from design storms with 5-year and 100-year recurrence intervals.

#### HYDRAULIC CALCULATIONS

Hydraulic calculations were estimated using the Manning's Formula and the methods described in the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual. The relevant data sheets are included in the Appendix of this report.

#### FLOODPLAIN STATEMENT

According to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel No. 08041C0756G, revised December 7, 2018. No portion of this site is located within the 100 year

floodplain. See Appendix.
The previous page indicates 2
sand filter basins. Please revise.

DRAINAGE CRITERIA

The drainage plan and recently approved drainage report for adjacent property indicate a 42" RCP along Meadowbrook Pwky. Please revise accordingly.

This drainage analysis has been prepared in accordance with the current City of Colorado Springs/El Paso County Drainage Criteria Manual. Calculations were performed to determine runoff quantities for the 5-year and 100-year frequency storms for developed conditions using the Rational Method as required for basins having areas less than 100 acres. See Appendix for calculations.

FOUR STEP PROCESS

Please revise your label of the previously approved drainage report as it is not an MDDP. It is a Final Drainage Report.

- **Step1 Employ Runoff Reduction Practices** –Roof drains will be directed to property lines swales to minimize direct connection of impervious surfaces.
- Step 2 Stabilize Drainageways The site is upstream of an existing 40"/48" RCP storm sewer system that directly discharges to Sand Creek Channel via an outlet structure with wingwalls. The "Final Drainage Report for Claremont Business Park Filing No. 2", dated November 2006, by Matrix Design Group, Inc. (henceforth referred to as "MDDP") has been designed to discharge developed flows via a 48" RCP storm sewer system directly into the East Fork Sand Creek. The Claremont Commercial Filing No. 2 site proposes a Sand Filter Water Quality Facility before flows are discharged to the existing private 40"/48" RCP system east of Meadowbrook Parkway. The outlet underdrain has been designed to drain the pond in a peak event within 12 hours, therefore it's not anticipated to have negative effects on the downstream drainageways.
- **Step 3 Provide Water Quality Capture Volume** Two Sand Filter Basin water quality facilities are proposed to provide WQCV.
- Step4 Consider Need for Industrial and Commercial BMP's This submittal provides a final grading and erosion control plan with BMPs in place. The proposed project will use silt fence, a vehicle

preliminary GEC has been provided. Final GEC plan will be provided with the final plat. Please revise.

Please include discussion regarding existing pipes/stub outs on the property indicated in the previously approved drainage reports by Matrix and why they were not used.

tracking control pad, a concrete washout area, mulching and reseeding to mitigate the potential for erosion across the site.

#### EXISTING DRAINAGE CONDITIONS

Please revise your label of the previously approved drainage report as it is not an MDDP. It is a Final Drainage Report.

The CLAREMONT COMMERCIAL Filing No, 2 site consists of 13.7 acres and is situated east of the East Fork Reach of the Sand Creek Watershed. This area was previously studied in the "Final Drainage Report for Claremont Business Park Filing No. 2", dated November 2006, by Matrix Design Group, Inc. (henceforth referred to as "MDDP"). The MDDP calculations indicate that, under the fully developed conditions, the total tributary area of Sub-basins B1, B2, and B3 (18.1 acres), with basin B3 including the eastern half of Meadowbrook Parkway, would produce a cumulative runoff of approximately Q5=42.6 cfs and Q100=86.6 cfs (Design Point 2). The MDDP illustrated that the watershed would drain from east to the southwest towards Meadowbrook Parkway. As stated in the MDDP, overlot grading activities for the entire site have been completed. Per Resolution 16-426 of the BoCC, on-site WQCV is required but on-site stormwater detention is not required per the FDR for Claremont Business Park Fil. 2.

A 48" public storm sewer runs along Woolsey Heights and is routed directly to the Sand Creek channel. Two 10' Type R at grade inlets exist at the intersection of Woolsey Heights and Meadowbrook Parkway, one on the northwest and the other on the northeast corner of the intersection. Runoff from the site and the two surrounding streets, Meadowbrook Parkway and Woolsey Heights, is intercepted by these inlets and conveyed to the Sand Creek channel via the existing 48" public storm sewer.

Refer to the drainage basin descriptions that follow for additional information as well as the Drainage Map located within the Appendix of this report.

# PROPOSED DRAINAGE CHARACTERIST TO Storm sewer.

revise sentence accordingly.

#### **General Concept Drainage Discussion**

The majority of the site will consist of neighborhood commercial and light industrial, asphalt, curb, two storm water quality sand filter basins, and landscaping. The site will typically drain using across asphalt and impermeable surfaces which direct runoff primarily to the south and southwest to proposed private pipe systems which direct runoff to one of two private ponds. The outlet structures of the proposed water quality ponds will release runoff to the existing private 42" RCP storm sewer located at the southwest corner of the site. A survey and inspection of the existing 42" RCP shall be made before use. The existing private 42" storm sewer ties into an existing public 48" storm sewer which will route the treated runoff to Sand Creek. For more information of drainage basins, existing and proposed structures refer to the Proposed Drainage Map located within the Appendix of this report.

#### **Detailed Drainage Discussion**

**Basin A**, 0.19 acres, consists of steep slopes of 32% adjacent to portions of U.S Highway 24 and N. Marksheffel Rd. The roadway embankment within **Basin A** slopes into a soil retention wall that runs along the south east boundary of the site. Runoff for **Basin A** is limited has been calculated to reach peak flow rates of Q5=0.1 cfs and Q100=0.6 cfs. Flows produced within the basin will be conveyed westward into adjacent basins (**Basin B**) as sheet flow.

**Basin B**, 1.39 acres, consists of Lot 11 along the northeast corner of the proposed site. Runoff produced within **Basin B** is anticipated to reach peak runoff rates of Q5=5.5 cfs and Q100=10.1 cfs. A proposed private 24" polyethylene storm drain (**Pipe 1**) will be extended to **Design Point 1**(Q5=5.5 cfs and Q100=10.1 cfs) to capture runoff from **Basins A** and **B**.

Please also include in your narrative how your proposed flows entering the existing storm system compare to the previously approved drainage report from Matrix. State whether or not the existing facilities are adequate. Please take into account the recently approved drainage report from the lot to the south (PCD file no. PPR192) that will also tie into this existing system.

The acreage shown on the drainage plan does not match the narrative. Revise so that they match.

The lot designations do not match what is shown on the preliminary plan please revise so that they match.

**Basin** C, 0.30 acres, consists of portion of steep slopes of up to 33% that lie adjacent to portions of U.S Highway 24. Similar to **Basin** A, the roadway embankment within **Basin** C, slopes into a soil retention wall that runs along the eastern boundary. Runoff for **Basin** C has been calculated to reach peak flow rates of Q5=0.1 cfs and Q100=1.0 cfs. The limited runoff produced is assumed to be conveyed westward into adjacent **Basin** D as sheet flow.

Basin D, 1.39 acres, consists of Lot 10 along the eastern boundary of the proposed site. Runoff produced within Basin D is anticipated to reach peak runoff rates of Q5=6.3 cfs and Q100=11.5 cfs. A proposed private 24" polyethylene storm drain (Pipe 2) will be extended to Design Point 2(Q5=6.4 cfs and Q100=12.4 cfs) to capture runoff from Basins C and D. Runoff collected within Pipes 1 and 2 will be routed to a proposed private water quality pond via a private 30" polyethylene storm drain (Pipe 3) at peak flow rates of Q5=11.8 cfs and Q100=22.6 cfs. A small riprap pad will be required to reduce velocities prior to entering the pond.

the swale shown between basin D and basin I. Basin E, 1.39 acres, consists of Lot 9 and a portion of the planned private access entrance, which is located adjacent to a portion of Meadowbrook Parkway. Runoff produced within Basin E is anticipated to reach peak runoff rates of Q5=6.5 cfs and Q100=11.8 cfs. A proposed private 24" polyethylene storm drain (Pipe 4) will be extended from the private pond to collect runoff reaching Design Point 3(Q5=5.5 cfs and Q100=10.1 cfs).

Basin F, 0.36 acres, consists of a land (Tract B) which is dedicated to house a proposed private onsite Sand Filter Basin Water Quality Pond (Pond 1) adjacent to existing Meadowbrook Parkway. Runoff produced within Basin F will ultimately combine with flows entering the pond via Pipes 3 and 4 at Design Point 4. The total flow anticipated to reach the pond (DP4) is calculated by the rational method to be Q5=18.2 cfs and Q100=35.0 cfs. Using the UD-Detention worksheet, flows treated via the Sand Filter Basin are to be discharged through a 6.0' x 2.91' CDOT Modified Type D outlet structure and proposed private 24" polyethylene Storm Sewer (Pipe Runs 5, 5.1, 5.2). The proposed pond shall be constructed with 4:1 SS and is anticipated to store 0.095, 0.155 and 0.183 ac-ft and discharge 0.1 cfs, 7.2 cfs, and 15.5 cfs in the water quality, 5 year and 100 year events respectively. The emergency spillway shall be designed to discharge the peak inflow safely to Meadowbrook Parkway in the event that the inlet would become clogged. Runoff conveyed in Pipe 5.2 will combine with flows from a second onsite pond, prior to being discharged downstream via an existing 42" RCP storm sewer.

**Basin G**, 0.27 acres, consists of a landscaping strip running alongside and adjacent to Meadowbrook Parkway and a small section of pavement associated with site access. Excluding the small section of street the basin consists primarily of trees, bushes/grasses, and decorative ground cover. Low runoff values produced by Basin Q of Q5=0.5 cfs and Q100=1.3 cfs will travel as sheet flow into Meadowbrook Parkway.

Should this be G?

Should this be G?

**Basin H**, 0.71 acres, consists of steep slopes of up to 33% adjacent to portions of U.S Highway 24. The roadway embankment within **Basin H** slopes into a soil retention wall that runs along the south east boundary of the site. Runoff for **Basin H** has been calculated to reach peak flow rates of Q5=0.3 cfs and Q100=2.0 cfs. Flows produced within the basin will be conveyed westward into adjacent basins (**Basin I**) as sheet flow.

**Basin I**, 2.75 acres, consists of Lots 5 and 6, portions of Lots 2-4 and 7 and section of proposed private street, which is generally located within the center of the proposed site. Runoff produced within **Basin I** is anticipated to reach peak runoff rates of Q5=9.8 cfs and Q100=17.9 cfs. Runoff from the **Basins H** and **I** shall be conveyed via side lot swales and curb and gutter to a proposed private street and a pair of proposed CDOT Type R at grade inlets located at **Design Point 5** (Q5=10.1 cfs and Q100=19.8 cfs). Runoff intercepted by the inlets will be conveyed south to a second proposed water quality pond via proposed private 24" polyethylene **Pipes 6** and 7 at 5 year flow rates of 6.4 cfs and 10.1 cfs and at 100 year flow rates of 10.6 and 16.6 cfs respectively. Runoff bypassing the inlets will continue west within the street to **Design Point 6**.

also includes lot 8

The flow should be greater in pipes 10 and 10.1 as flow from pipe 9 should also be included as stated in your narrative. Revise accordingly.

**Basin J,** 1.05 acres, consists of portions of Lots 1, 2 and 7 and a segment of the proposed street, which is located along the western edge of the proposed site. Runoff produced within **Basin J** is anticipated to reach peak runoff rates of Q5=4.4 cfs and Q100=8.0 cfs. Runoff from the **Basins J** and flow-by from **DP5** shall intercepted by a pair of proposed CDOT Type R at grade inlets located at **Design Point** 6(Q5=4.4 cfs and Q100=11.2 cfs). Runoff intercepted by the proposed inlets will be conveyed south to a second proposed water quality pond via proposed private 18" and 24" polyethylene **Pipes** 8 and 9 at 5 year flow rates of 2.8 cfs and 4.4 cfs and at 100 year flow rates of 6.9 and 11.0 cfs respectively preliminary assumptions, approximately 0.1 cfs will bypass DP6 and will be continue within the curb and gutter to the adjacent street in the 100 year event.

**Basin K**, 0.42 acres, consists of the rear halves of Lots 1 and 2, which is generally located along the southwest corner of the proposed site. Runoff produced within **Basin K** is anticipated to reach peak runoff rates of Q5=1.8 cfs and Q100=3.2 cfs. Runoff from the **Basins K** can be conveyed to a manhole at the southwest corner of Lot 1 which can be fitted with a beehive style grate or inlet. Runoff collected at the local depression would combine with flows in **Pipe 9** and continue to the proposed water quality pipe via pipes 10 and 10.1 at peak flow rates of 2.8 cfs and 4.4 cfs in the 5 and 100 year storm events.

**Basin L**, 1.32 acres, consists of steep slopes of 32% adjacent to portions of U.S Highway 24. The roadway embankment within **Basin L** slopes into a soil retention wall that runs along the south east boundary of the site. Runoff for **Basin L** has been calculated to reach peak flow rates of Q5=0.5 cfs and Q100=3.5 cfs. Flows produced within the basin will be conveyed westward into adjacent basins (**Basin M**) as sheet flow.

**Basin M**, 1.84 acres, consists of a portion of Lots 3 and 4, which is generally located along the south and southeast sides of the proposed site. Runoff produced within **Basin M** is anticipated to reach peak runoff rates of Q5=6.7 cfs and Q100=12.2 cfs. Runoff from the **Basins L** and **M** shall be conveyed to a proposed line swale or pipe system that will extend out of proposed WQ Pond 2. Peak runoff reaching **Design Point 8** is anticipated to have peak flow rates of Q5=7.2 cfs and Q100=15.7 cfs. The proposed swale would need to be a minimum of 1.5' deep at 0.5% using a 2' bottom width and 3:1 side slopes. A riprap rundown and pad would need to be required to arrest flows entering the pond. Should a pipe system be extend it would likely be a minimum of 24".

Basin N, 0.47 acres, consists of a land (Tract A) which is dedicated to house a proposed private onsite Sand Filter Basin Water Quality Pond (Pond 2) adjacent to existing Meadowbrook Parkway. Runoff produced within Basin N will ultimately combine with flows entering the pond via Pipes 7, 10.1 and from the Swale (DP8). The total flow anticipated to reach the pond (Design Point 9) is calculated by the rational method to be Q5=18.5 cfs and Q100=38.4 cfs. Using the UD-Detention worksheet, flows treated via the Sand Filter Basin are to be discharged through a 7.0' x 2.91' CDOT Modified Type D outlet structure and proposed private 24" polyethylene Storm Sewer (Pipe Run 11). The proposed pond shall be constructed with 4:1 SS and is anticipated to store 0.120, 0.196 and 0.298 ac-ft and discharge 0.2 cfs, 11.0 cfs, and 23.1 cfs in the water quality, 5 year and 100 year events respectively. The emergency spillway shall be designed to discharge the peak inflow safely to Meadowbrook Parkway in the event that the inlet would become clogged. Runoff conveyed in Pipe 11 will combine with flows within Pipe 5.2, prior to being discharged downstream via an existing 42" RCP storm sewer and into the backside of the existing 10' Type R at grade inlet along existing Woolsey Heights and then to the west via an existing 48" storm sewer.

**Basin O**, 0.16 acres, consists of a landscaping strip running alongside and adjacent to Meadowbrook Parkway. The basin will most likely be composed of trees, bushes/grasses, and decorative ground cover. Low runoff values produced by **Basin O** of Q5=0.2 cfs and Q100=0.6 cfs will travel as sheet flow into Meadowbrook Parkway.

**Basin P**, 0.03 acres, consists of steep slopes of up to 33% adjacent to portions of U.S Highway 24. The roadway embankment within **Basin P** slopes into a soil retention wall that runs along the south east boundary of the site. Runoff for **Basin P** has been calculated to reach peak flow rates of Q5=0.0 cfs and Q100=0.1 cfs. Flows produced within the basin will be conveyed westward into adjacent basins (**Basin Q**) as sheet flow.

**Basin Q**, 0.11 acres, consists of a thin utility corridor alongside the south boundary of the site. The basin will most likely be composed native ground cover. Low runoff values produced by Basin Q of Q5=0.0 cfs and Q100=0.3 cfs will combine with flows from **Basin P** and will discharge to adjacent site to the south as sheet flow.

There are no planned or required improvements to the Sand Creek Drainage Channel with the development of the CLAREMONT COMMERCIAL site.

#### WATER QUALITY PROVISIONS AND MAINTENANCE

The subject site was previously analyzed within the Final Drainage Report for Claremont Business Park Filing No. 2 prepared by Matrix Design Group approved April 24, 2006. Per Resolution 16-426 of the BoCC, on-site WQCV is required but on-site stormwater detention is not required per the FDR for Claremont Business Park Fil. 2. The water quality volume required for the site has been determined using the UDFCD UD-Detention workbook per the guidelines set forth in the City of Colorado Springs/El Paso County Drainage Criteria Manual - Volume II.

As previously discussed water quality for the site is provided by two proposed Sand Filter Basins (SFB). Pond 1 is designed to treat runoff from approx 5.33 acres, by providing 0.095 acre-feet of water quality storage, while Pond 2 will runoff from approx 8.57 acres, by providing 0.120 acre-feet of water quality storage.

#### will treat runoff

Flows tributary to the two SFBs are released through outlet structures into an existing storm sewer system located along Meadowbrook Parkway. The water quality basins will be private and shall be maintained by the property owner. Access shall be granted to the owner and El Paso County for access and maintenance of the private WQCV facility. A private maintenance agreement document shall accompany the final drainage report(s) submittal(s) which construct the two ponder County criteria water quality must be provided

#### **EROSION CONTROL**

It is the policy of the El Paso County that we submit a grading proposed basins that will not be treated and ensure that the total will not exceed 1 acre.

Proposed silt fence, vehicle traffic control, and concrete washout area are proposed as erosion control measures.

for 100% of the site, ECM section I.7.1.C.1

be excluded. Provide discussion regarding the

indicates that 20% of site, not to exceed 1 acre may

#### **CONSTRUCTION COST OPINION**

Private Drainage Facilities (NON-Reimbursable):

Item	Description	Quant	tity Unit	Cost	Cost
1.	18" PP	48	LF \$40	/LF	\$1,920.00
2.	24" PP	1327	LF \$48	/LF	\$63,696.00
3.	30" PP	126	LF \$65	/LF	\$8,190.00

4.	At Grade Inlets (Type R) L=15'	4	EA	\$7,200	/EA	\$28,800.00
5.	Manholes	5	EA	\$4,000	/EA	\$20,000.00
6.	WQCV Sand Filter Pond	2	EA	\$19,000	/EA	\$38,000.00
						TE + 1 01/0 /0/00

Total \$160,606.00

M & S Civil Consultants, Inc. (M & S) cannot and does not guarantee the construction cost will not vary from these opinions of probable costs. These opinions represent our best judgment as design professionals familiar with the construction industry and this development in particular. The above is only an estimate of the facility cost in 2018.

Please state that

#### **DRAINAGE & BRIDGE FEES**

drainage fees were previously paid for this property.

This site is in the Sand Creek Drainage Basin. The site is proposed to be subdivided into sixteen commercial lots. Since the property was previously platted as Tract C of Claremont Business Park Filing No. 2 (Reception No. 207712506), no additional Drainage Bridge and/or Pond fees are required. In the appendix, see "Final Drainage Report for Claremont Business Park Filing No. 2", Revised November 2006, by Matrix Design Group, Inc, for previously paid drainage and bridge fees.

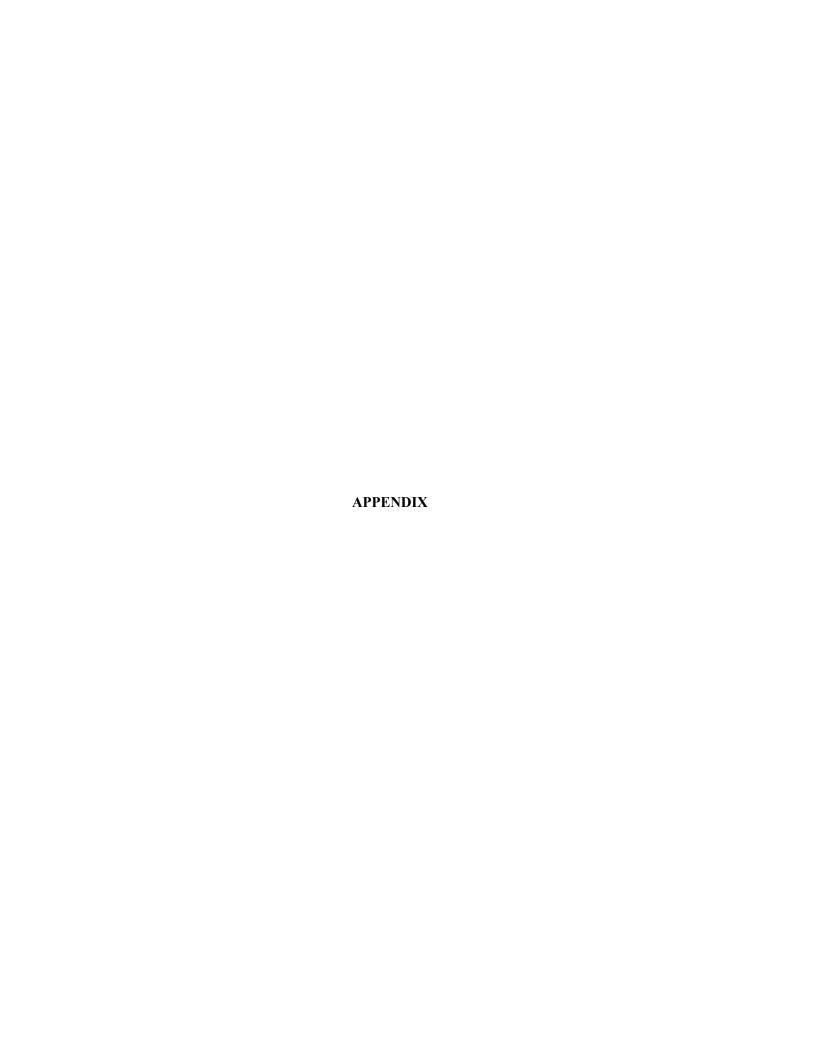
#### **SUMMARY**

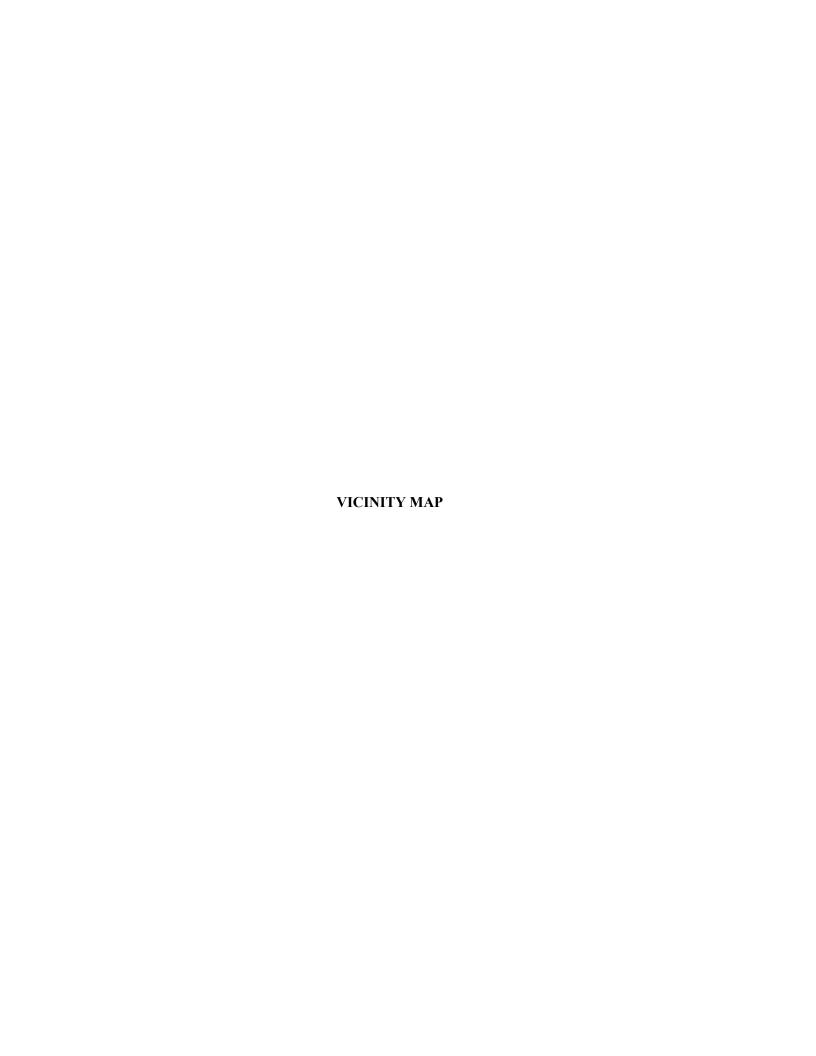
the drainage fees section of the Matrix report was not included. Please include in the appendix.

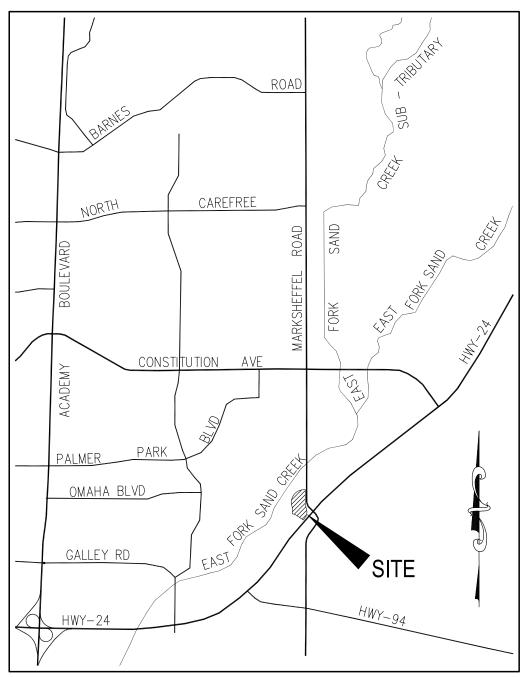
Development of Claremont Commercial Subdivision Filing No. 2 will not adversely affect the surrounding development. The proposed drainage facilities will adequately convey, detain and route runoff from the onsite & offsite flows to existing facilities. All drainage facilities described herein and shown on the included Proposed Drainage Map (See Appendix) are subject to change being dependent upon individual lot development. Care will be taken to accommodate overland emergency flow routes on site and temporary drainage conditions.

#### **REFERENCES**

- 1.) "El Paso County and City of Colorado Springs Drainage Criteria Manual".
- 2.) "Urban Storm Drainage Criteria Manual"
- 3.) SCS Soils Map for El Paso County.
- 4.) Flood Insurance Rate Map (FIRM), Federal Emergency Management Agency, Effective date December 7, 2018.
- 5.) "Final Drainage Report for Claremont Business Park Filing No. 2", dated November 2006, by Matrix Design Group, Inc.



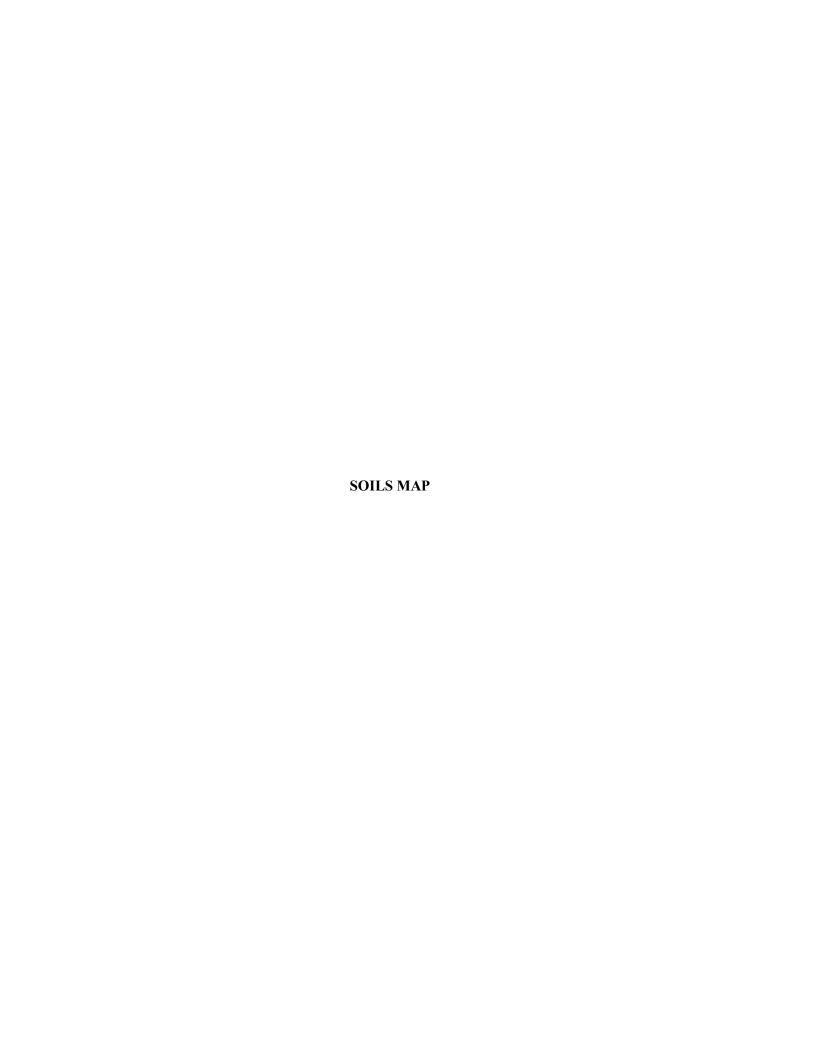




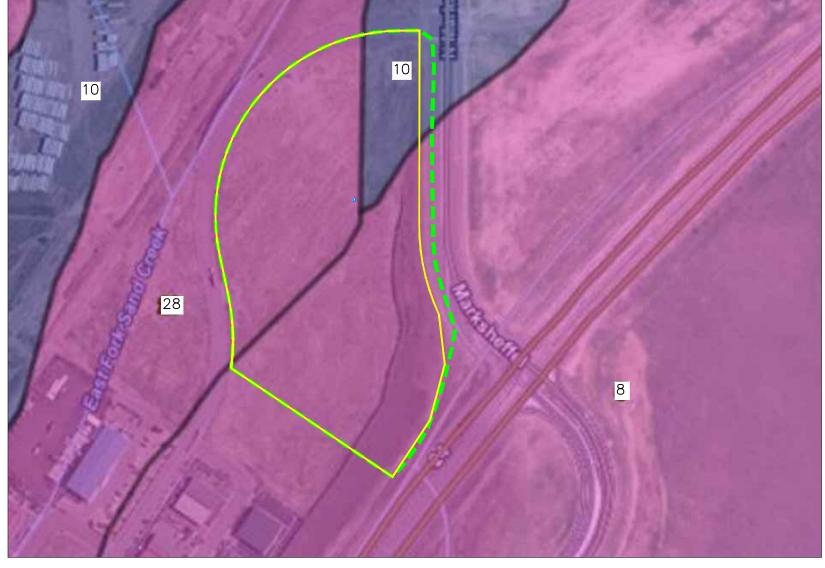
 $\frac{\text{VICINITY MAP}}{\text{\tiny N.T.S.}}$ 



20 BOULDER CRESCENT, SUITE 110 COLORADO SPRINGS, CO 80903 PHONE: 719.955.5485



28



Α

#### Summary by Map Unit — El Paso County Area, Colorado (CO625) Map unit symbol Map unit name Rating Blakeland loamy sand, 1 to 9 percent slopes 8 10 Blendon sandy loam, 0 to 3 percent slopes В

Ellicott loamy coarse sand, 0 to 5 percent slopes

#### CLAREMONT COMMERCIAL FILING NO. 2

HYDROLOGIC TYPE A SOILS

HYDROLOGIC TYPE B SOILS

SITE BOUNDARY



NOT TO SCALE

SOILS MAP







#### LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO-INDIDIDATION BY THE 1% ANNUAL CHANCE FLOOD

ZONE A No Base Road Bevalions determined.
ZONE AE Base Road Elevations determined.

ZONE AM Place depths of 1 to 3 feet (usually enems of ponding); Here Place

AO Flood depins of i to 3 feet (usually sheet Row on sloping terrain); swarage departs getermined. For areas of saluyisi fen Roading, vehicibes also determined.

determined.

COME AR Special Pland Heaved Area Foreign prospected from the 1% service chance flood by a Road control system that was subsequently described. Zone AR

ZONE 499 Area to be projected from 1% annual change flood by a Federal Bood protection system under construction; no Base Flood Elevations determines.

ZONE V Cossial flood zone with velocity hexard (we've action); no Base Flood

ZONE V Costal flood zone with velocity hezard (were includy, no Base Flood Elevations electronics).

ZONE VE - Costal Road zone with velocity hezard (were nothers. Rane Flood

ZONE VE Constal Bood zone with vehicity hazard (were actionly Basis Flows Elementaria distributed)

FLOODWAY AREAS IN ZONE AE

The Bootway is the creating of a stream plus any adjacent Roodpish areas that must be kept free at appropriately solved, the 1% annual change floor can be carried warright substantial sucreases in floor heights.

OTHER FLOOD AREAS

ZONE X

Areas of 9.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 floot or with distinger areas less than 1 sold are mile, and areas protected by leves from 1% annual chance flood.

OTHER AREAS

ZONE X Areas settlemined to be obtained the 0.25% entired that the modulation.

ZONE C Areas in stach flood hexards are undescripted, but phosphic.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and CPAs are normally located within or adjacent to Special Flood Hazard Areas.

Flooring boundary

Flooring boundary

John D Squadery

CBSS and OPA boundary

Aquindary d'viding Special Flood Herard Areas of different Session Clevetions, flood depths of flood velocities.

Spec Flood Elevation line and value; alevation in factor
(EL 987) Sees Flood Elevation value; alevation within same;
elevation in factor

\* Referenced to the North American Vertical Datum of 1988 (NAVO 88)

A Cross section line

57°07'30'00" Geographic continuets retained to the White American Debut of 1933 (NAD 33)

\*1500 meter Duvenat Transcens bereaty grid inde.

Egoogs FT 5000-foot grid ticks: Colorado State Plane coordinate. system, central sone (FIPSZONE 0500). Lembert Conformal Conic Projection.

DX8510 Sends mark (see explanation in Notes to Users section of this FRM panel)

MPL6 Rover MR

MAP REPOSITORIES
Reter to 1980 Repositories hat on Map Index

EPRECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP MARCH 17, 1997

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL.

DECEMBER 7, 2018 - Buckets corporate limits to charge Base Stood Elevations and 
Special Flood Research Arebs, to update map forms, to disc needed and note remote, and is 
incorporate grandously issued Lathers of Map Revision.

For continually man revision history prior to countywide mapping, refer to the Community Map Missory Table located in the Flood Insurance Saudy report for this job attack.

To determine 9 flow transence to evellable to this community content your lossuance, agent or call the Mattern Hood transence Program at 1-803-519-5620.

**LEGEND** 





# FIRM

FLOOD INSURANCE RATE MAP EL PASO COUNTY, COLORADO AND INCORPORATED AREAS

PANEL 756 OF 1300

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

COMMUNITY NUMBER PANEL SUFFIX CONCORDOR NO TO THAT OR CONCORDOR NO CON

Notice to Unit: The Wind Manthur Strotte States should be used when place growing products; the Compression humber shown acrows about the united or majorance people for the subject



MAP NUMBER 08041C0756G

MAP REVISED DECEMBER 7, 2018

Federal Emergency Management Agency

Please provide a legible FIRM Map

NOT TO SCALE

FIRM MAP



Cig Exhibits\ Eng /gwb/8-CBP ó CBP

31

2



Please update the title

# MDDP CLAREMONT COMMERICAL FILING NO. 2 PROPOSED DRAINAGE CALCULATIONS

(Area Runoff Coefficient Summary)

			COMMER	OOFS 0.73-0 CIAL AREA LT DRIVES	1S 0.81-0.88	GRAVEL S	APED AREAS TORAGE YAI VDUST AREA	RD 0.30-0.50	PARKS 0.12-0.39 GREENBELTS/AGRI. 0.09-0.36		WEIGHTED		
BASIN	TOTAL AREA (SF)	TOTAL AREA (Acres)	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	C <sub>100</sub>
A	8359.6	0.19	0.00	0.73	0.81	0.00	0.30	0.50	0.19	0.09	0.36	0.09	0.36
В	60660.5	1.39	1.39	0.81	0.88	0.00	0.59	0.70	0.00	0.30	0.50	0.81	0.88
С	13279.8	0.30	0.00	0.81	0.88	0.00	0.59	0.70	0.30	0.09	0.36	0.09	0.36
D	66703.6	1.53	1.53	0.81	0.88	0.00	0.59	0.70	0.00	0.09	0.36	0.81	0.88
E	67533.9	1.55	1.55	0.81	0.88	0.00	0.59	0.70	0.00	0.09	0.36	0.81	0.88
F	15781.4	0.36	0.00	0.73	0.81	0.00	0.30	0.50	0.36	0.12	0.39	0.12	0.39
G	12722.3	0.29	0.06	0.90	0.96	0.23	0.16	0.41	0.00	0.09	0.36	0.32	0.53
Н	31099.0	0.71	0.00	0.90	0.96	0.00	0.16	0.41	0.71	0.09	0.36	0.09	0.36
I	119584.6	2.75	2.75	0.81	0.88	0.00	0.30	0.50	0.00	0.12	0.39	0.81	0.88
J	45863.7	1.05	1.05	0.81	0.88	0.00	0.30	0.50	0.00	0.09	0.36	0.81	0.88
K	18476.1	0.42	0.42	0.81	0.88	0.00	0.30	0.50	0.00	0.09	0.36	0.81	0.88
L	57315.2	1.32	0.00	0.81	0.88	0.00	0.30	0.50	1.32	0.09	0.36	0.09	0.36
M	80126.1	1.84	1.84	0.81	0.88	0.00	0.30	0.50	0.00	0.09	0.36	0.81	0.88
N	20642.4	0.47	0.00	0.81	0.88	0.00	0.16	0.41	0.47	0.12	0.39	0.12	0.39
0	6997.2	0.16	0.02	0.90	0.96	0.00	0.30	0.50	0.14	0.12	0.41	0.22	0.48
P	1393.0	0.03	0.00	0.81	0.88	0.00	0.30	0.50	0.03	0.09	0.36	0.09	0.36
Q	4961.4	0.11	0.00	0.90	0.96	0.00	0.30	0.50	0.11	0.09	0.36	0.09	0.36

Calculated by: DLM

Date: 11/19/2019

Checked by: VAS

# **MDDP** CLAREMONT COMMERICAL FILING NO. 2 PROPOSED DRAINAGE CALCULATIONS

(Area Drainage Summary)

From Area Runoff	Coefficient Sumn	nary			OVERL.	4ND		ST	REET / CH	ANNEL FLO	)W	Time of T	ravel (T ,)	INTEN	VSITY *	TOTAL	FLOWS
BASIN	AREA TOTAL	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	Length	Height	$T_{\rm C}$	Length	Slope	Velocity	T <sub>t</sub>	TOTAL	CHECK	I <sub>5</sub>	I <sub>100</sub>	$Q_5$	Q <sub>100</sub>
	(Acres)	From DCM	A Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
A	0.19	0.09	0.36	0.09	40	5.0	5.0	0	0.0%	0.0	0.0	5.0	10.2	5.2	8.7	0.1	0.6
В	1.39	0.81	0.88	0.81	80	1.0	4.4	250	1.6%	2.5	1.7	6.0	11.8	4.9	8.2	5.5	10.1
C	0.30	0.09	0.36	0.09	40	8.0	4.3	0	0.0%	0.0	0.0	4.3	10.2	5.2	8.7	0.1	1.0
D	1.53	0.81	0.88	0.81	60	1.2	3.2	350	2.0%	2.8	2.1	5.3	12.3	5.1	8.5	6.3	11.5
E	1.55	0.81	0.88	0.81	60	1.2	3.2	167	2.0%	2.8	1.0	4.2	11.3	5.2	8.7	6.5	11.8
F	0.36	0.12	0.39	0.12	60	1.2	10.9	30	33.0%	11.5	0.0	10.9	10.5	4.1	6.8	0.2	1.0
$\boldsymbol{G}$	0.29	0.32	0.53	0.32	25	0.5	5.6	0	0.0%	0.0	0.0	5.6	10.1	5.0	8.4	0.5	1.3
Н	0.71	0.09	0.36	0.09	100	17.0	7.2	0	0.0%	0.0	0.0	7.2	10.6	4.6	7.8	0.3	2.0
I	2.75	0.81	0.88	0.81	60	1.2	3.2	425	2.0%	1.4	5.0	8.2	12.7	4.4	7.4	9.8	17.9
J	1.05	0.81	0.88	0.81	60	1.2	3.2	200	2.0%	2.8	1.2	4.4	11.4	5.2	8.7	4.4	8.0
K	0.42	0.81	0.88	0.81	60	1.2	3.2	175	2.0%	2.8	1.0	4.3	11.3	5.2	8.7	1.8	3.2
L	1.32	0.09	0.36	0.09	120	17.0	8.3	0	0.0%	0.0	0.0	8.3	10.7	4.4	7.4	0.5	3.5
M	1.84	0.81	0.88	0.81	100	1.0	5.2	400	1.5%	2.4	2.7	8.0	12.8	4.5	7.5	6.7	12.2
N	0.47	0.12	0.39	0.12	60	1.2	10.9	30	33.0%	11.5	0.0	10.9	10.5	4.1	6.8	0.2	1.3
0	0.16	0.22	0.48	0.22	25	0.5	6.3	0	0.0%	0.0	0.0	6.3	10.1	4.8	8.1	0.2	0.6
P	0.03	0.09	0.36	0.09	120	17.0	8.3	0	0.0%	0.0	0.0	8.3	10.7	4.4	7.4	0.0	0.1
Q	0.11	0.09	0.36	0.09	25	0.5	7.1	0	0.0%	0.0	0.0	7.1	10.1	4.6	7.8	0.0	0.3

<sup>\*</sup> Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: DLM
Date: 11/19/2019

Checked by: VAS

Per DCM ch 6, length of overland flow is max 100 ft. for urban land uses. Revise accordingly.

# MDDP CLAREMONT COMMERICAL FILING NO. 2 PROPOSED DRAINAGE CALCULATIONS

# (Basin Routing Summary)

	From Area Runoff Coefficient Summary				OVE	RLAND		PIPE	/ CHA	NNEL FLO	)W	Time of Travel $(T_t)$	INTE	VSITY *	TOTAL .	FLOWS	
DESIGN POINT	CONTRIBUTING BASINS	CA <sub>5</sub>	CA <sub>100</sub>	C <sub>5</sub> 1	Length	Height	$T_{C}$	Length	Slope	Velocity	T <sub>t</sub>	TOTAL	$I_5$	I <sub>100</sub>	$Q_5$	Q <sub>100</sub>	COMMENTS
	DPS AND/OR PIPES				(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
1	A, B	1.15	1.29				TAKEN FR	OM BASIN	В			6.0	4.9	8.2	5.6	10.6	Proposed PVT 24" Storm Sewer
2	C, D	1.27	1.46				TAKEN FR	OM BASIN	D			5.3	5.1	8.5	6.4	12.4	Proposed PVT 24" Storm Sewer
3	E	1.26	1.36			TAKE	N FROM BA	SIN E (Adj to	Min Tc)	I.		5.0	5.2	8.7	6.5	11.8	Proposed PVT 24" Storm Sewer
4	F, DP 1-3	3.71	4.26			TAK	EN FROM I	DESIGN POI	NT 1			6.0	4.9	8.2	18.2	35.0	PVT Sand Filter Basin FSD Pond 1
	•																
_																	
5	Н, І	2.29	2.67				TAKEN FR	OM BASIN	I	I		8.2	4.4	7.4	10.1	19.8	10' and 15' Type R Inlets
																	(assumed split flows)
6	J, FB DP5	0.85	1.29			TAKE	N FROM BA	SIN J (Adj to	Min Tc)			5.0	5.2	8.7	4.4	11.2	10' and 15' Type R Inlets
																	(assumed split flows)
7	K	0.34	0.37			TAKEN	N FROM BA	SIN K (Adj t	Min Tc)			5.0	5.2	8.7	1.8	3.2	Manhole w/ Grate
·	K							<u> </u>									
8	L, M	1.61	2.09				TAKEN FR	OM BASIN I	M			8.0	4.5	7.5	7.2	15.7	PVT Swale or PVT 24" Storm Sewer
9	DP5, DP7, DP8, N	4.30	5.32			TAI	KEN FROM	DESIGN PO	INT 8			8.0	4.5	7.5	19.2	40.0	PVT Sand Filter Basin FSD Pond 2

Calculated by: DLM
Date: 11/19/2019

Checked by: VAS

This design point should also include flow from design point 6.

# MDDP CLAREMONT COMMERICAL FILING NO. 2 PROPOSED DRAINAGE CALCULATIONS

pipe run 6

(Storm Sewer Routing Summary)

						Inter	ısity*	Fl	ow	Pipe Size
PIPE RUN	$\sqrt{}$	Contributing Pipes/Design Points	Equivalent CA 5	Equivalent CA <sub>100</sub>	Maximum T <sub>C</sub>	$I_5$	I 100	Q 5	Q 100	
1	$\overline{}$	DP1	1.15	1.29	6.0	5.2	8.7	6.5	11.8	PROP 24" PP
2	/	DP2	1.27	1.46	5.3	5.1	8.5	6.4	12.4	PROP 24" PP
3		PR1, PR2	2.41	2.75	6.0	4.9	8.2	11.8	22.6	PROP 30" PP
4		DP3	1.26	1.36	5.0	5.2	8.7	6.5	11.8	PROP 24" PP
5		FOND 1 OUTFALL	1.48	1.89	6.0	4.9	8.2	7.2	15.5	PROP 24" PP
5.1		PIPE 5	1.48	1.89	6.0	4.9	8.2	7.2	15.5	PROP 24" PP
5.2		PIPE 5.1	1.48	1.89	6.0	4.9	8.2	7.2	15.5	PROP 24" PP
6		NLET 1	1.44	1.43	8.2	4.4	7.4	6.4	10.6	PROP 24" PP
7		PIPE 1, INLET 2	2.28	2.24	8.2	4.4	7.4	10.1	16.6	PROP 30" PP
8		INLET 3	0.55	0.80	5.0	5.2	8.7	2.8	6.9	PROP 18" PP
9		PIPE 8, INLET 4	0.86	1.27	5.0	5.2	8.7	4.4	11.0	PROP 24" PP
10		PIPE 9, DP7	1.20	1.64	5.0	5.2	8.7	6.2	14.3	PROP 24" PP
10.1		PIPE 10	1.20	1.64	5.0	5.2	8.7	6.2	14.3	PROP 24" PP
11		POND 2 OUTFALL	2.45	3.07	8.0	4.5	7.5	11.0	23.1	PROP 30" PP
12		PR5.2, PR11	3.93	4.50	8.0	4.5	7.5	17.6	33.8	PROP-24" PP

\* Intensity equations assume a minimum travel time of 5 minutes.

DP - Design Point

PR - Pipe Run

FB- Flow By from Design Point INT- Intercepted Flow from Design Point Calculated by: DLM
Date: 11/20/2019
Checked by: VAS

existing 42" pipe?



CLAREMONT COMMERICAL FILING NO. 2 (PROPOSED CONDITIONS)

Weighted Perce	nt Impervio	usness of Pr	oposed WQ Sand I	Filter Basin 1
Contributing Basins	Area (Acres)	C 5	Impervious % (I)	(Acres)*(I)
A	0.19	0.09	2	0.38
В	1.39	0.81	95	132.29
С	0.30	0.09	2	0.61
D	1.53	0.81	95	145.47
E	1.55	0.81	95	147.28
F	0.36	0.12	7	2.54
Totals	5.33			428.58
Imperviousness % to FSD	80.4			

1.77 A soils 33% 3.57 B soils 67%

5.33 total area

Revise the title to match the other calculation sheets which indicate Claremont Commercial.....

# Claremont Bus. Park Filing No. 2 MASTER DEVELOPMENT DRAINAGE PLAN CALCULATIONS (Pond Volume Calculation)

## **WQCV POND 1**

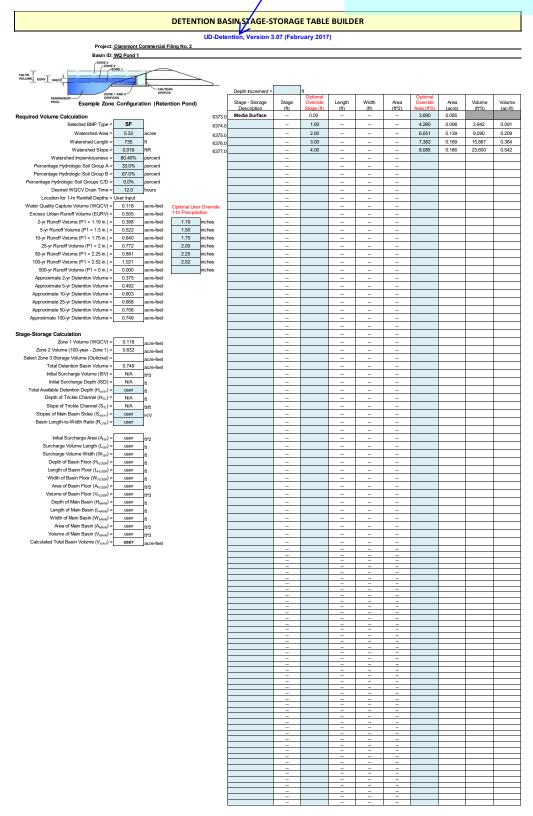
			Stora	age
Elevation	SF	CF	AF	Sum
6373.00	3,690.00	0.00	0.00	0.00
6374.00	4,280.00	3,985.00	0.09	0.09
6375.00	6,051.00	5,165.50	0.12	0.21
6376.00	7,382.00	6,716.50	0.15	0.36
6376.50	8,085.00	3,866.75	0.09	0.45
	Total =	19,734 C Total =		Ac-ft

Calculated by: DLM

Date: 11/20/2019

Checked by:

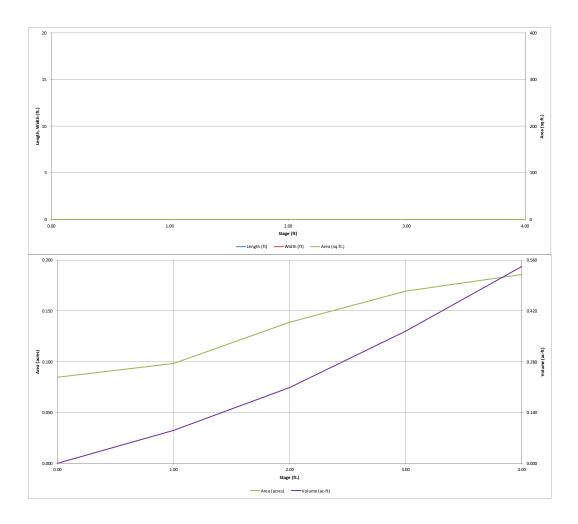
Please use the latest UD detention worksheet by Urban Drainage. Note that the hydraulics and pond design will be reviewed with the final drainage report.



UD-Detention\_v3.07-WQ Pond1.xism, Basin 11/20/2019, 4:07 PM

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)



UD-Deterition\_v3.07-WQ Pond1.xism, Basin 11/20/2019, 4:07 PM

#### UD-Detention, Version 3.07 (February 2017)

Project: Claremont Commercial Filing No. 2



	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	1.26	0.118	Filtration Media
!one 2 (100-year)		0.632	Weir&Pipe (Restrict)
Zone 3			
•		0.749	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = 2.55 ft (distance below the filtration media surface)
Underdrain Orifice Diameter = 1.61 inches

Calculate	a rarameters for	Onaciaia
Underdrain Orifice Area =	0.0	ft <sup>2</sup>
Jnderdrain Orifice Centroid =	0.07	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	N/A	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	N/A	inches

lated Parameters fo	r Plate
N/A	ft <sup>2</sup>
N/A	feet
N/A	feet
N/A	ft <sup>2</sup>
	N/A N/A N/A

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

Stage of Orifice Centroid (ft) N	'A N/A	N/A	N/A	N/A	N/A	N/A	N/A
Orifice Area (sq. inches)	'A N/A	N/A	N/A	N/A	N/A	N/A	N/A

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected	
Invert of Vertical Orifice =			ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =			ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =			inches

<b>Calculated Parameters for Vertical Orifice</b>				
	Not Selected	Not Selected		
Vertical Orifice Area =			ft <sup>2</sup>	
Vertical Orifice Centroid =	•		fee	

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 2 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	1.26		ft (relative to basin bottom at Stage = 0 f
Overflow Weir Front Edge Length =	6.00		feet
Overflow Weir Slope =	0.00		H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	2.91		feet
Overflow Grate Open Area % =	70%		%, grate open area/total area
Debris Clogging % =	50%		%

Calculated	ated Parameters for Overflow Weir			
	Zone 2 Weir	Not Selected		
Height of Grate Upper Edge, $H_t$ =	1.26		feet	
Over Flow Weir Slope Length =	2.91		feet	
Grate Open Area / 100-yr Orifice Area =	4.84		should be	
Overflow Grate Open Area w/o Debris =	12.22		ft <sup>2</sup>	
Overflow Grate Open Area w/ Debris =	6.11		ft <sup>2</sup>	

Jser Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

rice i ipe w/ i low hestriction i late (elicular office, hestrictor i late, of hectange			alai Office)	Calculated I didilicter	3 for Outlet i ipe w/	iow itestriction i lat	
	Zone 2 Restrictor	Not Selected			Zone 2 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.69		ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	2.53		ft <sup>2</sup>
Outlet Pipe Diameter =	24.00		inches O	utlet Orifice Centroid =	0.83		feet
rictor Plate Height Above Pipe Invert =	18.00		inches Half-Central Angle of Re	strictor Plate on Pipe =	2.09	N/A	radians

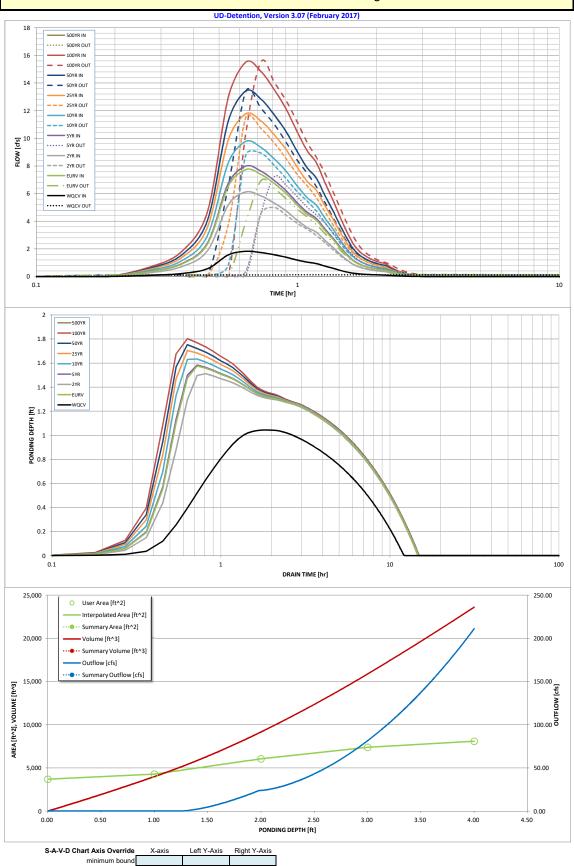
User Input: Emergency Spillway	(Rectangular or Trapezoidal)

2.00	ft (relative to basin bottom at Stage = 0 ft)
15.00	feet
4.00	H:V
1.00	feet
	2.00 15.00 4.00

Calculated Parameters for Spills					
Spillway Design Flow Depth=	0.46	feet			
Stage at Top of Freeboard =	3.46	feet			
sin Area at Ton of Freehoard =	0.18	acres			

Routed Hydrograph Results									
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	0.00
Calculated Runoff Volume (acre-ft) =	0.118	0.505	0.398	0.522	0.640	0.772	0.881	1.021	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.117	0.505	0.398	0.521	0.640	0.772	0.881	1.020	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.01	0.01	0.12	0.41	0.62	0.90	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.0	0.1	0.7	2.2	3.3	4.8	0.0
Peak Inflow Q (cfs) =	1.8	7.7	6.1	8.0	9.8	11.8	13.4	15.5	#N/A
Peak Outflow Q (cfs) =	0.1	6.9	5.0	7.2	8.9	11.5	13.4	15.5	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	95.8	13.5	5.2	4.1	3.2	#N/A
Structure Controlling Flow =	Filtration Media	Overflow Grate 1	#N/A						
Max Velocity through Grate 1 (fps) =	N/A	0.54	0.37	0.5	0.7	0.9	1.0	1.2	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	NXA	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	12	13	13	13	13	12	12	12	#N/A
Time to Drain 99% of Inflow Volume (hours) =	12	14	14	14	14	14	14	14	#N/A
Maximum Ponding Depth (ft) =	1.04	1.58	1.51	1.58	1.63	1.70	1.75	1.80	#N/A
Area at Maximum Ponding Depth (acres) =	0.10	0.12	0.12	0.12	0.12	0.13	0.13	0.13	#N/A
Maximum Volume Stored (acre-ft) =	0.095	0.154	0.147	0.155	0.161	0.170	0.177	0.183	#N/A

\*Provide note indicating that per resolution 16-426 of the BoCC, on-site WQCV is required but on-site stormwater detention is not required per the FDR for Claremont Business Park Fil. 2. This has been requested on previous projects you've done in this area.



maximum bound

Outflow Hydrograph Workbook Filename:

Storm Inflow Hydrographs

UD-Detention, Version 3.07 (February 2017)

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

SOURCE WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK WORKBOOK #N/A

	SOURCE	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	#N/A
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5 40 min	0:00:00	0.00	0.00				0.00		0.00	#81/A
5.43 min		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	0:05:26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
Hydrograph	0:10:52	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
Constant	0:16:17	0.08	0.35	0.27	0.36	0.43	0.52	0.59	0.68	#N/A
0.921	0:21:43	0.22	0.93	0.73	0.96	1.17	1.40	1.60	1.84	#N/A
	0:27:09	0.57	2.38	1.89	2.46	3.00	3.60	4.10	4.73	#N/A
	0:32:35	1.57	6.54	5.18	6.75	8.24	9.90	11.26	12.99	#N/A
	0:38:01	1.82	7.74	6.11	7.99	9.78	11.78	13.42	15.51	#N/A
	0:43:26	1.73	7.38	5.83	7.62	9.33	11.25	12.82	14.83	#N/A
	0:48:52	1.57	6.72	5.30	6.94	8.50	10.24	11.67	13.50	#N/A
	0:54:18	1.39	5.99	4.72	6.19	7.59	9.15	10.44	12.08	#N/A
	0:59:44	1.19	5.17	4.07	5.34	6.55	7.91	9.03	10.46	#N/A
	1:05:10	1.04	4.51	3.55	4.65	5.71	6.89	7.86	9.10	#N/A
	1:10:35	0.94	4.08	3.21	4.21	5.17	6.24	7.13	8.25	#N/A
	1:16:01	0.76	3.36	2.64	3.47	4.27	5.16	5.90	6.84	#N/A
	1:21:27									
		0.61	2.74	2.14	2.83	3.48	4.22	4.83	5.61	#N/A
	1:26:53	0.46	2.10	1.64	2.17	2.68	3.26	3.74	4.35	#N/A
	1:32:19	0.33	1.56	1.21	1.61	2.00	2.44	2.80	3.27	#N/A
	1:37:44	0.24	1.13	0.88	1.17	1.45	1.76	2.02	2.37	#N/A
	1:43:10	0.19	0.88	0.69	0.91	1.12	1.36	1.56	1.82	#N/A
	1:48:36	0.16	0.72	0.56	0.75	0.92	1.12	1.28	1.49	#N/A
	1:54:02	0.14	0.61	0.48	0.63	0.78	0.95	1.09	1.27	#N/A
	1:59:28	0.12	0.54	0.42	0.56	0.69	0.83	0.95	1.11	#N/A
	2:04:53	0.11	0.49	0.38	0.50	0.62	0.75	0.86	1.00	#N/A
	2:10:19	0.10	0.45	0.35	0.46	0.57	0.69	0.79	0.92	#N/A
	2:15:45	0.07	0.33	0.26	0.34	0.42	0.51	0.58	0.67	#N/A
	2:21:11	0.05	0.24	0.19	0.25	0.31	0.37	0.43	0.49	#N/A
	2:26:37	0.04	0.18	0.14	0.18	0.23	0.27	0.31	0.36	#N/A
	2:32:02	0.03	0.13	0.10	0.13	0.17	0.20	0.23	0.27	#N/A
	2:37:28	0.02	0.09	0.07	0.10	0.12	0.14	0.17	0.19	#N/A
	2:42:54	0.01	0.07	0.05	0.07	0.08	0.10	0.12	0.14	#N/A
	2:48:20	0.01	0.05	0.04	0.05	0.06	0.07	0.08	0.10	#N/A
	2:53:46	0.01	0.03	0.02	0.03	0.04	0.05	0.06	0.07	#N/A
	2:59:11	0.00	0.02	0.01	0.02	0.02	0.03	0.03	0.04	#N/A
	3:04:37	0.00	0.02	0.01	0.02	0.02	0.03	0.03	0.04	#N/A
	3:10:03									
		0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	#N/A
	3:15:29	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:20:55	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:26:20	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:31:46	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:37:12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:42:38	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:48:04	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:53:29	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	3:58:55	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:04:21	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:09:47	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:15:13	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:20:38	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:26:04	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:31:30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:36:56	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:42:22	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:47:47	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:53:13	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	4:58:39	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	5:04:05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	5:09:31 5:14:56	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	5:20:22	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A #N/A
	5:25:48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	5:31:14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	5:36:40	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	5:42:05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	5:47:31	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	5:52:57	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	5:58:23	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	6:03:49	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	6:09:14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	6:14:40	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	6:20:06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	6:25:32	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A
	6:30:58	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	#N/A

#### CLAREMONT COMMERICAL FILING NO. 2 (PROPOSED CONDITIONS)

Weighted Perce	nt Impervio	usness of P	roposed WQ Sand I	Filter Basin 2
Contributing Basins	Area (Acres)	C 5	Impervious % (I)	(Acres)*(I)
Н	0.71	0.09	2	1.43
I	2.75	0.81	95	260.80
J	1.05	0.81	95	100.02
K	0.42	0.81	2	0.85
L	1.32	0.09	2	2.63
M	1.84	0.81	95	174.75
N	0.47	0.12	7	3.32
Totals	<b>8.5</b> 7			543.80
Imperviousness of WQ Pond 2	63.5			_

8.57 B soils 8.57 total area

# Claremont Commercial Filing No.2 DRAINAGE REPORT DRAINAGE CALCULATIONS (Pond Volume Calculation)

# WQCV POND 2

			Stora	age
Elevatio	n SF	CF	AF	Sum
6365.5	0 3,292.00	0.00	0.00	0.00
6366.0	0 3,840.00	1,783.00	0.04	0.04
6367.0	5,015.00	4,427.50	0.10	0.14
6368.0	0 6,290.00	5,652.50	0.13	0.27
6369.0	7,665.00	6,977.50	0.16	0.43
	Total =	<u>18,841</u> Total =		Ac-ft

Calculated by: DLM

Date: 3/20/2017

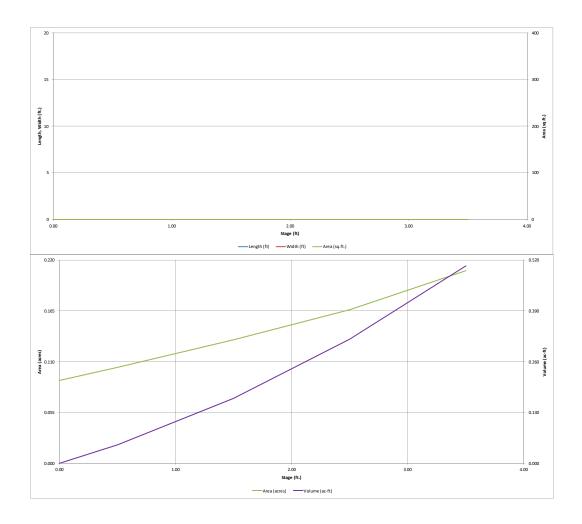
Checked by:

DETENTION BASIN STAGE-STORAGE TABLE BUILDER														
UD-Detention Version 3.07 (February 2017)														
Project: Claremont Commerical Fil No. 2 Basin ID: WQ Pond 2														
7000 to 10 10 7000 to 10 10 7000 to 10														
100.791 0001 0001 0000														
ZONE	1 AND 2	100-YE ORIFIC	EAR CE	7	Depth Increment =		ft Optional	ı			Ontional			
PERMANENT ORIFI POOL Example Zone		tion (Rete	ntion Pond)		Stage - Storage Description	Stage (ft)	Override Stage (ft)	Length (ft)	Width (ft)	Area (ft*2)	Optional Override Area (ft'2)	Area (acre)	Volume (ft*3)	Volume (ac-ft)
Required Volume Calculation		1		65.5	Media Surface	-	0.00	-	-	-	3,907	0.090		
Selected BMP Type = Watershed Area =	<b>SF</b> 8.57	acres /		<b>66</b>			0.50 1.50		-	-	4,521 5,829	0.104	2,062 7,224	0.047
Watershed Length =	665	ft /		68.00		-	2.50		-	-	7,244	0.166	13,818	0.317
Watershed Slope = Watershed Imperviousness =	0.018 63.50%	ft/ft percent		69.00		-	3.50	-	-	-	9,079	0.208	21,980	0.505
Percentage Hydrologic Soil Group A =	0.0%	percent							-	-				
Percentage Hydrologic Soil Group B = Percentage Hydrologic Soil Groups C/D =	100.0%	percent percent				-		-	-	-				
Desired WQCV Drain Time = Location for 1-hr Rainfall Depths =	12.0	hours				-			-	-				
Water Quality Capture Volume (WQCV) =	0.142	acre-feet	Optional Use					-	-					
Excess Urban Runoff Volume (EURV) = 2-yr Runoff Volume (P1 = 1.19 in.) =	0.593 0.490	acre-feet acre-feet	1-hr Precipita 1.19	inches		-		-	-	-				
5-yr Runoff Volume (P1 = 1.5 in.) =	0.656	acre-feet	1.50	inches					-	-				
10-yr Runoff Volume (P1 = 1.75 in.) = 25-yr Runoff Volume (P1 = 2 in.) =	0.846 1.097	acre-feet acre-feet	1.75 2.00	inches inches						-				
50-yr Runoff Volume (P1 = 2.25 in.) =	1.278	acre-feet	2.25	inches		-			-	-				
100-yr Runoff Volume (P1 = 2.52 in.) = 500-yr Runoff Volume (P1 = 0 in.) =	1.516 0.000	acre-feet acre-feet	2.52	inches inches		-		-	-	-				
Approximate 2-yr Detention Volume =	0.459	acre-feet		-					-	-				
Approximate 5-yr Detention Volume = Approximate 10-yr Detention Volume =	0.616 0.788	acre-feet acre-feet							-					
Approximate 25-yr Detention Volume = Approximate 50-yr Detention Volume =	0.850 0.885	acre-feet acre-feet				-			-	-				
Approximate 30-yr Detention Volume =	0.960	acre-feet						-	-					
Stage-Storage Calculation						-			-	-				
Zone 1 Volume (WQCV) =	0.142	acre-feet				_		-	-	-				
Zone 2 Volume (100-year - Zone 1) = Select Zone 3 Storage Volume (Optional) =	0.818	acre-feet acre-feet				-		-	-	-				
Total Detention Basin Volume =	0.960	acre-feet							-	-				
Initial Surcharge Volume (ISV) = Initial Surcharge Depth (ISD) =	user	ft/3				-			-	-				
Total Available Detention Depth (H <sub>total</sub> ) =	user	ft				-		-	-	-				
Depth of Trickle Channel ( $H_{TC}$ ) = Slope of Trickle Channel ( $S_{TC}$ ) =	user	ft/ft				-		-	-	-				
Slopes of Main Basin Sides $(S_{main})$ = Basin Length-to-Width Ratio $(R_{L/W})$ =	user	H:V				-			-	-				
	usei	_				_		-	-	-				
Initial Surcharge Area (A <sub>SV</sub> ) = Surcharge Volume Length (L <sub>SV</sub> ) =	user	ft*2				-		-	-	-				
Surcharge Volume Width (W <sub>ISV</sub> ) =	user	ft							-	-				
Depth of Basin Floor ( $H_{FLOOR}$ ) = Length of Basin Floor ( $L_{FLOOR}$ ) =	user	ft ft				-			-	-				
Width of Basin Floor (W <sub>FLOOR</sub> ) =	user	ft				-			-	-				
Area of Basin Floor ( $A_{FLOOR}$ ) = Volume of Basin Floor ( $V_{FLOOR}$ ) =	user	ft/2 ft/3						-	-					
Depth of Main Basin $(H_{MAIN}) =$ Length of Main Basin $(L_{MAIN}) =$	user	ft ft				-			-	-				
Width of Main Basin (W <sub>MAIN</sub> ) =	user	ft							-	-				
Area of Main Basin (A <sub>MAIN</sub> ) = Volume of Main Basin (V <sub>MAIN</sub> ) =	user	ft/2 ft/3				-			-	-				
Calculated Total Basin Volume (V <sub>total</sub> ) =	user	acre-feet							-	-				
						-		=	-	=				
						-		-	-	-				
						-			-	-				
						-		-	-	-				
						-		-	-	-				
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UD-Deterition\_v3.07-WQ Pond2.xism, Basin 11/20/2019, 4:11 PM

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)



UD-Deterition\_v3.07-WQ Pond2.xism, Basin 11/20/2019, 4:11 PM

#### UD-Detention, Version 3.07 (February 2017)



	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	1.31	0.142	Filtration Media
!one 2 (100-year)		0.818	Weir&Pipe (Restrict)
Zone 3			
'		0.960	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = 2.65 ft (distance below the filtration media surface)

Underdrain Orifice Diameter = 1.75

Calculate	ed Parameters for Un	iderdrai
Underdrain Orifice Area =	0.0	ft <sup>2</sup>
Jnderdrain Orifice Centroid =	0.07	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	N/A	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	N/A	inches
Orifice Plate: Orifice Area per Row =	N/A	inches

lated Parameters fo	r Plate
N/A	ft <sup>2</sup>
N/A	feet
N/A	feet
N/A	ft <sup>2</sup>
	N/A N/A N/A

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (optional)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	N/A							
Orifice Area (sq. inches)	N/A							

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Orifice Area (sq. inches)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected	
Invert of Vertical Orifice =			ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =			ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =			inches

<b>Calculated Parameters for Vertical Orifice</b>						
	Not Selected	Not Selected				
Vertical Orifice Area =			ft <sup>2</sup>			
Vertical Orifice Centroid =	•		feet			

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 2 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	1.31		ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	7.00		feet
Overflow Weir Slope =	0.00		H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	2.91		feet
Overflow Grate Open Area % =	70%		%, grate open area/total area
Debris Clogging % =	50%		%

Calculated Parameters for Overflow Weir					
	Zone 2 Weir	Not Selected			
Height of Grate Upper Edge, $H_t$ =	1.31		feet		
Over Flow Weir Slope Length =	2.91		feet		
Grate Open Area / 100-yr Orifice Area =	6.41		should be		
Overflow Grate Open Area w/o Debris =	14.26		ft <sup>2</sup>		
Overflow Grate Open Area w/ Debris =	7.13		ft <sup>2</sup>		
·-					

Outlet ripe w/ riow Restriction riate (Circular Office, Restrictor riate, or Rectangular Office)			Calculated Farameters for Outlet Fipe w/ Flow Restriction Flate				
	Zone 2 Restrictor	Not Selected			Zone 2 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	3.00		ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	2.22		ft <sup>2</sup>
Outlet Pipe Diameter =	24.00		inches	Outlet Orifice Centroid =	0.75		feet
estrictor Plate Height Above Pipe Invert =	16.00		inches Half-Central Angle of F	Restrictor Plate on Pipe =	1.91	N/A	radians

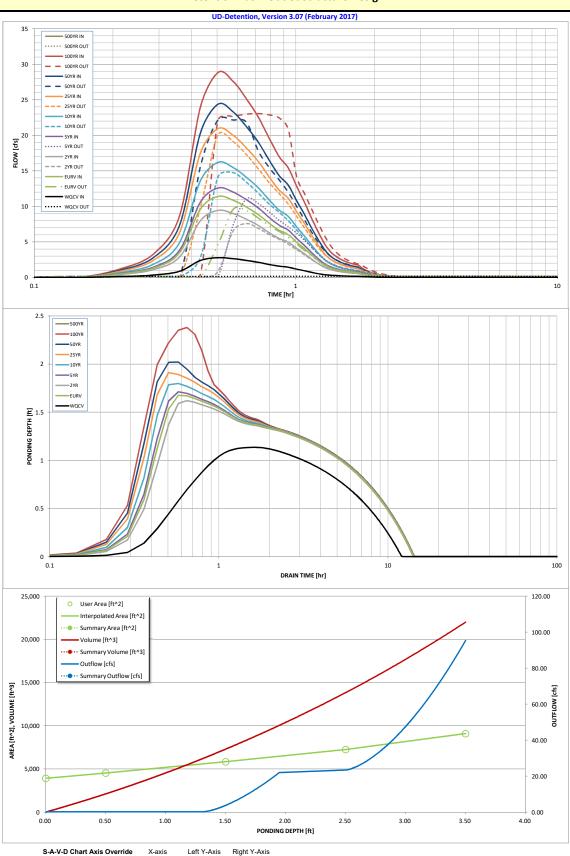
User Input: Emergency Spillway (Rectangular or Trapezoidal)

Jser Input: Emergency Spillway (Rectang	ular or Trapezoidal)		Calculate	d Parameters
Spillway Invert Stage=	2.50	ft (relative to basin bottom at Stage = 0 ft)	Spillway Design Flow Depth=	0.57
Spillway Crest Length =	20.00	feet	Stage at Top of Freeboard =	4.07
Spillway End Slopes =	4.00	H:V	Basin Area at Top of Freeboard =	0.21
Freeboard above Max Water Surface =	1.00	feet	_	

Routed Hydrograph Results									
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	0.00
Calculated Runoff Volume (acre-ft) =	0.142	0.593	0.490	0.656	0.846	1.097	1.278	1.516	0.000
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.141	0.593	0.489	0.655	0.845	1.096	1.277	1.515	#N/A
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.01	0.03	0.25	0.79	1.10	1.46	0.00
Predevelopment Peak Q (cfs) =	0.0	0.0	0.1	0.2	2.1	6.8	9.4	12.5	0.0
Peak Inflow Q (cfs) =	2.8	11.4	9.4	12.6	16.2	20.9	24.4	28.8	#N/A
Peak Outflow Q (cfs) =	0.2	9.6	7.6	11.0	14.7	20.0	22.1	23.1	#N/A
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	51.3	6.9	3.0	2.4	1.8	#N/A
Structure Controlling Flow =	Filtration Media	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	#N/A				
Max Velocity through Grate 1 (fps) =	N/A	0.62	0.49	0.∇	1.0	1.4	1.5	1.6	#N/A
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	#N/A
Time to Drain 97% of Inflow Volume (hours) =	12	13	13	13	12	11	11	10	#N/A
Time to Drain 99% of Inflow Volume (hours) =	12	14	14	14	14	13	13	13	#N/A
Maximum Ponding Depth (ft) =	1.13	1.67	1.62	1.71	1.80	1.91	2.02	2.38	#N/A
Area at Maximum Ponding Depth (acres) =	0.12	0.14	0.14	0.14	0.14	0.15	0.15	0.16	#N/A
Maximum Volume Stored (acre-ft) =	0.120	0.190	0.183	0.196	0.207	0.225	0.241	0.298	#N/A

\*Provide note indicating that per resolution 16-426 of the BoCC, on-site WQCV is required but on-site stormwater detention is not required per the FDR for Claremont Business Park Fil. 2. This has been requested on previous projects you've done in this area.

#### **Detention Basin Outlet Structure Design**



minimum bound maximum bound

#### **Detention Basin Outlet Structure Design**

Outflow Hydrograph Workbook Filename:

Storm Inflow Hydrographs

UD-Detention, Version 3.07 (February 2017)

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

SOURCE WORKBOOK WORKBOO

A.32 min   0:00:00   0.00	Year [cfs]	
4.32 min		500 Year [cfs]
Description   Description	0.00	#NI/A
Hydrograph Constant 0:12:58 0.13 0.51 0.42 0.56 0.71 0.92 1.06 0.1157 0:17:17 0.34 1.36 1.13 1.50 1.93 2.48 2.88 0.2136 0.86 3.50 2.90 3.86 4.95 6.37 7.40 0.25:55 2.38 9.61 7.97 10.59 13.59 17.50 20.31 0.30:14 2.77 11.40 9.43 12:58 16:19 20.93 24.35 0.34:34 2.63 10.87 8.99 12.00 15.47 20.00 23.29 0.38:63 2.39 9.90 8.18 10.93 14.08 18.21 21.20 0.34:34 2.63 10.87 8.99 12.00 15.47 20.00 23.29 0.34:34 2.63 10.87 8.99 12.00 15.47 20.00 23.29 0.34:35 0.34:34 2.63 10.87 8.99 12.00 15.47 20.00 23.29 0.34:31 1.81 7.63 6.29 8.43 10.89 14.12 16.47 0.51:50 1.58 6.65 5.48 7.34 9.48 12.29 14.32 0.56:10 1.43 6.02 4.97 6.65 8.59 11.14 12.99 1.00:50:50 1.58 6.65 5.48 7.34 9.48 12.29 14.32 1.00:50:10 1.43 6.02 4.97 6.65 8.59 11.14 12.99 1.00:29 1.16 4.96 4.09 5.49 7.11 9.24 10.79 1.00:49 1.10:48 0.93 4.05 3.33 4.49 5.82 7.58 8.86 1.09:07 0.70 3.12 2.55 3.46 4.50 5.88 6.90 1.13:26 0.51 2.32 1.89 2.57 3.37 4.43 5.21 1.17:46 0.37 1.68 1.37 1.68 1.37 1.86 2.43 3.21 3.79 1.12:20 5 0.29 1.30 1.07 1.44 1.88 2.47 2.90 1.12:20 5 0.29 1.30 1.07 1.44 1.88 2.47 2.90 1.12:20 5 0.29 1.30 1.07 1.44 1.88 2.47 2.90 1.12:20 5 0.29 1.30 1.07 1.44 1.88 2.47 2.90 1.12:20.50 0.29 1.30 1.07 1.44 1.88 2.47 2.90 1.12:20.50 0.29 1.30 1.07 1.44 1.88 2.47 2.90 1.12:20.50 0.29 1.30 1.07 1.44 1.88 2.47 2.90 1.12:20.50 0.29 1.30 0.66 0.88 1.19 1.54 2.02 2.38 1.30:43 0.21 0.91 0.75 1.01 1.31 1.71 2.01 1.33:0.43 0.21 0.91 0.75 1.01 1.31 1.71 2.01 1.35:0.2 0.18 0.80 0.66 0.88 1.19 1.54 2.02 2.38 1.36:43 1.37 1.56 1.33:0.2 0.18 0.80 0.66 0.88 1.15 1.50 1.76 0.78 1.15:1.15:1.15:1.15:1.15:1.15:1.15:1.15	0.00	#N/A
Constant   0:12:58	0.00	#N/A
1.157	0.00	#N/A
0.21:36         0.86         3.50         2.90         3.86         4.95         6.37         7.40           0.25:55         2.38         9.61         7.97         10.59         13.59         17.50         20.31           0.30:14         2.77         11.40         9.43         12.58         16.19         20.93         24.35           0.38:34         2.63         10.87         8.99         12.00         15.47         20.00         23.29           0.38:53         2.39         9.90         8.18         10.93         14.08         18.21         21.20           0.47:31         1.81         7.63         6.29         8.43         10.89         16.31         19.00           0.47:31         1.81         7.63         6.29         8.43         10.89         14.12         16.47           0.551:50         1.58         6.65         5.48         7.34         9.48         12.29         14.32           0.56:10         1.43         6.02         4.97         6.65         8.59         11.14         12.99           1:00:29         1.16         4.96         4.09         5.49         7.11         9.24         10.79           1:04:48	1.25	#N/A
0.25:55         2.38         9.61         7.97         10.59         13.59         17.50         20.31           0.30:14         2.77         11.40         9.43         12.58         16.19         20.93         24.35           0.34:34         2.63         10.87         8.99         12.00         15.47         20.00         23.29           0.43:12         2.12         8.84         7.30         9.76         12.59         16.31         19.00           0.47:31         1.81         7.63         6.29         8.43         10.89         14.12         16.47           0.51:50         1.58         6.65         5.48         7.34         9.48         12.29         14.32           0.56:10         1.43         6.02         4.97         6.65         8.59         11.14         12.99           1:00:29         1.16         4.96         4.09         5.49         7.11         9.24         10.79           1:04:48         0.93         4.05         3.33         4.49         5.82         7.58         8.86           1:09:07         0.70         3.12         2.55         3.46         4.50         5.89         6.90           1:13:26	3.40	#N/A
0:30:14         2.77         11.40         9.43         12.58         16.19         20.93         24.35           0:34:34         2.63         10.87         8.99         12.00         15.47         20.00         23.29           0:38:53         2.39         9.90         8.18         10.93         14.08         18.21         21.20           0:43:12         2.12         8.84         7.30         9.76         12.59         16.31         19.00           0:47:31         1.81         7.63         6.29         8.43         10.89         14.12         16.47           0:551:50         1.58         6.65         5.48         7.34         9.48         12.29         14.32           0:56:10         1.43         6.02         4.97         6.65         8.59         11.14         12.99           1:00:29         1.16         4.96         4.09         5.49         7.11         9.24         10.79           1:04:48         0.93         4.05         3.33         4.49         5.82         7.58         8.86           1:09:07         0.70         3.12         2.55         3.46         4.50         5.89         6.90           1:13:26	8.73	#N/A
0:34:34         2.63         10.87         8.99         12.00         15.47         20.00         23.29           0:38:53         2.39         9.90         8.18         10.93         14.08         18.21         21.20           0:43:12         2.12         8.84         7.30         9.76         12.59         16.31         19.00           0:51:50         1.58         6.65         5.48         7.34         9.48         12.29         14.32           0:56:10         1.43         6.02         4.97         6.65         8.59         11.14         12.99           1:00:29         1.16         4.96         4.09         5.49         7.11         9.24         10.79           1:04:48         0.93         4.05         3.33         4.49         5.82         7.58         8.86           1:09:07         0.70         3.12         2.55         3.46         4.50         5.89         6.90           1:13:26         0.51         2.32         1.89         2.57         3.37         4.43         5.21           1:7:46         0.37         1.68         1.37         1.86         2.43         3.21         3.79           1:20:5         0.2	23.97	#N/A
0:38:53         2.39         9.90         8.18         10.93         14.08         18.21         21.20           0:43:12         2.12         8.84         7.30         9.76         12.59         16.31         19.00           0:47:31         1.81         7.63         6.29         8.43         10.89         14.12         16.47           0:55:50         1.58         6.65         5.48         7.34         9.48         12.29         14.32           0:56:10         1.43         6.02         4.97         6.65         8.59         11.14         12.99           1:00:29         1.16         4.96         4.09         5.49         7.11         9.24         10.79           1:04:48         0.93         4.05         3.33         4.49         5.82         7.58         8.86           1:09:07         0.70         3.12         2.55         3.46         4.50         5.89         6.90           1:13:26         0.51         2.32         1.89         2.57         3.37         4.43         5.21           1:17:46         0.37         1.68         1.37         1.86         2.43         3.21         3.79           1:26:24         0.2	28.82	#N/A
0:43:12         2:12         8.84         7:30         9.76         12:59         16:31         19:00           0:47:31         1.81         7:63         6:29         8.43         10:89         14:12         16:47           0:51:50         1.58         6:65         5.48         7:34         9.48         12:29         14:32           0:56:10         1.43         6:02         4.97         6:65         8:59         11:14         12:99           1:00:29         1.16         4.96         4.09         5.49         7:11         9:24         10:79           1:04:48         0.93         4.05         3:33         4.49         5.82         7:58         8:86           1:09:07         0.70         3:12         2:55         3.46         4.50         5.89         6:90           1:13:26         0.51         2:32         1:89         2:57         3:37         4.43         5:21           1:17:46         0.37         1:68         1:37         1:86         2:43         3:21         3:79           1:26:24         0.24         1:07         0:88         1:19         1:54         2:02         2:38           1:30:43         0:21 <td>27.58</td> <td>#N/A</td>	27.58	#N/A
0:43:12         2:12         8.84         7:30         9.76         12:59         16:31         19:00           0:47:31         1.81         7:63         6:29         8.43         10:89         14:12         16:47           0:51:50         1.58         6:65         5.48         7:34         9.48         12:29         14:32           0:56:10         1.43         6:02         4.97         6:65         8:59         11:14         12:99           1:00:29         1.16         4.96         4.09         5.49         7:11         9:24         10:79           1:04:48         0.93         4.05         3:33         4.49         5.82         7:58         8:86           1:09:07         0.70         3:12         2:55         3.46         4.50         5.89         6:90           1:13:26         0.51         2:32         1:89         2:57         3:37         4.43         5:21           1:17:46         0.37         1:68         1:37         1:86         2:43         3:21         3:79           1:26:24         0.24         1:07         0:88         1:19         1:54         2:02         2:38           1:30:43         0:21 <td>25.10</td> <td>#N/A</td>	25.10	#N/A
0:47:31         1.81         7.63         6.29         8.43         10.89         14.12         16.47           0:51:50         1.58         6.65         5.48         7.34         9.48         12.29         14.32           0:56:10         1.43         6.02         4.97         6.65         8.59         11.14         12.99           1:00:29         1.16         4.96         4.09         5.49         7.11         9.24         10.79           1:04:48         0.93         4.05         3.33         4.49         5.82         7.58         8.86           1:09:07         0.70         3.12         2.55         3.46         4.50         5.89         6.90           1:13:26         0.51         2.32         1.89         2.57         3.37         4.43         5.21           1:17:46         0.37         1.68         1.37         1.86         2.43         3.21         3.79           1:26:24         0.24         1.07         0.88         1.19         1.54         2.02         2.38           1:30:43         0.21         0.91         0.75         1.01         1.31         1.71         2.01           1:35:02         0.18	22.51	#N/A
0:51:50         1.58         6.65         5.48         7.34         9.48         12.29         14.32           0:56:10         1.43         6.02         4.97         6.65         8.59         11.14         12.99           1:00:29         1.16         4.96         4.09         5.49         7.11         9.24         10.79           1:04:48         0.93         4.05         3.33         4.49         5.82         7.58         8.86           1:09:07         0.70         3.12         2.55         3.46         4.50         5.89         6.90           1:13:26         0.51         2.32         1.89         2.57         3.37         4.43         5.21           1:17:46         0.37         1.68         1.37         1.86         2.43         3.21         3.79           1:22:05         0.29         1.30         1.07         1.44         1.88         2.47         2.90           1:26:24         0.24         1.07         0.88         1.19         1.54         2.02         2.38           1:30:43         0.21         0.91         0.75         1.01         1.31         1.71         2.01           1:35:02         0.18	19.54	#N/A
0:56:10         1.43         6.02         4.97         6.65         8.59         11.14         12.99           1:00:29         1.16         4.96         4.09         5.49         7.11         9.24         10.79           1:04:48         0.93         4.05         3.33         4.49         5.82         7.58         8.86           1:09:07         0.70         3.12         2.55         3.46         4.50         5.89         6.90           1:13:26         0.51         2.32         1.89         2.57         3.37         4.43         5.21           1:77:46         0.37         1.68         1.37         1.86         2.43         3.21         3.79           1:22:05         0.29         1.30         1.07         1.44         1.88         2.47         2.90           1:26:24         0.24         1.07         0.88         1.19         1.54         2.02         2.38           1:30:43         0.21         0.91         0.75         1.01         1.31         1.71         2.01           1:35:02         0.18         0.80         0.66         0.88         1.15         1.50         1.76           1:39:22         0.17	16.98	#N/A
1:00:29         1.16         4.96         4.09         5.49         7.11         9.24         10.79           1:04:48         0.93         4.05         3.33         4.49         5.82         7.58         8.86           1:09:07         0.70         3.12         2.55         3.46         4.50         5.89         6.90           1:13:26         0.51         2.32         1.89         2.57         3.37         4.43         5.21           1:17:46         0.37         1.68         1.37         1.86         2.43         3.21         3.79           1:22:05         0.29         1.30         1.07         1.44         1.88         2.47         2.90           1:26:24         0.24         1.07         0.88         1.19         1.54         2.02         2.38           1:30:43         0.21         0.91         0.75         1.01         1.31         1.71         2.01           1:35:02         0.18         0.80         0.66         0.88         1.15         1.50         1.76           1:39:02         0.17         0.72         0.59         0.80         1.03         1.35         1.58           1:43:41         0.15	15.40	#N/A
1:04:48         0.93         4.05         3.33         4.49         5.82         7.58         8.86           1:09:07         0.70         3.12         2.55         3.46         4.50         5.89         6.90           1:13:26         0.51         2.32         1.89         2.57         3.37         4.43         5.21           1:17:46         0.37         1.68         1.37         1.86         2.43         3.21         3.79           1:22:05         0.29         1.30         1.07         1.44         1.88         2.47         2.90           1:26:24         0.24         1.07         0.88         1.19         1.54         2.02         2.38           1:30:43         0.21         0.91         0.75         1.01         1.31         1.71         2.01           1:35:02         0.18         0.80         0.66         0.88         1.15         1.50         1.76           1:39:22         0.17         0.72         0.59         0.80         1.03         1.35         1.58           1:43:41         0.15         0.66         0.55         0.74         0.95         1.24         1.46           1:48:00         0.11	12.81	#N/A
1:09:07         0.70         3.12         2.55         3.46         4.50         5.89         6.90           1:13:26         0.51         2.32         1.89         2.57         3.37         4.43         5.21           1:17:46         0.37         1.68         1.37         1.86         2.43         3.21         3.79           1:22:05         0.29         1.30         1.07         1.44         1.88         2.47         2.90           1:26:24         0.24         1.07         0.88         1.19         1.54         2.02         2.38           1:30:43         0.21         0.91         0.75         1.01         1.31         1.71         2.01           1:35:02         0.18         0.80         0.66         0.88         1.15         1.50         1.76           1:39:22         0.17         0.72         0.59         0.80         1.03         1.35         1.58           1:43:41         0.15         0.66         0.55         0.74         0.95         1.24         1.46           1:48:00         0.11         0.49         0.40         0.54         0.70         0.91         1.07           1:56:19         0.08		
1:13:26         0.51         2.32         1.89         2.57         3.37         4.43         5.21           1:17:46         0.37         1.68         1.37         1.86         2.43         3.21         3.79           1:22:05         0.29         1.30         1.07         1.44         1.88         2.47         2.90           1:26:24         0.24         1.07         0.88         1.19         1.54         2.02         2.38           1:30:43         0.21         0.91         0.75         1.01         1.31         1.71         2.01           1:35:02         0.18         0.80         0.66         0.88         1.15         1.50         1.76           1:39:22         0.17         0.72         0.59         0.80         1.03         1.35         1.58           1:43:41         0.15         0.66         0.55         0.74         0.95         1.24         1.46           1:48:00         0.01         0.49         0.40         0.54         0.70         0.91         1.07           1:56:38         0.06         0.26         0.29         0.40         0.51         0.67         0.78           1:56:38         0.04	10.54	#N/A
1:17:46         0.37         1.68         1.37         1.86         2.43         3.21         3.79           1:22:05         0.29         1.30         1.07         1.44         1.88         2.47         2.90           1:26:24         0.24         1.07         0.88         1.19         1.54         2.02         2.38           1:30:43         0.21         0.91         0.75         1.01         1.31         1.71         2.01           1:35:502         0.18         0.80         0.66         0.88         1.15         1.50         1.76           1:39:22         0.17         0.72         0.59         0.80         1.03         1.35         1.58           1:43:41         0.15         0.66         0.55         0.74         0.95         1.24         1.46           1:48:00         0.11         0.49         0.40         0.54         0.70         0.91         1.07           1:56:38         0.06         0.26         0.29         0.40         0.51         0.67         0.78           1:56:38         0.06         0.26         0.22         0.29         0.38         0.49         0.58           2:00:58         0.04	8.23	#N/A
1:22:05         0.29         1.30         1.07         1.44         1.88         2.47         2.90           1:26:24         0.24         1.07         0.88         1.19         1.54         2.02         2.38           1:30:43         0.21         0.91         0.75         1.01         1.31         1.71         2.01           1:35:02         0.18         0.80         0.66         0.88         1.15         1.50         1.76           1:39:22         0.17         0.72         0.59         0.80         1.03         1.35         1.58           1:43:41         0.15         0.66         0.55         0.74         0.95         1.24         1.46           1:48:00         0.11         0.49         0.40         0.54         0.70         0.91         1.07           1:56:38         0.06         0.26         0.29         0.40         0.51         0.67         0.78           1:56:38         0.06         0.26         0.22         0.29         0.38         0.49         0.58           2:00:58         0.04         0.19         0.16         0.21         0.28         0.36         0.43           2:05:17         0.03	6.24	#N/A
1:26:24         0.24         1.07         0.88         1.19         1.54         2.02         2.38           1:30:43         0.21         0.91         0.75         1.01         1.31         1.71         2.01           1:35:02         0.18         0.80         0.66         0.88         1.15         1.50         1.76           1:39:22         0.17         0.72         0.59         0.80         1.03         1.35         1.58           1:43:41         0.15         0.66         0.55         0.74         0.95         1.24         1.46           1:48:00         0.11         0.49         0.40         0.54         0.70         0.91         1.07           1:52:19         0.08         0.36         0.29         0.40         0.51         0.67         0.78           1:56:38         0.06         0.26         0.22         0.29         0.38         0.49         0.58           2:00:58         0.04         0.19         0.16         0.21         0.28         0.36         0.43           2:05:17         0.03         0.14         0.11         0.15         0.20         0.26         0.31           2:09:36         0.02	4.56	#N/A
1:30:43         0.21         0.91         0.75         1.01         1.31         1.71         2.01           1:35:02         0.18         0.80         0.66         0.88         1.15         1.50         1.76           1:39:22         0.17         0.72         0.59         0.80         1.03         1.35         1.58           1:43:41         0.15         0.66         0.55         0.74         0.95         1.24         1.46           1:48:00         0.11         0.49         0.40         0.54         0.70         0.91         1.07           1:52:19         0.08         0.36         0.29         0.40         0.51         0.67         0.78           1:56:38         0.06         0.26         0.22         0.29         0.38         0.49         0.58           2:00:58         0.04         0.19         0.16         0.21         0.28         0.36         0.43           2:05:17         0.03         0.14         0.11         0.15         0.20         0.26         0.31           2:09:36         0.02         0.10         0.08         0.11         0.14         0.19         0.22           2:13:55         0.01	3.48	#N/A
1:35:02         0.18         0.80         0.66         0.88         1.15         1.50         1.76           1:39:22         0.17         0.72         0.59         0.80         1.03         1.35         1.58           1:43:41         0.15         0.66         0.55         0.74         0.95         1.24         1.46           1:48:00         0.11         0.49         0.40         0.54         0.70         0.91         1.07           1:52:19         0.08         0.36         0.29         0.40         0.51         0.67         0.78           1:56:38         0.06         0.26         0.22         0.29         0.38         0.49         0.58           2:00:58         0.04         0.19         0.16         0.21         0.28         0.36         0.43           2:05:17         0.03         0.14         0.11         0.15         0.20         0.26         0.31           2:09:36         0.02         0.10         0.08         0.11         0.14         0.19         0.22           2:13:55         0.01         0.07         0.06         0.08         0.10         0.13         0.16           2:18:14         0.01	2.84	#N/A
1:39:22         0.17         0.72         0.59         0.80         1.03         1.35         1.58           1:43:41         0.15         0.66         0.55         0.74         0.95         1.24         1.46           1:48:00         0.11         0.49         0.40         0.54         0.70         0.91         1.07           1:55:38         0.06         0.26         0.29         0.40         0.51         0.67         0.78           1:56:38         0.06         0.26         0.22         0.29         0.38         0.49         0.58           2:00:58         0.04         0.19         0.16         0.21         0.28         0.36         0.43           2:09:36         0.02         0.10         0.08         0.11         0.14         0.19         0.22           2:13:55         0.01         0.07         0.06         0.08         0.10         0.13         0.16           2:18:14         0.01         0.05         0.04         0.05         0.07         0.09         0.11           2:22:34         0.01         0.03         0.02         0.03         0.04         0.05         0.06           2:26:53         0.00	2.40	#N/A
1:43:41         0.15         0.66         0.55         0.74         0.95         1.24         1.46           1:48:00         0.11         0.49         0.40         0.54         0.70         0.91         1.07           1:52:19         0.08         0.36         0.29         0.40         0.51         0.67         0.78           1:56:38         0.06         0.26         0.22         0.29         0.38         0.49         0.58           2:00:58         0.04         0.19         0.16         0.21         0.28         0.36         0.43           2:05:17         0.03         0.14         0.11         0.15         0.20         0.26         0.31           2:09:36         0.02         0.10         0.08         0.11         0.14         0.19         0.22           2:13:55         0.01         0.07         0.06         0.08         0.10         0.13         0.16           2:18:14         0.01         0.05         0.04         0.05         0.07         0.09         0.11           2:22:34         0.01         0.03         0.02         0.03         0.04         0.05         0.06           2:26:53         0.00	2.10	#N/A
1:48:00     0.11     0.49     0.40     0.54     0.70     0.91     1.07       1:52:19     0.08     0.36     0.29     0.40     0.51     0.67     0.78       1:56:38     0.06     0.26     0.22     0.29     0.38     0.49     0.58       2:00:58     0.04     0.19     0.16     0.21     0.28     0.36     0.43       2:05:17     0.03     0.14     0.11     0.15     0.20     0.26     0.31       2:09:36     0.02     0.10     0.08     0.11     0.14     0.19     0.22       2:13:55     0.01     0.07     0.06     0.08     0.10     0.13     0.16       2:18:14     0.01     0.05     0.04     0.05     0.07     0.09     0.11       2:22:34     0.01     0.03     0.02     0.03     0.04     0.05     0.06       2:26:53     0.00     0.01     0.01     0.01     0.01     0.02     0.03     0.03	1.89	#N/A
1:52:19         0.08         0.36         0.29         0.40         0.51         0.67         0.78           1:56:38         0.06         0.26         0.22         0.29         0.38         0.49         0.58           2:00:58         0.04         0.19         0.16         0.21         0.28         0.36         0.43           2:05:17         0.03         0.14         0.11         0.15         0.20         0.26         0.31           2:09:36         0.02         0.10         0.08         0.11         0.14         0.19         0.22           2:13:55         0.01         0.07         0.06         0.08         0.10         0.13         0.16           2:18:14         0.01         0.05         0.04         0.05         0.07         0.09         0.11           2:22:34         0.01         0.03         0.02         0.03         0.04         0.05         0.06           2:26:53         0.00         0.01         0.01         0.01         0.02         0.03         0.03	1.73	#N/A
1:56:38         0.06         0.26         0.22         0.29         0.38         0.49         0.58           2:00:58         0.04         0.19         0.16         0.21         0.28         0.36         0.43           2:05:17         0.03         0.14         0.11         0.15         0.20         0.26         0.31           2:09:36         0.02         0.10         0.08         0.11         0.14         0.19         0.22           2:13:55         0.01         0.07         0.06         0.08         0.10         0.13         0.16           2:18:14         0.01         0.05         0.04         0.05         0.07         0.09         0.11           2:22:34         0.01         0.03         0.02         0.03         0.04         0.05         0.06           2:26:53         0.00         0.01         0.01         0.01         0.02         0.03         0.03	1.28	#N/A
2:00:58         0.04         0.19         0.16         0.21         0.28         0.36         0.43           2:05:17         0.03         0.14         0.11         0.15         0.20         0.26         0.31           2:09:36         0.02         0.10         0.08         0.11         0.14         0.19         0.22           2:13:55         0.01         0.07         0.06         0.08         0.10         0.13         0.16           2:18:14         0.01         0.05         0.04         0.05         0.07         0.09         0.11           2:22:34         0.01         0.03         0.02         0.03         0.04         0.05         0.06           2:26:53         0.00         0.01         0.01         0.01         0.02         0.03         0.03         0.03	0.93	#N/A
2:05:17         0.03         0.14         0.11         0.15         0.20         0.26         0.31           2:09:36         0.02         0.10         0.08         0.11         0.14         0.19         0.22           2:13:55         0.01         0.07         0.06         0.08         0.10         0.13         0.16           2:18:14         0.01         0.05         0.04         0.05         0.07         0.09         0.11           2:22:34         0.01         0.03         0.02         0.03         0.04         0.05         0.06           2:26:53         0.00         0.01         0.01         0.01         0.02         0.03         0.03	0.69	#N/A
2:09:36         0.02         0.10         0.08         0.11         0.14         0.19         0.22           2:13:55         0.01         0.07         0.06         0.08         0.10         0.13         0.16           2:18:14         0.01         0.05         0.04         0.05         0.07         0.09         0.11           2:22:34         0.01         0.03         0.02         0.03         0.04         0.05         0.06           2:26:53         0.00         0.01         0.01         0.01         0.02         0.03         0.03	0.51	#N/A
2:13:55         0.01         0.07         0.06         0.08         0.10         0.13         0.16           2:18:14         0.01         0.05         0.04         0.05         0.07         0.09         0.11           2:22:34         0.01         0.03         0.02         0.03         0.04         0.05         0.06           2:26:53         0.00         0.01         0.01         0.01         0.02         0.03         0.03	0.37	#N/A
2:13:55         0.01         0.07         0.06         0.08         0.10         0.13         0.16           2:18:14         0.01         0.05         0.04         0.05         0.07         0.09         0.11           2:22:34         0.01         0.03         0.02         0.03         0.04         0.05         0.06           2:26:53         0.00         0.01         0.01         0.01         0.02         0.03         0.03	0.26	#N/A
2:18:14     0.01     0.05     0.04     0.05     0.07     0.09     0.11       2:22:34     0.01     0.03     0.02     0.03     0.04     0.05     0.06       2:26:53     0.00     0.01     0.01     0.01     0.02     0.03     0.03	0.19	#N/A
2:22:34         0.01         0.03         0.02         0.03         0.04         0.05         0.06           2:26:53         0.00         0.01         0.01         0.01         0.02         0.03         0.03         0.03	0.13	#N/A
2:26:53 0.00 0.01 0.01 0.01 0.02 0.03 0.03	0.08	#N/A
	0.04	#N/A
	0.02	#N/A
	0.00	#N/A
2:39:50	0.00	#N/A
2:44:10 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
2:48:29 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
2:52:48 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
2:57:07 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
3:01:26 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
3:05:46 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
3:10:05 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
3:14:24 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
3:18:43 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
3:23:02 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
3:27:22 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
3:31:41 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
3:36:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
3:40:19 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
3:44:38 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
3:48:58 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
3:53:17 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
3:57:36 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
4:01:55 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
4:06:14 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
4:10:34 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	0.00	#N/A
4:14:53	0.00	#N/A
4:19:12         0.00	0.00	#N/A #N/A
4:23:51 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	0.00	#N/A
4.27.30 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
4:36:29 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
4:40:48 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
4:45:07 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
4:49:26 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
4:53:46 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
4:58:05 0.00 0.00 0.00 0.00 0.00 0.00 0.00		mis/A
5:02:24 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A
5:06:43 0.00 0.00 0.00 0.00 0.00 0.00 0.00		
5:11:02 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00	#N/A

	WOI KS	nieet for Pipe i
Project Description		
Friction Mothed	Manning	
Friction Method	Formula	
Solve For	Normal Depth	_
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.005 ft/ft	
Diameter	24.0 in	
Discharge	11.80 cfs	
Results		
Normal Depth	15.3 in	
Flow Area	2.1 ft <sup>2</sup>	
Wetted Perimeter	3.7 ft	
Hydraulic Radius	6.9 in	
Top Width	1.92 ft	
Critical Depth	14.8 in	
Percent Full	63.9 %	
Critical Slope	0.006 ft/ft	
Velocity	5.57 ft/s	
Velocity Head	0.48 ft	
Specific Energy	1.76 ft	
Froude Number	0.935	
Maximum Discharge	17.21 cfs	
Discharge Full	16.00 cfs	
Slope Full	0.003 ft/ft	
Flow Type	Subcritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise		
Normal Depth Over Rise	0.0 %	
Downstream Velocity	0.00 ft/s	
Upstream Velocity	0.00 ft/s	
Normal Depth	15.3 in	
Critical Depth	14.8 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.006 ft/ft	
Citical Slope	0.000 1910	

Project Description		
Cristian Mathad	Manning	
Friction Method	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.005 ft/ft	
Diameter	24.0 in	
Discharge	12.40 cfs	
Results		
Normal Depth	15.9 in	
Flow Area	2.2 ft <sup>2</sup>	
Wetted Perimeter	3.8 ft	
Hydraulic Radius	7.0 in	
Top Width	1.89 ft	
Critical Depth	15.2 in	
Percent Full	66.1 %	
Critical Slope	0.006 ft/ft	
Velocity	5.62 ft/s	
Velocity Head	0.49 ft	
Specific Energy	1.81 ft	
Froude Number	0.918	
Maximum Discharge	17.21 cfs	
Discharge Full	16.00 cfs	
Slope Full	0.003 ft/ft	
Flow Type	Subcritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	0.0 %	
Downstream Velocity	0.00 ft/s	
Upstream Velocity	0.00 ft/s	
Normal Depth	15.9 in	
Critical Depth	15.2 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.006 ft/ft	

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Project Description		
Friction Mother	Manning	
Friction Method	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.005 ft/ft	
Diameter	30.0 in	
Discharge	22.60 cfs	
Results		
Normal Depth	19.9 in	
Flow Area	3.5 ft <sup>2</sup>	
Wetted Perimeter	4.8 ft	
Hydraulic Radius	8.7 in	
Top Width	2.36 ft	
Critical Depth	19.4 in	
Percent Full	66.4 %	
Critical Slope	0.005 ft/ft	
Velocity	6.53 ft/s	
Velocity Head	0.66 ft	
Specific Energy	2.32 ft	
Froude Number	0.952	
Maximum Discharge	31.20 cfs	
Discharge Full	29.00 cfs	
Slope Full	0.003 ft/ft	
Flow Type	Subcritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
·	0.0 :	
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise		
Normal Depth Over Rise	33.8 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	19.9 in	
Critical Depth	19.4 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.005 ft/ft	

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Project Description		
Friction Method	Manning	
Friction Method	Formula	
Solve For	Normal Depth	
In most District		
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.005 ft/ft	
Diameter	24.0 in	
Discharge	11.80 cfs	
Results		
Normal Depth	15.3 in	
Flow Area	2.1 ft <sup>2</sup>	
Wetted Perimeter	3.7 ft	
Hydraulic Radius	6.9 in	
Top Width	1.92 ft	
Critical Depth	14.8 in	
Percent Full	63.9 %	
Critical Slope	0.006 ft/ft	
Velocity	5.57 ft/s	
Velocity Head	0.48 ft	
Specific Energy	1.76 ft	
Froude Number	0.935	
Maximum Discharge	17.21 cfs	
Discharge Full	16.00 cfs	
Slope Full	0.003 ft/ft	
Flow Type	Subcritical	
GVF Input Data		
-	0.0 in	
Downstream Depth Length	0.0 m 0.0 ft	
Number Of Steps	0.0 10	
ויעוווטכו טו אנפףא	U	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise		
Normal Depth Over Rise	33.8 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	15.3 in	
Critical Depth	14.8 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.006 ft/ft	

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Project Description		
Edding Math.	Manning	
Friction Method	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.005 ft/ft	
Diameter	24.0 in	
Discharge	15.50 cfs	
Desults		
Results		
Normal Depth	19.0 in	
Flow Area	2.7 ft <sup>2</sup>	
Wetted Perimeter	4.4 ft	
Hydraulic Radius	7.3 in	
Top Width	1.62 ft	
Critical Depth	17.0 in	
Percent Full	79.3 %	
Critical Slope	0.006 ft/ft	
Velocity	5.80 ft/s	
Velocity Head	0.52 ft	
Specific Energy	2.11 ft	
Froude Number	0.796	
Maximum Discharge	17.21 cfs	
Discharge Full	16.00 cfs	
Slope Full	0.005 ft/ft	
Flow Type	Subcritical	
711-2		
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise		
Normal Depth Over Rise	33.8 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	19.0 in	
Critical Depth	17.0 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.006 ft/ft	

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Project Description		
Eriction Mothod	Manning	
Friction Method	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.005 ft/ft	
Diameter	24.0 in	
Discharge	15.50 cfs	
Results		
Normal Depth	19.0 in	
Flow Area	2.7 ft <sup>2</sup>	
Wetted Perimeter	4.4 ft	
Hydraulic Radius	7.3 in	
Top Width	1.62 ft	
Critical Depth	17.0 in	
Percent Full	79.3 %	
Critical Slope	0.006 ft/ft	
Velocity	5.80 ft/s	
Velocity Head	0.52 ft	
Specific Energy	2.11 ft	
Froude Number	0.796	
Maximum Discharge	17.21 cfs	
Discharge Full	16.00 cfs	
Slope Full	0.005 ft/ft	
Flow Type	Subcritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	33.8 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	19.0 in	
Critical Depth	17.0 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.006 ft/ft	

		<u> </u>
Project Description		
Frietian Mathad	Manning	
Friction Method	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.005 ft/ft	
Diameter	24.0 in	
Discharge	15.50 cfs	
Results		
Normal Depth	19.0 in	
Flow Area	2.7 ft <sup>2</sup>	
Wetted Perimeter	4.4 ft	
Hydraulic Radius	7.3 in	
Top Width	1.62 ft	
Critical Depth	17.0 in	
Percent Full	79.3 %	
Critical Slope	0.006 ft/ft	
Velocity	5.80 ft/s	
Velocity Head	0.52 ft	
Specific Energy	2.11 ft	
Froude Number	0.796	
Maximum Discharge	17.21 cfs	
Discharge Full	16.00 cfs	
Slope Full	0.005 ft/ft	
Flow Type	Subcritical	
	Subciticul	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	33.8 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	19.0 in	
Critical Depth	17.0 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.006 ft/ft	

		•
Project Description		
Cristian Mathead	Manning	
Friction Method	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.005 ft/ft	
Diameter	24.0 in	
Discharge	10.60 cfs	
Results		
Normal Depth	14.3 in	
Flow Area	1.9 ft <sup>2</sup>	
Wetted Perimeter	3.5 ft	
Hydraulic Radius	6.6 in	
Top Width	1.96 ft	
Critical Depth	14.0 in	
Percent Full	59.5 %	
Critical Slope	0.005 ft/ft	
Velocity	5.44 ft/s	
Velocity Head	0.46 ft	
Specific Energy	1.65 ft	
Froude Number	0.964	
Maximum Discharge	17.21 cfs	
Discharge Full	16.00 cfs	
Slope Full	0.002 ft/ft	
Flow Type	Subcritical	
GVF Input Data		
-	0.0 in	
Downstream Depth		
Length Number Of Steps	0.0 ft 0	
пишьег Ог этеря	U	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise		
Normal Depth Over Rise	33.8 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	14.3 in	
Critical Depth	14.0 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.005 ft/ft	

Project Description		<u> </u>
•	Manning	
Friction Method	Formula	
Solve For	Normal Depth	
Input Data		
	0.012	
Roughness Coefficient	0.013	
Channel Slope	0.005 ft/ft	
Diameter	30.0 in	
Discharge	16.60 cfs	
Results		
Normal Depth	16.3 in	
Flow Area	2.7 ft <sup>2</sup>	
Wetted Perimeter	4.1 ft	
Hydraulic Radius	7.9 in	
Top Width	2.49 ft	
Critical Depth	16.5 in	
Percent Full	54.2 %	
Critical Slope	0.005 ft/ft	
Velocity	6.11 ft/s	
Velocity Head	0.58 ft	
Specific Energy	1.94 ft	
Froude Number	1.031	
Maximum Discharge	31.20 cfs	
Discharge Full	29.00 cfs	
Slope Full	0.002 ft/ft	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	54.2 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	16.3 in	
Critical Depth	16.5 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.005 ft/ft	

		<u> </u>
Project Description		
Et it Mail !	Manning	
Friction Method	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.005 ft/ft	
Diameter	18.0 in	
Discharge	6.90 cfs	
Results		
Normal Depth	13.7 in	
Flow Area	1.4 ft²	
Wetted Perimeter	3.2 ft	
Hydraulic Radius	5.4 in	
Top Width	1.28 ft	
Critical Depth	12.2 in	
Percent Full	76.2 %	
Critical Slope	0.007 ft/ft	
Velocity	4.77 ft/s	
Velocity Head	0.35 ft	
Specific Energy	1.50 ft	
Froude Number	0.791	
Maximum Discharge	7.99 cfs	
Discharge Full	7.43 cfs	
Slope Full	0.004 ft/ft Subcritical	
Flow Type	Subcritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	45.9 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	13.7 in	
Critical Depth	12.2 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.007 ft/ft	

		<u> </u>
Project Description		
Edular Malland	Manning	
Friction Method	Formula	
Solve For	Normal Depth	
Innut Data		
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.005 ft/ft	
Diameter	24.0 in	
Discharge	11.00 cfs	
Results		
Normal Depth	14.6 in	
Flow Area	2.0 ft <sup>2</sup>	
Wetted Perimeter	3.6 ft	
Hydraulic Radius	6.7 in	
Top Width	1.95 ft	
Critical Depth	14.3 in	
Percent Full	60.9 %	
Critical Slope	0.005 ft/ft	
Velocity	5.49 ft/s	
Velocity Head	0.47 ft	
Specific Energy	1.69 ft	
Froude Number	0.955	
Maximum Discharge	17.21 cfs	
Discharge Full	16.00 cfs	
Slope Full	0.002 ft/ft	
Flow Type	Subcritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	45.9 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	14.6 in	
Critical Depth	14.3 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.005 ft/ft	

		<b>-</b>
Project Description		
Friction Method	Manning	
Friction Method	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.005 ft/ft	
Diameter	24.0 in	
Discharge	14.30 cfs	
Results		
Normal Depth	17.7 in	
Flow Area	2.5 ft <sup>2</sup>	
Wetted Perimeter	4.1 ft	
Hydraulic Radius	7.2 in	
Top Width	1.76 ft	
Critical Depth	16.3 in	
Percent Full	73.8 %	
Critical Slope	0.006 ft/ft	
Velocity	5.76 ft/s	
Velocity Head	0.52 ft	
Specific Energy	1.99 ft	
Froude Number	0.854	
Maximum Discharge	17.21 cfs	
Discharge Full	16.00 cfs	
Slope Full	0.004 ft/ft	
Flow Type	Subcritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0.0 10	
·	<u> </u>	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	45.9 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	17.7 in	
Critical Depth	16.3 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.006 ft/ft	

#### **Worksheet for Pipe 10.1**

Project Description		
Friction Method	Manning	
Friction Method	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.005 ft/ft	
Diameter	24.0 in	
Discharge	14.30 cfs	
Results		
Normal Depth	17.7 in	
Flow Area	2.5 ft <sup>2</sup>	
Wetted Perimeter	4.1 ft	
Hydraulic Radius	7.2 in	
Top Width	1.76 ft	
Critical Depth	16.3 in	
Percent Full	73.8 %	
Critical Slope	0.006 ft/ft	
Velocity	5.76 ft/s	
Velocity Head	0.52 ft	
Specific Energy	1.99 ft	
Froude Number	0.854	
Maximum Discharge	17.21 cfs	
Discharge Full	16.00 cfs	
Slope Full	0.004 ft/ft	
Flow Type	Subcritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	45.9 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	17.7 in	
Critical Depth	16.3 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.006 ft/ft	

Project Description		
Friction Method	Manning	
	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.005 ft/ft	
Diameter	30.0 in	
Discharge	23.10 cfs	
Results		
Normal Depth	20.2 in	
Flow Area	3.5 ft <sup>2</sup>	
Wetted Perimeter	4.8 ft	
Hydraulic Radius	8.8 in	
Top Width	2.34 ft	
Critical Depth	19.6 in	
Percent Full	67.4 %	
Critical Slope	0.005 ft/ft	
Velocity	6.56 ft/s	
Velocity Head	0.67 ft	
Specific Energy	2.35 ft	
Froude Number	0.943	
Maximum Discharge	31.20 cfs	
Discharge Full	29.00 cfs	
Slope Full	0.003 ft/ft	
Flow Type	Subcritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	49.6 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	20.2 in	
Critical Depth	19.6 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.005 ft/ft	

		•
Project Description		
Friction Method	Manning	
Friction Metriod	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.005 ft/ft	
Diameter	42.0 in	
Discharge	33.80 cfs	
Results		
Normal Depth	20.4 in	
Flow Area	4.6 ft <sup>2</sup>	
Wetted Perimeter	5.4 ft	
Hydraulic Radius	10.3 in	
Top Width	3.50 ft	
Critical Depth	21.6 in	
Percent Full	48.5 %	
Critical Slope	0.004 ft/ft	
Velocity	7.30 ft/s	
Velocity Head	0.83 ft	
Specific Energy	2.53 ft	
Froude Number	1.119	
Maximum Discharge	76.52 cfs	
Discharge Full	71.14 cfs	
Slope Full	0.001 ft/ft	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	48.5 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	20.4 in	
Critical Depth	21.6 in	
Channel Slope	0.005 ft/ft	
Critical Slope	0.004 ft/ft	



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Rec \$0.00 Pages



21613/149

#### **RESOLUTION NO. 16-426**

## **BOARD OF COUNTY COMMISSIONERS COUNTY OF EL PASO, STATE OF COLORADO**

Resolution Denying an Appeal by Hammers Construction LLC (APP-16-002) of the Administrative Determination made by the Planning and Community Development Department Executive Director regarding the requirement for permanent/post construction Water Quality (permanent stormwater quality best management practices or BMP's).

WHEREAS, pursuant to §§30-11-101(1)(e) and 30-11-107(1)(e), C.R.S., the Board of County Commissioners of El Paso County, Colorado (hereinafter "Board) has the legislative authority to manage the concerns of El Paso County when deemed by the Board to be in the best interests of the County and its inhabitants; and

WHEREAS, after consultation with the County Attorney's Office, the Executive Director of Planning and Community Development on August 4, 2016 issued an administrative determination finding made an administrative determination that all undeveloped lots within the Claremont Business Park are subject to installation of permanent stormwater management best management practices (BMP's) associated with development, and that the terms of a 2008 approved deviation relieving the developer of the requirements have not been met.; and

WHEREAS, an appeal of the administrative determination was filed by Hammers Construction on August 10, 2016, and a hearing date was set for September 27, 2016 to hear the appeal; and

WHEREAS, the hearing was continued to a date certain of November 22, 2016; and

WHEREAS, at the Applicant's appeal hearing on November 22, 2016, testimony from the Applicant and the Applicant's representatives was heard by the Board in favor of the appeal, testimony from representatives of Planning and Community Development Department and was presented, and such testimony and associated evidence was weighed by the Board; and

Resolution No. 16- 426 Page 2

WHEREAS, the Board, having reviewed the testimony and evidence, hereby finds and determines that the requested appeal of the administrative determination by the Planning and Community Development Executive Director by the Applicant did not satisfy the criteria of approval to overturn the administrative determination.

NOW, THEREFORE, BE IT RESOLVED that the Board of County Commissioners of El Paso County, Colorado, hereby denies the appeal of the administrative determination by Hammers Construction and determines that permanent stormwater management best management practices (BMP's) are required with new development within the Claremont Business Park: and

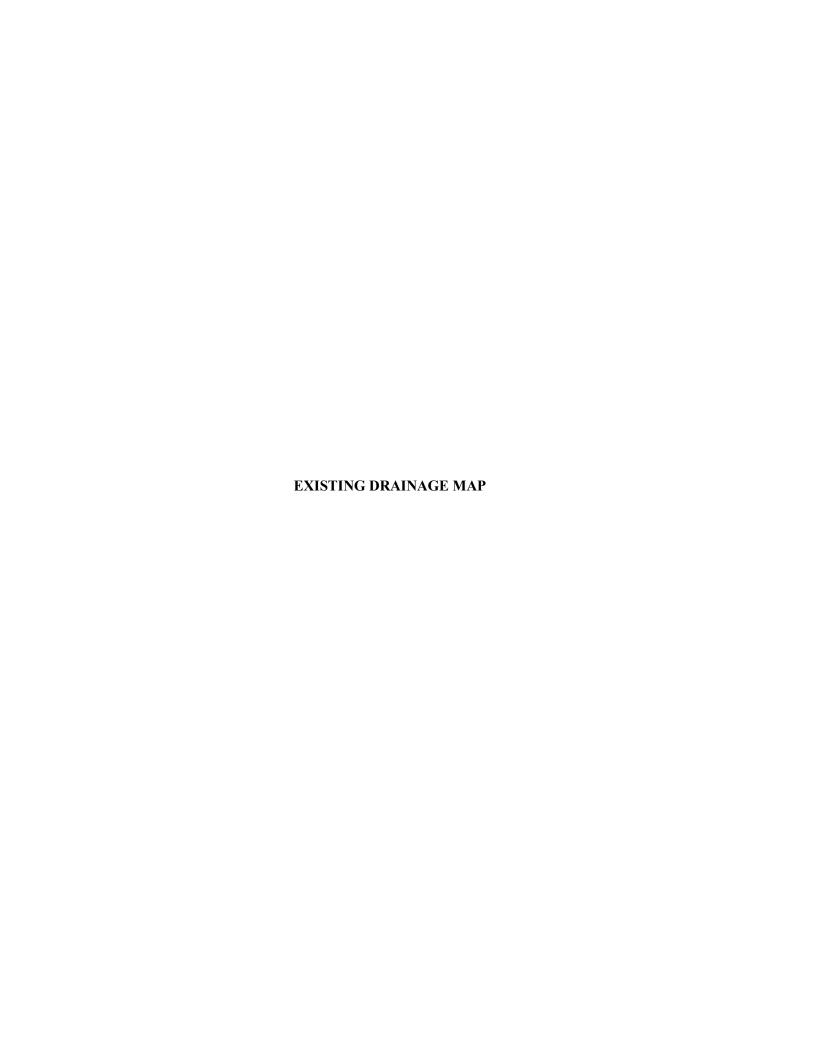
BE IT FURTHER RESOLVED that Sallie Clark, duly elected, qualified member and Chair of the Board of County Commissioners, or Darryl Glenn, duly elected, qualified member and Vice Chair of the Board of County Commissioners, be and is hereby authorized on behalf of the Board to execute any and all documents necessary to carry out the intent of the Board as described herein.

DONE THIS 22<sup>nd</sup> day of November, 2016, at Colorado Springs Colorado.

BOARD OF COUNTY COMMISSIONERS EL PASO COUNTY, COLORADO

\_ by.—€

Copply-Charte Recorder





#### FINAL DRAINAGE REPORT

#### For

"Claremont Business Park Filing No. 2"

# Prepared for: El Paso County Department of Public Works Engineering Division

On Behalf of: Claremont Development, Inc.

Prepared by:



2435 Research Parkway, Suite 300 Colorado Springs, CO 80920 (719) 575-0100 fax (719) 572-0208

Revised November 2006

05.151.006

#### **Engineer's Statement:**

The revisions (changes made to the base Final Drainage Report since July, 2006) to the attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. The revisions encompassed adding additional right of way to the study area at the County's request, the handling of offsite drainage due to the additional right of way, a breakdown of private drainage within lot numbers 10 through 25 of Filing No. 2 due to cross-lot drainage (contrary to note # 25 on the recorded plat), profiling additional inlets along the channel edge, and rip-rap sizing for outlet structures along the channel. The Final Drainage Report dated July, 2006 was prepared under the direct supervision of Richard G. Gallegos, Jr. in July, 2006 and stamped (see next sheet).

The Final Drainage Report was prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing the *revisions* to this report.

**SEAL** 

Brady A. Shyrock Registered Professional Engineer State of Colorado No. 38164



#### **Engineer's Statement:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Richard G. Gallegos, Jr.
Registered Professional Engineer
State of Colorado
No. 36247

SEAL TO REAL AGAIL FOR STANDING AGAIL FOR STANDING

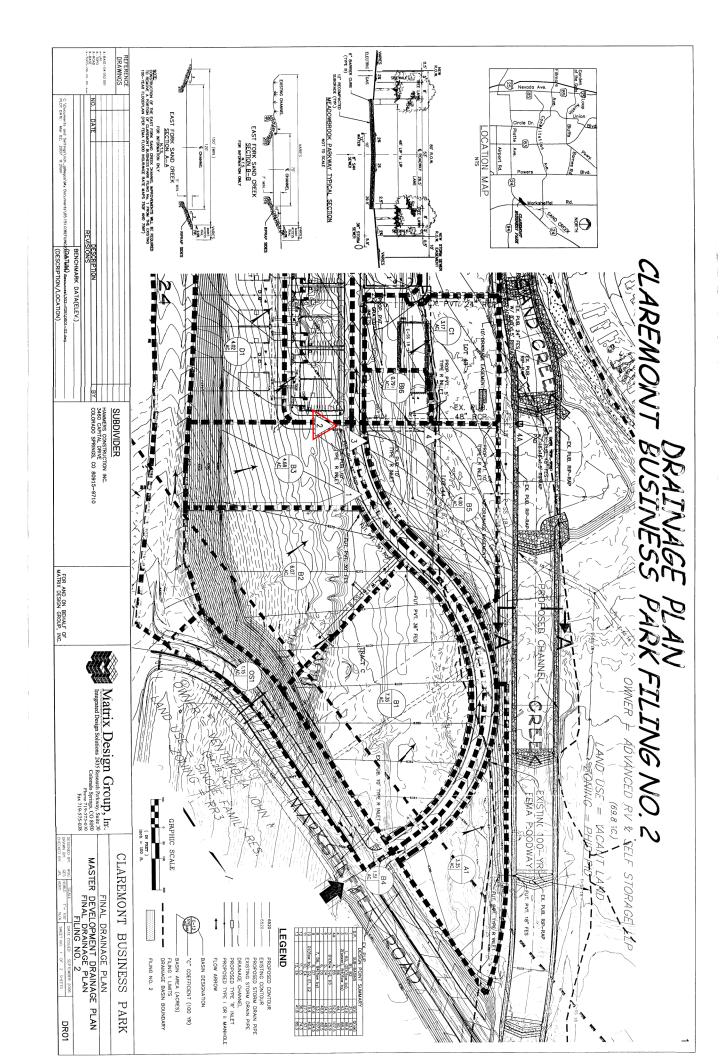
#### **Developer's Statement:**

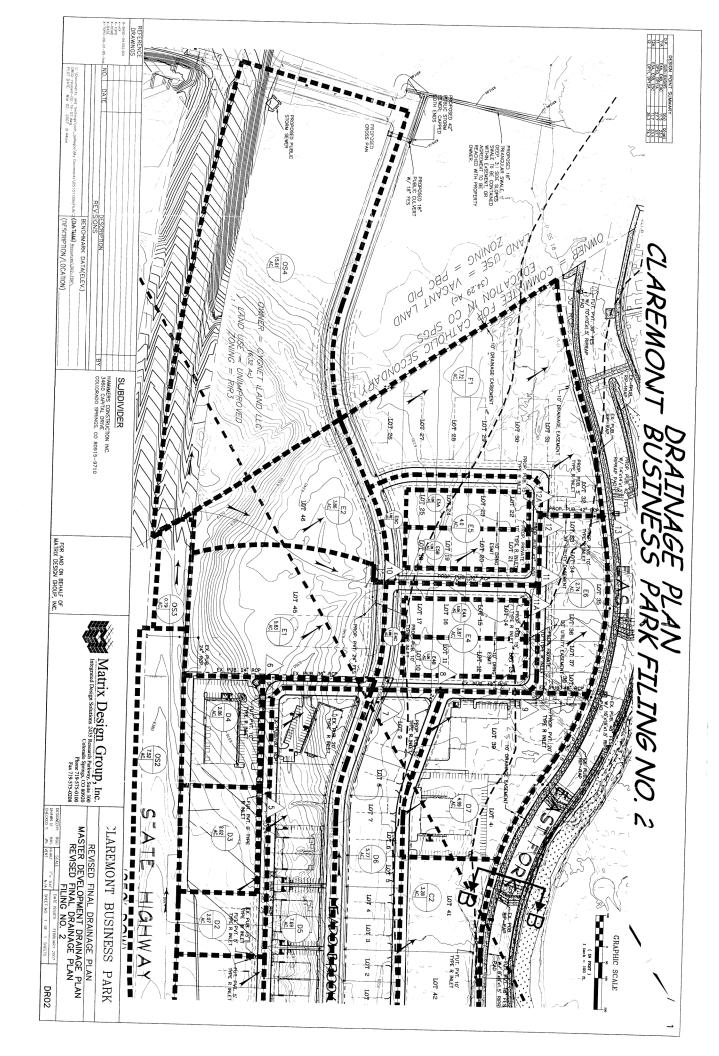
I, the developer have read and	will comply with all of the requirements specified in this drainage
report and plan.	/
Claremont Development, Inc	· . /
Business Name	
	$\mathcal{G}_{\mathcal{A}}$
By:	
Title:	- Jun
Address: 3460 Capital Drive	· · · · · · · · · · · · · · · · · · ·
Colorado Springs, C	O 80915

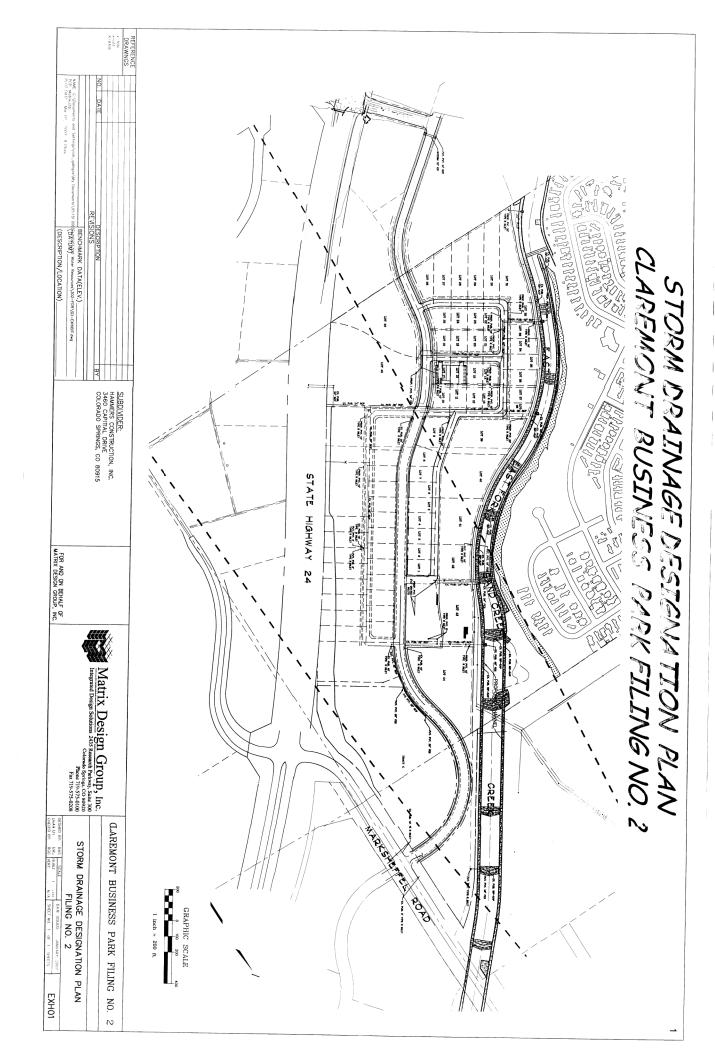
#### El Paso County:

Filed In accordance with Section 51.1 of the El I	Paso Land Development Code, as amended.
Lang Hamachen	4/23/01
Mr. John McCarty, County Engineer/Director	Date /

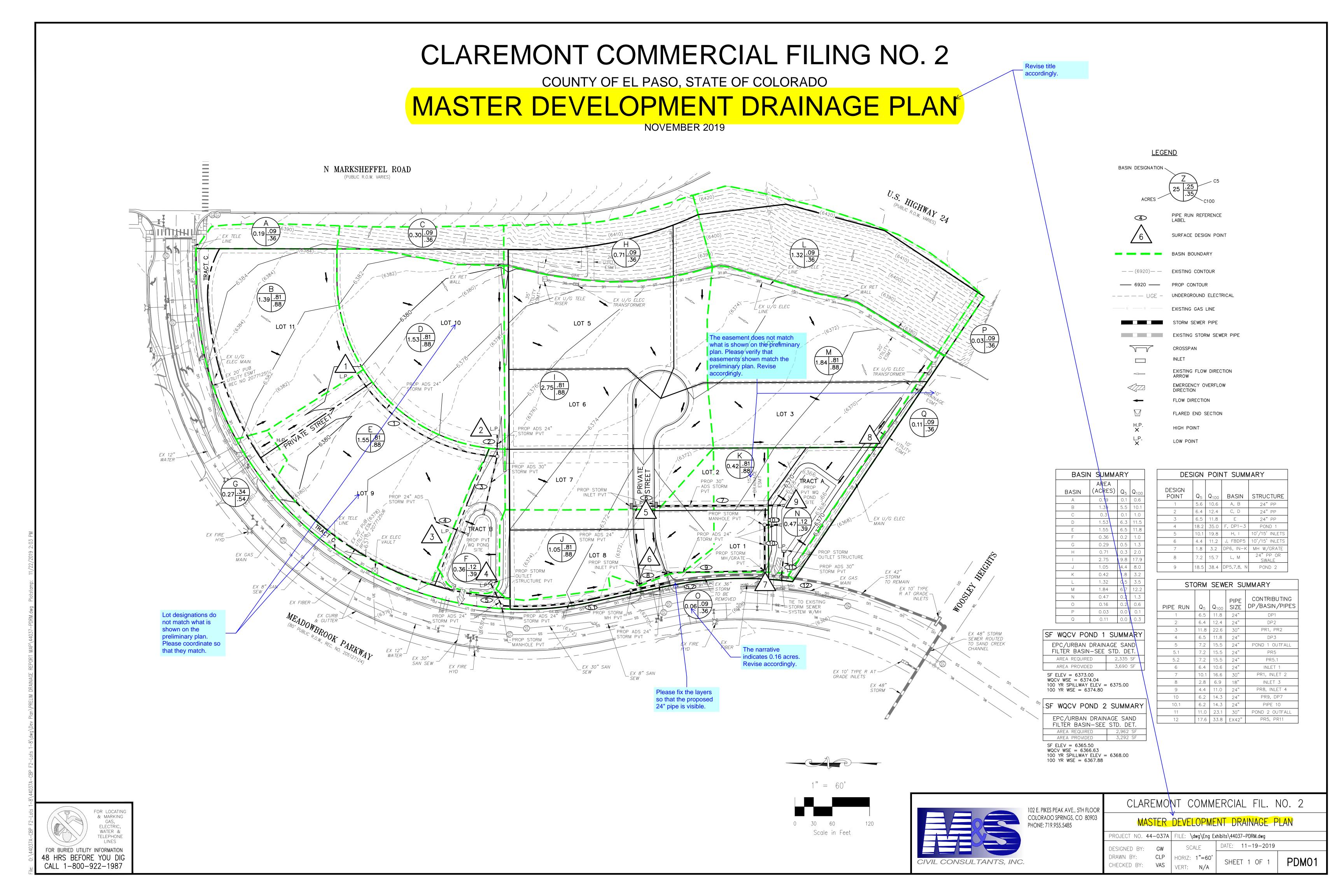
Conditions:











### Prelim Drainage Report\_v1\_redlines.pdf Markup Summary

#### Callout (41)



Subject: Callout Page Label: 10 Author: Daniel Torres Date: 1/13/2020 1:08:29 PM

Status: Color: Layer: Space: the drainage fees section of the Matrix report was not included. Please include in the appendix.

ta design professionals
ove is only an estimate
Please state that
drainage fees were
previously paid for
this property.
ed into sixteen
at Busiyes Park Filing
es are required. In the

Subject: Callout Page Label: 10

Author: Daniel Torres Date: 1/13/2020 1:17:48 PM

Status: Color: Layer: Space: Please state that drainage fees were previously paid for this property.

Revise the 16th to Preliminary
Drantege Report.

MASTER DEVELOPMENT
FOR
CLAPEMONT COL

Subject: Callout Page Label: 1

Author: Daniel Torres Date: 1/13/2020 1:28:32 PM

Status: Color: Layer: Space: Revise the title to Preliminary Drainage Report.



Subject: Callout Page Label: 18

Author: Daniel Torres

Date: 1/13/2020 10:27:32 AM

Status: Color: Layer: Space: Please fix the title.



Subject: Callout Page Label: 20 Author: Daniel Torres Date: 1/13/2020 10:30:20 AM

Status: Color: Layer: Space: Please update the title



Subject: Callout Page Label: 27 Author: Daniel Torres

**Date:** 1/13/2020 10:53:58 AM

Status: Color: Layer: Space: Please use the latest UD detention worksheet by Urban Drainage. Note that the hydraulics and pond design will be reviewed with the final drainage report.



Subject: Callout Page Label: 65 Author: Daniel Torres Date: 1/13/2020 10:56:02 AM

Status: Color: Layer: Space: Please fix the layers so that the proposed 24" pipe is visible.

Pir DOM at 8, larger of overlead fixes in rate (SSR) for unbear land uses. Reviews accordingly.

Subject: Callout Page Label: 21 Author: Daniel Torres Date: 1/13/2020 11:44:13 AM

Status: Color: Layer: Space: Per DCM ch 6, length of overland flow is max 100 ft. for urban land uses. Revise accordingly.

also includes lot 8

Basin J, 1.05 acres, consists of portions of Lots 1, 2 and 7 located along the western edge of the proposed site. Runcach peak runoff rates of (52-44. 45 and q0)lou-8.0 efs.

Page Label: 8 Author: Daniel Torres Date: 1/13/2020 12:30:

Subject: Callout

Date: 1/13/2020 12:30:58 PM

Status: Color: Layer: Space: also includes lot 8

This design point should also socials from the following point disage; point 6.

Subject: Callout Page Label: 22 Author: Daniel Torres Date: 1/13/2020 12:33:15 PM

Status: Color: Layer: Space: This design point should also include flow from design point 6.

Subject: Callout Page Label: 23 Author: Daniel Torres Date: 1/13/2020 12:35:23 PM

Status: Color: Layer: Space: pipe run 6



Subject: Callout Page Label: 23 Author: Daniel Torres Date: 1/13/2020 12:38:31 PM

Status: Color: Layer: Space: existing 42" pipe?



Subject: Callout Page Label: 26 Author: Daniel Torres Date: 1/13/2020 12:40:56 PM

Status: Color: \_\_\_

Color: Layer: Space:

Revise title



Subject: Callout Page Label: 26 Author: Daniel Torres Date: 1/13/2020 12:41:49 PM

Status: Color: Layer: Space: Revise the title to match the other calculation sheets which indicate Claremont Commercial.....



Subject: Callout Page Label: 34 Author: Daniel Torres Date: 1/13/2020 12:49:11 PM

Status: Color: Layer: Space: based on the soils map provided, the soil group for this pond should be "A"

arged convisiteam via an existing 4.c. rect. sorm set

7 acres, consists of a landscaping strip running al
small section of pavement associated with site acce
sists primarily of trees, bushes/grasses, and decorBasin Q of Q\$=0.5 cfs and Q100+1.3 cfs will to

Should this be G?

acres, consists of steen slones of up to 33% adiace.

and decorr s cfs will tr

a 33% adjace a soil retenti alculated to r be conveyed

Subject: Callout Page Label: 7

**Author:** Daniel Torres **Date:** 1/13/2020 8:29:26 AM

Status: Color: Layer: Space: Should this be G?



Subject: Callout Page Label: 7

Author: Daniel Torres Date: 1/13/2020 8:34:23 AM

Status: Color: Layer: Space: Pipe 7 is indicated as 30" on the drainage plan. Revise accordingly.



Subject: Callout Page Label: 65 Author: Daniel Torres Date: 1/13/2020 9:21:21 AM

Status: Color: Layer: Space: The easement does not match what is shown on the preliminary plan. Please verify that easements shown match the preliminary plan. Revise

accordingly.



Subject: Callout Page Label: 65 Author: Daniel Torres Date: 1/13/2020 9:46:49 AM

Status: Color: Layer: Space: The narrative indicates 0.16 acres. Revise accordingly.

County Drainage Criteria Manual - Volume As previously discussed water quality for th

As previously discussed water quality for the Pond 1 is designed to treat runoff from approstorage, while Pond 2 will runoff from approstorage, will reat runoff.

Flows tributary to the two SFBs are released

Flows tributary to the two SFBs are released located along Meadowbrook Parkway. The w the property owner. Access shall be granted of the private WQCV facility. A private mai drainage report(s) submittal(s) which constru

Subject: Callout Page Label: 9

**Author:** Daniel Torres **Date:** 1/13/2020 9:59:01 AM

Status: Color: Layer: Space: will treat runoff

Subject: Callout Page Label: 2

Author: Daniel Torres Date: 1/14/2020 7:28:44 AM

Status: Color: Layer: Space: Please revise title, typical.

The two relatives in the property of the SI (SI) o

Subject: Callout Page Label: 8

Author: Daniel Torres Date: 1/14/2020 7:35:02 AM

Status: Color: Layer: Space: The flow should be greater in pipes 10 and 10.1 as flow from pipe 9 should also be included as stated in course parential. Parise passed in the course parential properties are provided by the course parential provided by the course parent provided by the course parent provided by the course parent parent provided by the course parent provided by the course parent provided by the course parent parent provided by the course par

in your narrative. Revise accordingly.



**Subject:** Callout **Page Label:** 9

**Author:** Daniel Torres **Date:** 1/14/2020 7:35:27 AM

Status: Color: Layer: Space: Per County criteria water quality must be provided for 100% of the site. ECM section I.7.1.C.1 indicates that 20% of site, not to exceed 1 acre may be excluded. Provide discussion regarding the proposed basins that will not be treated and ensure that the total will not exceed 1 acre.



Subject: Callout Page Label: 29 Author: Daniel T

Author: Daniel Torres Date: 1/14/2020 7:49:33 AM

Status: Color: Layer: Space: \*Provide note indicating that per resolution 16-426 of the BoCC, on-site WQCV is required but on-site stormwater detention is not required per the FDR for Claremont Business Park Fil. 2. This has been requested on previous projects you've done in this area.



Subject: Callout Page Label: 36 Author: Daniel Torres Date: 1/14/2020 7:49:49 AM

Status: Color: Layer: Space: \*Provide note indicating that per resolution 16-426 of the BoCC, on-site WQCV is required but on-site stormwater detention is not required per the FDR for Claremont Business Park Fil. 2. This has been requested on previous projects you've done in this



Subject: Callout Page Label: 65 Author: Daniel Torres Date: 1/14/2020 7:50:14 AM

Status: Color: Layer: Space: Revise title accordingly.

Comments are the first from the comments of the first first

Subject: Callout Page Label: 5 Author: Daniel Torres Date: 1/8/2020 1:10:08 PM

Status: Color: Layer: Space: The previous page indicates 2 sand filter basins. Please revise.

NFILING NO. 2
OF Previous report was approved in December of 2018
2 Plan for Claremont Conference in approved Preliminary Drainage histon of Tract Joff Claremont proposed in Mutto de 2018. The 1 putterns and to ensure that post

Subject: Callout Page Label: 4

Author: Daniel Torres Date: 1/8/2020 1:15:07 PM

Status: Color: Layer: Space: Previous report was approved in December of

of pile, a marrie website me, making and conting to singue the possible arms do not be presented as the pile of th

Subject: Callout Page Label: 6

Author: Daniel Torres Date: 1/8/2020 1:16:27 PM

Status: Color: Layer: Space: Please revise your label of the previously approved drainage report as it is not an MDDP. It is a Final Drainage Report.

of Filing No. 2 sits proposes a Small Filine Water Quality Facility believe flows on Filine Water Small In the Small Sma Subject: Callout Page Label: 5

Author: Daniel Torres
Date: 1/8/2020 1:31:55 PM

Status: Color: Layer: Space: preliminary GEC has been provided. Final GEC plan will be provided with the final plat. Please revise.

Subject: Callout Page Label: 5 Author: Daniel Torres Date: 1/8/2020 1:32:40 PM

Status: Color: Layer: Space:

Please revise your label of the previously approved drainage report as it is not an MDDP. It is a Final Drainage Report.

Subject: Callout Page Label: 5 Author: Daniel Torres Date: 1/8/2020 1:34:28 PM

Status: Color: Layer: Space:

The drainage plan and recently approved drainage report for adjacent property indicate a 42" RCP along Meadowbrook Pwky. Please revise accordingly.

Subject: Callout Page Label: 6

Author: Daniel Torres Date: 1/8/2020 1:37:29 PM

Status: Color: Layer: Space:

revise sentence accordingly.

RCIAL NO. 2 ACT OF Subject: Callout Page Label: 1

Author: Daniel Torres Date: 1/8/2020 12:39:30 PM

Status: Color: Layer: Space:

Tract C

Subject: Callout Page Label: 1

Subject: Callout

Page Label: 6 Author: Daniel Torres Date: 1/8/2020 4:58:22 PM

**Author:** Daniel Torres Date: 1/8/2020 12:40:27 PM

Status: Color: Layer: Space:

SP197

Status: Color: Layer: Space:

Please indicate who owns the private storm sewer.



Subject: Callout Page Label: 65 Author: Daniel Torres Date: 1/9/2020 3:05:05 PM

Status: Color: Layer: Space: Lot designations do not match what is shown on the preliminary plan. Please coordinate so that they match.

The description of the distinguishment of the

Subject: Callout Page Label: 7 Author: Daniel Torres Date: 1/9/2020 3:09:18 PM

Status: Color: Layer: Space: The acreage shown on the drainage plan does not match the narrative. Revise so that they match.

And the second of the second o

Subject: Callout Page Label: 7

Author: Daniel Torres Date: 1/9/2020 3:28:17 PM

Status: Color: Layer: Space: Include in your narrative a discussion regarding the swale shown between basin D and basin I.

And the second s

Subject: Callout Page Label: 6

Author: Daniel Torres Date: 1/9/2020 7:35:02 AM

Status: Color: Layer: Space: Please include discussion regarding existing pipes/stub outs on the property indicated in the previously approved drainage reports by Matrix and why they were not used.

The fit disruptions do not really held in Norma on the control of the Norma of the Companions provided in the control of the Norma of

Subject: Callout Page Label: 7 Author: Daniel Torres

**Date:** 1/9/2020 8:35:00 AM **Status:** 

Status: Color: Layer: Space: The lot designations do not match what is shown on the preliminary plan please revise so that they match.

Highlight (24)

Subject: Highlight

Page Label: 20
MDDP Cl Author: Daniel Torres

PRO Date: 1/13/2020 10:30:26 AM

Status: Color: Layer: Space: **MDDP** 

Subject: Highlight **MDDP** Page Label: 21 MDDP Cl Author: Daniel Torres Date: 1/13/2020 10:33:04 AM Status: Color: Layer: Space: Subject: Highlight **MDDP** Page Label: 22 MDDP Cl Author: Daniel Torres PRO Date: 1/13/2020 10:33:11 AM Status: Color: Layer: Space: Subject: Highlight **MDDP** Page Label: 23 MDDP C1 Author: Daniel Torres PRO Date: 1/13/2020 10:33:16 AM Status: Color: Layer: Space: Subject: Highlight MASTER DEVELOPMENT DRAINAGE PLAN Page Label: 26 **Author:** Daniel Torres Date: 1/13/2020 10:33:30 AM Status: Color: Layer: Space: INLET 1 Subject: Highlight Page Label: 23 PIPE 1, INL **Author:** Daniel Torres Date: 1/13/2020 12:35:37 PM INLET 3 Status: Color: Layer: Space: cussed water quality Subject: Highlight will runoff d to treat runoff from Page Label: 9 nd 2 will runoff from Author: Daniel Torres Date: 1/13/2020 9:54:01 AM Status: Color: Layer: Space:

Subject: Highlight MASTER DEVELOPMENT DRAINAGE PLAN Page Label: 2 **Author:** Daniel Torres Date: 1/14/2020 7:28:26 AM Status: Color: Layer: Space: Subject: Highlight "MDDP Park Filing No Page Label: 5 as "MDDP") h Author: Daniel Torres directly into th Date: 1/8/2020 1:08:38 PM Status: Cand Eiltan I Color: Layer: Space: Subject: Highlight a Sand Filter Water Quality Facility Page Label: 5 Author: Daniel Torres Date: 1/8/2020 1:10:18 PM Status: Color: Layer: Space: Subject: Highlight "MDDP usiness Park Fi Page Label: 6 as "MDDP"). **Author:** Daniel Torres utary area of S<sub>1</sub> Date: 1/8/2020 1:13:52 PM Status: heads Darlesson Color: Layer: Space: Subject: Highlight ling No. 2", da Page Label: 6 **MDDP** The MDDP cal Author: Daniel Torres ıb-basins B1, B Date: 1/8/2020 1:13:55 PM wanta anadina Status: Color: Layer: Space: Subject: Highlight **MDDP** would produc Page Label: 6 The MDDP illu Author: Daniel Torres Parkway. As sta **Date:** 1/8/2020 1:14:00 PM Status: ---1--4: --- 1 C A' Color: Layer: Space:

murauve runon Subject: Highlight e MDDP ed that the water Page Label: 6 n the MDDP, ov Author: Daniel Torres the BoCC, on-s: Date: 1/8/2020 1:14:04 PM aremont Rusines Status: Color: Layer: Space: Subject: Highlight MASTER DEVELOPMENT DRAINAGE PLAN Page Label: 65 **Author:** Daniel Torres Date: 1/8/2020 1:29:51 PM Status: Color: Layer: Space: Subject: Highlight Page Label: 65 Author: Daniel Torres Date: 1/8/2020 1:30:10 PM Status: Color: Layer: Space: Subject: Highlight Page Label: 5
Author: Daniel Torres Date: 1/8/2020 1:34:39 PM at ctrincti Status: Color: Layer: Space: Subject: Highlight 0 Page Label: 5 Author: Daniel Torres Date: 1/8/2020 1:34:40 PM ctructin Status: Color: Layer: Space: propose: Subject: Highlight 40" Page Label: 5 te 40"/48 Author: Daniel Torres Date: 1/8/2020 1:34:45 PM o drain the Status: Color: Layer: Space:

Subject: Highlight n using across dustrial, asphalt, curb, tv Page Label: 6 drain using across asph thwest to proposed priva Author: Daniel Torres Date: 1/8/2020 1:37:13 PM ures of the proposed wa Status: Color: Layer: Space: Subject: Highlight MASTER DEVELOPMENT DRAINAGE PLAN Page Label: 3 Author: Daniel Torres Date: 1/8/2020 12:41:10 PM Status: Color: Layer: Space: Subject: Highlight MASTER DEVELOPMENT DRAINAGE PLAN Page Label: 4 Author: Daniel Torres Date: 1/8/2020 12:41:26 PM Status: Color: Layer: Space: Subject: Highlight t 10 Page Label: 7 Lot 10 alo Author: Daniel Torres Date: 1/9/2020 10:57:59 AM reach pea Status: Color: Layer: Space: Subject: Highlight 9 Page Label: 7
Author: Daniel Torres Date: 1/9/2020 10:58:01 AM adowhre Status: Color: Layer: Space: Text Box (2) ORGO: BERT, 4919 Solen Guerrasi Salesta resigning Subject: Text Box Please provide a legible FIRM Map



Page Label: 18 **Author:** Daniel Torres Date: 1/13/2020 10:30:54 AM

Status: Color: Layer: Space:

The content of the co

Subject: Text Box Page Label: 6 Author: Daniel Torres

**Date:** 1/14/2020 7:29:49 AM

Status: Color: Layer: Space: Please also include in your narrative how your proposed flows entering the existing storm system compare to the previously approved drainage report from Matrix. State whether or not the existing facilities are adequate. Please take into account the recently approved drainage report from the lot to the south (PCD file no. PPR192) that will also tie into this existing system.