

For

## **MAYBERRY, COLORADO SPRINGS**

**PREPARED FOR:** 

COLORADO SPRINGS MAYBERRY, LLC 3296 DEVINE HEIGHTS #208 COLORADO SPRINGS, CO 80922

**PREPARED BY:** 

R & R ENGINEERS - SURVEYORS, INC. 1635 W. 13<sup>TH</sup> AVE, SUITE 310 DENVER, CO 80204 CONTACT: CLIF DAYTON, P.E. (303) 753-6730

SKP236

EPC number added accordingly.

R&R JOB #MC22208 EPC PROJECT NO. XXX

**ORIGINAL SUBMITTAL: JULY 2023** 

## **ENGINEER'S STATEMENT:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for liability caused by negligent acts, errors, or omissions on my part in preparing this report.

SIGNATURE: \_\_\_\_

Clif Dayton, P.E. Registered Professional Engineer State of Colorado No. 51674

## **DEVELOPER'S STATEMENT:**

I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan.

SIGNATURE: \_\_\_\_\_

John Mick Colorado Springs Mayberry, LLC 3296 Devine Heights #208 Colorado Springs, CO 80922

## **EL PASO COUNTY'S STATEMENT:**

Filed in accordance with the requirements of the El Paso County Land Development Code, Drainage Criteria Manual, Volumes 1 and 2, and Engineering Criteria Manual as amended.

SIGNATURE:

Joshua Palmer, P.E. County Engineer/ECM Administrator

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## I. GENERAL LOCATION AND DESCRIPTION

## A. Background

Mayberry, Colorado Springs (formerly known as "Ellicott Town Center") is a proposed subdivision located west of Ellicott, Colorado in El Paso County. The development is located on the south side of State Highway 94, approximately 1-1/2 miles west of Ellicott Highway, as shown in Figure 1.



There is an existing Master Development Drainage Plan (MDDP) for Ellicott Town Center that was approved in December of 2005. This new MDDP will supersede the previous report and is being prepared as part of the Sketch Plan submittal.

## B. Scope

This report has been prepared in support of the Sketch Plan application for Mayberry, Colorado Springs. The report is intended to fulfill the El Paso County requirements for an MDDP.

The report will provide a summary of site drainage issues impacting the proposed development, including analysis of impacts from upstream drainage patterns, site-specific developed drainage patterns, and impacts on downstream facilities. This drainage report was prepared based on the guidelines and criteria presented in the El Paso County Drainage Criteria Manual.

## C. Site Location and Description

The Mayberry, Colorado Springs development (hereon called the site) is approximately 632 acres (of which 80 acres is within parcel 3400000232 and is not yet owned by the developer) and comprises the northern half and southwest quadrant of Section 14 along with the eastern quarter of Section 15. More specifically, the site lies within portions of Sections 14 and 15, Township 14 South, Range 63 West of the 6<sup>th</sup> Principal Meridian. The site is located at an elevation of approximately 6,060 feet.

State Highway 94 borders the Site to the north and unplatted agricultural properties border the Site on the west, south, and east sides. Properties to the west and southwest are zoned RR-5 and properties to the east/southeast are zoned A-35. Log Road borders the northeastern portion of the site to the east.

The master plan proposes single-family lots, multifamily development, commercial/mixed-use development, parks and open space, and an elementary school.

The primary access to the Site will be provided by newly constructed roads off Highway 94 and Log Road. The new roads, Springs Road and New Log Road, will run through the site from north to south. Additionally, a new road will be constructed to run east west and will be an extension of the existing Handle Road located to the east of the Site.

The intermittent streams throughout this area drain into the Black Squirrel Creek Basin which ultimately outfalls into the Arkansas River. A majority of the site is located within the Ellicott Consolidated Drainage Basin (CHBS1200). This basin conveys surface drainage to the West Fork of Black Squirrel Creek, which is located east of this parcel between the site and Ellicott Highway. The Southwest Corner of the site is located within the Telephone Exchange Drainage Basin (CHW0200)

The terrain is generally flat with gentle northwest to southeast slopes ranging from one to two percent. Historic drainage patterns from the site are conveyed overland to the south and east boundaries of the site. Construction of roadways and single-family homes has begun within Filing 1, Filing 2, and Filing 3 while the remainder of the site is covered with native grasses. For the purpose of this MDDP, Filings 4 and 5 are assumed to be existing as these projects are currently under review.

### **D.** General Soil Conditions

According to the Soil Survey of El Paso County prepared by the Soil Conservation Service, on-site soils are comprised primarily of "Blakeland Loamy Sand (type 8)" soils

and "Truckton Loamy Sand (map symbol 95) (see Appendix). The onsite soils are characterized as well-drained sandy soils with low runoff rates and low erosion potential. These soils are classified as hydrologic soils group "A" for drainage analysis purposes.

### E. References

David R. Sellon & Associates Inc., "Antelope Park Ranchettes Interior Drainage Plan," March, 1972.

El Paso County "Drainage Criteria Manual County of El Paso, Colorado – Volumes 1 and 2" dated October 31, 2018. (Referred to throughout as EPC DCM)

El Paso County Planning Department, "Ellicott Valley Comprehensive Plan," March, 1989.

El Paso County "Engineering Criteria Manual," January 9, 2006.

El Paso County Resolution No. 15-042 (El Paso County adoption of "Chapter 6: Hydrology" and "Chapter 13, Section 3.2.1: Full Spectrum Detention" of the City of Colorado Springs Drainage Criteria Manual dated May 2014).

JPS Engineering, "Master Development Drainage Plan for Ellicott Town Center," November 22, 2005 (approved by El Paso County 12/02/05).

JPS Engineering, "Master Development Drainage Plan and Preliminary Drainage Report for Springs East Village," March 21, 2002 (approved by El Paso County 10/23/02).

JPS Engineering, "Master Development Drainage Plan and Preliminary Drainage Report for Viewpoint Village," January 28, 2002 (approved by El Paso County 9/11/02).

JPS Engineering, "Preliminary Drainage Report for Ellicott Town Center - Phase 1," January 15, 2007.

JPS Engineering, "Preliminary Drainage Report Amendment for Mayberry, Colorado Springs – Phase 1 PUD," revised February 2022

JPS Engineering, "Final Drainage Report for Mayberry, Colorado Springs – Filing No. 1A Replat," approved June 2022.

Leigh Whitehead & Associates, Inc., "Master Development Drainage Plan for Sunset Village," May, 2000 (approved by El Paso County 8/31/00).

Pacific Summits Engineering, "Final Drainage Report for Viewpoint Estates," January 6, 1998 (approved by El Paso County 10/6/99).

United Planning and Engineering, "Preliminary Drainage Plan & Report for Springs East," November 19, 1999.

United Planning and Engineering, "Drainage Plan & Report for Viewpoint Subdivision," May, 2000.

USDA/NRCS, "Soil Survey of El Paso County Area, Colorado," June, 1981.

Federal Emergency Management Agency, Map Number 08041C0810G, Panel 810 of 1300, December 7, 2018

R&R Engineers-Surveyors, "Final Drainage Report for Mayberry, Colorado Springs – Filing No. 3," Approved May 2023

## II. DRAINAGE BASINS AND SUB-BASINS

## A. Major Drainage Basins

It looks like a portion of the project is within Telephone Exchange Drainage Basin. Discuss both basin and address any transfer of flows

The Telephone Exchange Drainage Basin is now discussed in this section as being part of the overall master drainage study boundary.

The proposed development lies primarily within the Ellicott Consolidated Drainage Basin (CHBS1200) as classified by El Paso County. This basin is comprised of the area tributary to the West Fork of Black Squirrel Creek, with the majority of the basin bounded by SH94 to the north and Ellicott Highway to the east. No drainage planning study has been completed for the Ellicott Consolidated Drainage Basin or any adjacent

 inage basins. El Paso County approved the "Sunset Village Master Development inage Plan (MDDP)" prepared by Leigh Whitehead & Associates. This MDDP covers adjacent Telephone Exchange Drainage Basin, which borders the Mayberry parcel the west. Based on the Drainage Report for Viewpoint Estates, stormwater ention ponds were constructed to maintain historic flows leaving the upstream reloped areas. As such, the drainage analysis for major basins impacting the site assume that historic flows enter this parcel from upstream.

major drainage basins lying in and around the proposed development are depicted in the appendix. Mayberry, Colorado Springs is located primarily within the Ellicott Consolidated Drainage Basin, which comprises a tributary area of about 13 square miles, or 8,320 acres. The proposed subdivision represents a total of approximately 632 acres of development, or 7 percent of the total basin area. An "onsite" drainage planning approach has been proposed based on the relatively small developed area in comparison to the remaining undeveloped basin area, which is primarily agricultural land.

The existing site topography has several off-site drainage basins that enter the north and west boundaries of the Mayberry parcel. Triple 30-inch CMP culverts cross SH94

at several locations along the north boundary of the site. These off-site basins combine with on-site flows, following existing grass-lined swales southeasterly through the site. The site historically consists of six major basins conveying flows towards the south and eastern boundaries of the site, as shown in Figure DR1 in Appendix D.

## **B.** Floodplain Impacts

Mayberry, Colorado Springs is located approximately one mile southwest of the 100year floodplain limits for the West Fork of Black Squirrel Creek, as delineated by the Federal Emergency Management Agency (FEMA). The floodplain limits in the vicinity of the site are shown in Flood Insurance Rate Map (FIRM) Number 08041C0810G, dated December 7, 2018 (see Appendix A).

## C. Sub-Basin Description

The developed drainage basins lying within the site are depicted on the proposed drainage maps in Appendix D. The interior site layout has been delineated into several major drainage basins (A, B, D, E, F, and G) based on the anticipated proposed interior road layout and grading scheme. The natural drainage patterns were held to decrease the impact on downstream properties. Each of these sub-basins drain towards the southeast and sheet-flow onto neighboring properties to the east and south.

## III. DRAINAGE CRITERIA

## A. Hydrologic Criteria

Rational method procedures were utilized for calculations of peak flows within the existing and proposed on-site drainage basins. Rational method hydrologic calculations were based on the following assumptions:

•	Design storm (minor)	5-year	
•	Design storm (major)	100-year	
•	Rainfall Intensities	El Paso Count	y I-D-F Curve
•	Hydrologic soil type	А	
		C5	C100
•	Runoff Coefficients - undeveloped:		
	Existing pasture/meadow areas	0.04	0.35
•	Runoff Coefficients - developed:		
	Proposed Residential (1/8-1/4 acre lots)	0.375	0.545
	Proposed Neighborhood Commercial	0.81	0.88
	Proposed Multi-Family	0.81	0.88

Composite runoff coefficients for the developed residential areas have been calculated based on average lot sizes between 1/8-acre and 1/4-acre. A rational method spreadsheet was utilized for modeling these flows and can be found in Appendix B.

Two offsite drainage basins to the north of State Highway 94 will be routed through the development as intended in the Mayberry Filing No. 1 Final Drainage Report (FDR) and the Mayberry Filing No. 3 Final Drainage Report. The SCS method was used for both offsite basins, EC10 and EC11, to identify the peak flows within the referenced FDRs. Please refer to Appendix E for supporting calculations.

## B. Detention and Water Quality Criteria

This MDDP anticipates six full spectrum extended detention basins (EDB) to accommodate the entire master development. Basin volumes have been calculated using the Mile High Flood District (MHFD) spreadsheet and incorporated into the preliminary overlot grading surface to ensure a minimum 3% pond bottom can be satisfied and to identify pond outfall locations. The MHFD worksheets can be found in Appendix C. It is the responsibility of the individual Final Drainage Reports for future Mayberry filings to design an outlet structure which accommodate required release rates. The future facilities shall be designed to pass and release the water quality capture volume (WQCV), excess urban runoff volume (EURV), and the 100-year storm to meet all local and state regulations by means of a multi-stage outlet structure.

## IV. DRAINAGE DESIGN

## A. General Concept

The drainage design intent is to maintain existing drainage patterns while protecting downstream properties and infrastructure from this development. This master drainage plan delineates six drainage basins, therefore six full spectrum extended detention basins are proposed. Open channels and future storm infrastructure are anticipated to route stormwater to the EDBs. For the purpose of this overview approach, only major roadways have been detail graded into the proposed overlot surface to demonstrate how these drainage basin divides will be accomplished.

As there is no existing stormwater infrastructure to the south and east of this development, the ultimate stormwater discharge from the proposed EDBs will first enter a plunge pool before exiting the site. The recommended plunge pools will decrease the velocity and act as a level spreader to convert point discharges to a sheet-flow condition leaving the site.

Three offsite basins will impact this master development. Basin EC12 combining with

This offsite flow (EC12 and OFF-1) will now be channelized. Erosion and downstream impacts should be addressed.

Please identify where this flow will be directed if prevented from entering the site as done in historic conditions. MAYBERR Provide design points and flows of the offsite basins MASTER DEVELO entering the development.

The narrative and drainage map has been enhanced to discuss recommended BMPs to avoid erosion and downstream impacts.

storically flows in and has been recommende

The narrative and drainage age pattern destination map has been enhanced to discuss the flow patterns and ugh culverts under SH ultimate discharge point.

maintain the ent, a height Basin EC11 is erry Filing No. ues this offsite flow south through an RCP pipe under Achison Way.<sup>E</sup>This

add street label to Drainage map Now

labeled

on the

map.

Channel E? Channel E

is now noted for clarity.

open-channel (Channel B) where it will discharge with Pond A and Pond B's outfall points to Plunge Pool 3. Basin EC12 is conveyed through culverts under SH94, north of Filing No. 3. The Mayberry Filing No. 3 FDR continues this offsite flow via an open channel to the south where the ultimate discharge point enters the existing Log Road roadside ditch with the outfall of Pond D. This master drainage plan recommends continuing this flow via storm pipe along the same alignment as the existing Filing 3 channel to support the proposed development. The discharge location will remain the same.

master drainage plan recommends continuing this flow south until it reaches a defined

**B. Existing Basins** 

## Channel F? Channel F is now noted for clarity.

should this be EC10 as this offsite flow is on the eastern side of filing 3& 4?

Historic drainage conditions for this MUDP assume Mayberry Filings 1, Yes, this was an error. to exist. This will include single family homes, apartment buildings, tow Text corrected roadways, and commercial lots. The remaining undeveloped land to th accordingly. filings are depicted as pastures. Existing basins EX-A and EX-B depict the developed Mayberry Filings approved or currently under review with El Paso County as forementioned. Existing Basins EX-C, EX-D, EX-E, and EX-F depict the areas undeveloped on the Mayberry property. The general flow pattern of the entire site gradually falls from the northwest to the southeast at slopes ranging from one to two percent. Stormwater currently sheetflows across the eastern and southern property boundaries.

## C. Developed Drainage Basins

The developed drainage basins and projected flows are shown in the proposed drainage maps in Appendix D. A description of each basin is as follows:

Drainage Basin A is a total of 81 acres consisting of multifamily development and commercial development located in the northwest portion of the site. Stormwater is anticipated to be routed via curb and gutter, storm pipe, and Channel A to ultimately be detained by Pond A in the lower southeast corner of the basin.

Drainage Basin B is a total of 106 acres consisting of single-family homes, multifamily development, and commercial development. Basin B encompasses Mayberry Filings 1 and 5. Stormwater is anticipated to be routed via curb and gutter and storm pipe to ultimately be detained by Pond B in the lower southeast corner of the basin.

<u>Drainage Basin D</u> is a total of 110 acres consisting of single-family homes, multifamily development, and commercial development. Basin D encompasses Mayberry Filings 2, 3, and 4. Stormwater is anticipated to be routed via curb and gutter, storm pipe, and Channel D to ultimately be detained by Pond D in the lower southeast corner of the basin.

<u>Drainage Basin E</u> is a total of 73 acres consisting of single-family homes and commercial development located in the northeast portion of the site. Stormwater is anticipated to be routed via curb and gutter and storm pipe to ultimately be detained by Pond E in the lower southeast corner of the basin.

<u>Drainage Basin F</u> is a total of 75 acres consisting of single-family homes and multifamily development located in the southwest portion of the site. Stormwater is anticipated to be routed via curb and gutter, storm pipe, and Channel F to ultimately be detained by Pond F in the lower south side of the basin.

<u>Drainage Basin G</u> is a total of 160 acres consisting of single-family homes and multifamily development located in the southeast portion of the site. Stormwater is anticipated to be routed via curb and gutter, storm pipe, and Channel G to ultimately be detained by Pond G in the lower southeast corner of the basin.

## D. Detention Design

An extended detention basin is proposed for each major drainage basin to mitigate developed stormwater flows leaving the site. The total volume requiring storage is equivalent to the 100 Year + ½ WQCV produced by the onsite developed area. See Appendix C for each respective MHFD worksheet. A description of each EDB is as follows:

<u>Pond A</u> is located at the southeast corner of drainage Basin A. Based on the tributary landuse, the required volume for the pond is 11.8 acre-feet. Pond A will discharge into an underground RCP pipe that will continue east under Boulevard A until the flow ultimately discharges into a channel combined with the Pond B outfall and the offsite basin EC11.

<u>Pond B</u> is located at the southeast corner of drainage Basin B. Based on the tributary landuse, the required volume for the pond is 15.7 acre-feet. Once Pond B is fully developed and functioning, the existing Pond C, designed and constructed within Mayberry Filing No. 1, will be filled in and taken offline. Pond B will discharge into Channel B, combining with the flow from offsite basin EC11. Discuss Plunge Pool 3

Pond D is located at the southeast corner use, the required volume for the pond i approved in the Filing No. 3 Final Drain Pond design is sufficient for this full development, the configuration will be revised to

### **MAYBERRY COMMUNITIES**

#### MASTER DEVELOPMENT DRAINAGE PLAN

accommodate this future layout of single-family lots. Pond D will discharge into Channel F, combining with the flow from offsite basin EC10.

Channel F? (see SF2219) Channel F is now noted.

<u>Pond E</u> is located at the southeast corner of drainage Basin E. Based on the tributary landuse, the required volume for the pond is 11.1 acre-feet. Pond E will discharge into Channel E, combining with the flow from Pond D and the offsite basin, EC10. Discuss Plunge Pool 4

Pond F is located at the southern boundary of drainage Basin F. Based land-use, the required volume for the pond is 11.3 acre-feet. Pond F w Plunge Pool 1, where stormwater flow will slow down and sheet-flow o property.

<u>Pond G</u> is located at the southeast corner of drainage Basin G. Based on the tributary landuse, the required volume for the pond is 22.6 acre-feet. Pond G will discharge into Plunge Pool 2, where stormwater flow will slow down and sheet-flow onto the adjacent property.

## E. Open Channels

Six open channels are proposed as part of this master development: A, B, D, E, F, and G. These channels will generally be designed as stable native grass-lined channels with subcritical flow regimes. Drainage channels have been designed to convey the 100-year flows, with trapezoidal cross-sections, side slopes of 4:1, and a minimum freeboard of 1-foot. Channel geometry can be subject to change in the final drainage reports for future filings, however the conservative parameters for the preliminary design is as follows:

<u>Channel A</u> conveys flows from portions of Basin A, with a tributary area of 11.6 acres (see Appendix B). The channel is trapezoidal with a bottom width of 8 feet and a total depth of 2.5'. The channel is recommended to be lined with a native grass mixture.

<u>Channel B</u> conveys flows from the offsite basin, EC11. The flows for EC11 have been taken from the approved Final Drainage Report for Mayberry Filing No. 1A (see Appendix E for referenced calculations). The channel is trapezoidal with a bottom width of 8 feet and a total depth of 3.5'. The channel is recommended to be lined with a native grass mixture.

<u>Channel D</u> conveys flows from the northern portion of Basin D, assumed to be existing as Mayberry Filings 2, 3, and 4. The flows have been taken from the approved Final Drainage Report for Mayberry Filing No. 3 (see Appendix E for referenced calculations). The channel is trapezoidal with a bottom width of 8 feet and a total depth of 4'. The channel is recommended to be lined with a native grass mixture.

Now Channel F

<u>Channel E</u> conveys flows from the offsite basin, EC10 and the discharge of Pond D. The flows for EC10 have been taken from the approved Final Drainage Report for Mayberry Filing No. 3 (see Appendix E for referenced calculations). The channel is trapezoidal with

a bottom width of 8 feet and a total depth of 3.5'. The channel is recommended to be lined with a native grass mixture.

## Now Channel H

<u>Channel F</u> conveys flows from portions of Basin F, with a tributary area of 24 acres (see Appendix B). The channel is trapezoidal with a bottom width of 8 feet and a total depth of 2.5'. The channel is recommended to be lined with a native grass mixture.

<u>Channel G</u> conveys flows from portions of Basin G, with a tributary area of 64.4 acres (see Appendix B). The channel is trapezoidal with a bottom width of 8 feet and a total depth of 3'. The channel is recommended to be lined with a native grass mixture.

## F. Culverts

Eight culverts are proposed beneath proposed roadways crossing the open channels. The culverts are designed so that during the 100-year storm event, water levels do not exceed 12 inches above finished grade when overtopping the roadway above per Table 6-4 of EPC DCM.

Culverts 1 and 2 will continue the stormwater flows of Channel B, consisting of the offsite basin, EC11 and the Pond B outfall. Culvert 3 will continue the stormwater flows of Channel E, consisting of the offsite basin, EC10 and the Pond D outfall. Culverts 4, 5, and 6 will continue the stormwater flows of Channel G. Lastly, culverts 7 and 8 will continue stormwater flows of Channel F. Refer to Appendix E for supporting calculations of the 5-year and 100-year flows for culverts 1, 2, and 3. Refer to Appendix B for supporting calculations of the 5-year and 100-year and 100-year flows for culverts 4, 5, 6, 7, and 8.

## G. Riprap and Plunge Pools

Rip-Rap and plunge pools are recommended to be sized for the 100 year storm per UDFCD Chapter 9 Section 3.2.1 and 3.2.2. Rip-rap shall be placed where all pipes discharge into channels across the site and is sized to reduce velocities to 5 feet per second (fps). Plunge pools have been proposed where flows from the extended detention basins discharge before ultimately leaving the property. The plunge pools shall be sized to reduce velocities to 1.3 fps to ensure flows leaving the property are as non-erosive as possible and sheet-flow onto the adjacent properties to maintain historic pool 3 is adjacent to flow patterns. plunge pool 4 pond B Corrected. Plunge Pool 1, locate Corrected. Pond B, will mitigate Por lls, and the offsite flow of Basin EC11. Plunge Pool 2, focated south of Pond E and west of Log Road, will mitigate Pond D and E outfalls, and the offsite flow of Basin EC10 before discharging to the existing roadside ditch along Log Road. Plunge Pool 3 is located south of Pond F and will mitigate the Pond F outfall. Plunge Pool 4 is located south of Pond G and will mitigate the Pond G outfall. Corrected.

2

Corrected.

- 12 -

Please discuss the downstream conditions of each of the design points where flows are conveyed offsite. Discuss the ultimate outfall for these flows. For example is Log Rd ditch anticipated to need improvements; will the flows from DP 4 continue south and cross handle Rd ultimately ending up at Black Squirrel Creek? please address

## H. Analysis of Existing and Propos

The general concept of the pro

from the developed site by rout

A discussion has been added to this section about the ultimate receiving body/basin and condition.

te peak flows on ponds. The

onsite detention ponds are designed to convert the developed flows from the Mayberry Communities master to historic levels before discharging to the adjacent property. The historic drainage patterns show stormwater sheet-flowing across the project boundaries along the southern and eastern property lines. As the proposed detention ponds will create a point discharge condition, plunge pools are recommended to slow down the stormwater flow, and convert the point discharge to a sheet-flow condition as the plunge pools will allow the stormwater to slowly spill over. A detail of a plunge pool has been added to Appendix C.

## I. Anticipated Drainage Problems and Solutions

The proposed stormwater detention ponds are designed to mitigate the impacts of developed drainage from this master planned development. The overall drainage plan anticipates a system of improved public streets with curb and gutter, storm inlets, and storm sewers conveying developed flows to improved drainage channels running throughout the site. The primary drainage problems anticipated within this development will consist of maintenance of these storm sewer systems, culverts, drainage channels, and detention pond facilities. Continuing maintenance will need to be implemented for proper erosion control measures in the proposed channels and swales, which will be designed to meet allowable velocity criteria.

A trail system shall be constructed along the major drainage channels to provide maintenance access to the drainage facilities throughout the development. Proper construction and maintenance of the proposed detention facilities will minimize downstream drainage impacts. The proposed detention ponds and channels throughout the site will be privately owned and maintained by the homeowner's association or metropolitan district.

Address water quality for the site.

A water quality section has been added to the report as section V.

please include in the narrative the total flows at the design points. These will be the basis for future final drainage reports

## V. SUMMARY

A description and table is now added to the report in section C.

The proposed Mayberry Communities master development will generate an increase in developed runoff from the site, which will be mitigated through construction of on-site

stormwater detention facilities. The proposed drainage patterns will remain consistent with historic conditions, and new drainage facilities constructed to El Paso County standards will safely convey runoff to adequate outfalls protected by utilizing the design of plunge pools. The proposed detention ponds at the south and east boundaries of the site will ensure that developed flows from Mayberry Communities remain below historic levels. Construction of the proposed drainage facilities will ensure that this subdivision will not adversely affect downstream or surrounding areas.

## VI. Appendix

Appendix A – Referenced Maps

- Vicinity Map
- Soils Map
- FEMA Map

Appendix B – Hydrologic Calculations

Appendix C – Hydraulic Calculations

- **C1.** Detention Basin Volumes
- C2. Open Channels
- C3. Culvert Sizing

Appendix D – Drainage Maps

Appendix E – Referenced Drainage Reports

# **APPENDIX A – REFERENCED MAPS**





United States Department of Agriculture



Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

# Custom Soil Resource Report for El Paso County Area, Colorado

Mayberry Colorado Springs -MDDP



# Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2\_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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# **How Soil Surveys Are Made**

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

# Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP LEGEND			)	MAP INFORMATION		
Area of In	terest (AOI)	201	Spoil Area	The soil surveys that comprise your AOI were mapped at 1:24 000		
	Area of Interest (AOI)	۵	Stony Spot	,		
Soils	Soil Man Unit Polygons	0	Very Stony Spot	Please rely on the bar scale on each map sheet for map		
	Soil Map Unit Lines	Ŷ	Wet Spot	measurements.		
<u>~</u>	Soil Map Unit Points	$\triangle$	Other	Source of Map: Natural Resources Conservation Service		
Spacial	Point Foaturos	, <b>*</b> *	Special Line Features	Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)		
fol	Blowout	Water Fea	atures			
N N	Borrow Pit	$\sim$	Streams and Canals	Maps from the Web Soil Survey are based on the Web Mercator		
	Clay Shat	Transport	ation	distance and area. A projection that preserves area, such as the		
英	Ciay Spot	+++	Rails	Albers equal-area conic projection, should be used if more		
$\diamond$	Closed Depression	~	Interstate Highways	accurate calculations of distance or area are required.		
X	Gravel Pit	~	US Routes	This product is generated from the USDA-NRCS certified data as		
***	Gravelly Spot	~	Major Roads	of the version date(s) listed below.		
٥	Landfill	~	Local Roads	Soil Survey Area: El Paso County Area, Colorado		
A.	Lava Flow	Backgrou	nd	Survey Area Data: Version 20, Sep 2, 2022		
عليہ	Marsh or swamp	Mar.	Aerial Photography	Soil man units are labeled (as space allows) for man scales		
R	Mine or Quarry			1:50,000 or larger.		
0	Miscellaneous Water			Data(c) parial images were photographod: Sop 11, 2018. Oct		
0	Perennial Water			20, 2018		
$\vee$	Rock Outcrop			The other has a other base man on which the soil lines were		
⊹	Saline Spot			compiled and digitized probably differs from the background		
	Sandy Spot			imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident		
-	Severely Eroded Spot					
$\diamond$	Sinkhole					
∌	Slide or Slip					
Ś	Sodic Spot					

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	930.4	61.7%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	29.7	2.0%
28	Ellicott loamy coarse sand, 0 to 5 percent slopes	29.4	1.9%
95	Truckton loamy sand, 1 to 9 percent slopes	519.2	34.4%
Totals for Area of Interest		1,508.7	100.0%

# Map Unit Legend

# Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

## El Paso County Area, Colorado

## 8-Blakeland loamy sand, 1 to 9 percent slopes

#### **Map Unit Setting**

National map unit symbol: 369v Elevation: 4,600 to 5,800 feet Mean annual precipitation: 14 to 16 inches Mean annual air temperature: 46 to 48 degrees F Frost-free period: 125 to 145 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

Blakeland and similar soils: 98 percent Minor components: 2 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Blakeland**

#### Setting

Landform: Flats, hills Landform position (three-dimensional): Side slope, talf Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium derived from sedimentary rock and/or eolian deposits derived from sedimentary rock

#### **Typical profile**

A - 0 to 11 inches: loamy sand AC - 11 to 27 inches: loamy sand C - 27 to 60 inches: sand

#### **Properties and qualities**

Slope: 1 to 9 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat excessively drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 5 percent
Available water supply, 0 to 60 inches: Low (about 4.5 inches)

#### Interpretive groups

Land capability classification (irrigated): 3e Land capability classification (nonirrigated): 6e Hydrologic Soil Group: A Ecological site: R049XB210CO - Sandy Foothill Hydric soil rating: No

#### **Minor Components**

#### Other soils

Percent of map unit: 1 percent

Hydric soil rating: No

#### Pleasant

Percent of map unit: 1 percent Landform: Depressions Hydric soil rating: Yes

### 19—Columbine gravelly sandy loam, 0 to 3 percent slopes

#### **Map Unit Setting**

National map unit symbol: 367p Elevation: 6,500 to 7,300 feet Mean annual precipitation: 14 to 16 inches Mean annual air temperature: 46 to 50 degrees F Frost-free period: 125 to 145 days Farmland classification: Not prime farmland

#### Map Unit Composition

Columbine and similar soils: 97 percent Minor components: 3 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Columbine**

#### Setting

Landform: Fans, fan terraces, flood plains Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium

#### **Typical profile**

*A - 0 to 14 inches:* gravelly sandy loam *C - 14 to 60 inches:* very gravelly loamy sand

#### **Properties and qualities**

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Very low (about 2.5 inches)

#### Interpretive groups

Land capability classification (irrigated): 4e Land capability classification (nonirrigated): 6e Hydrologic Soil Group: A Ecological site: R049XY214CO - Gravelly Foothill Hydric soil rating: No

#### **Minor Components**

#### Fluvaquentic haplaquolls

Percent of map unit: 1 percent Landform: Swales Hydric soil rating: Yes

#### Other soils

*Percent of map unit:* 1 percent *Hydric soil rating:* No

#### Pleasant

Percent of map unit: 1 percent Landform: Depressions Hydric soil rating: Yes

### 28—Ellicott loamy coarse sand, 0 to 5 percent slopes

#### **Map Unit Setting**

National map unit symbol: 3680 Elevation: 5,500 to 6,500 feet Mean annual precipitation: 13 to 15 inches Mean annual air temperature: 47 to 50 degrees F Frost-free period: 125 to 145 days Farmland classification: Not prime farmland

#### Map Unit Composition

*Ellicott and similar soils:* 97 percent *Minor components:* 3 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Ellicott**

#### Setting

Landform: Stream terraces, flood plains Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Parent material: Sandy alluvium

#### **Typical profile**

A - 0 to 4 inches: loamy coarse sand

C - 4 to 60 inches: stratified coarse sand to sandy loam

#### Properties and qualities

*Slope:* 0 to 5 percent *Depth to restrictive feature:* More than 80 inches *Drainage class:* Somewhat excessively drained *Runoff class:* Very low

#### **Custom Soil Resource Report**

Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr) Depth to water table: More than 80 inches

Frequency of flooding: NoneFrequent Frequency of ponding: None Available water supply, 0 to 60 inches: Low (about 4.1 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7w Hydrologic Soil Group: A Ecological site: R069XY031CO - Sandy Bottomland Other vegetative classification: SANDY BOTTOMLAND (069AY031CO) Hydric soil rating: No

#### Minor Components

#### Fluvaquentic haplaquoll

Percent of map unit: 1 percent Landform: Swales Hydric soil rating: Yes

#### Other soils

Percent of map unit: 1 percent Hydric soil rating: No

#### Pleasant

Percent of map unit: 1 percent Landform: Depressions Hydric soil rating: Yes

### 95—Truckton loamy sand, 1 to 9 percent slopes

#### Map Unit Setting

National map unit symbol: 2yvrm Elevation: 5,800 to 7,100 feet Mean annual precipitation: 12 to 19 inches Mean annual air temperature: 46 to 50 degrees F Frost-free period: 90 to 155 days Farmland classification: Not prime farmland

#### Map Unit Composition

*Truckton and similar soils:* 87 percent *Minor components:* 13 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### Description of Truckton

#### Setting

Landform: Interfluves, fan remnants Down-slope shape: Linear Across-slope shape: Linear Parent material: Wind re-worked alluvium derived from arkose

#### **Typical profile**

A - 0 to 4 inches: loamy sand Bt1 - 4 to 12 inches: sandy loam Bt2 - 12 to 19 inches: sandy loam C - 19 to 80 inches: sandy loam

#### **Properties and qualities**

Slope: 1 to 9 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 1 percent
Maximum salinity: Nonsaline to very slightly saline (0.1 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: Moderate (about 6.5 inches)

#### Interpretive groups

Land capability classification (irrigated): 6e Land capability classification (nonirrigated): 6e Hydrologic Soil Group: A Ecological site: R049XB210CO - Sandy Foothill Hydric soil rating: No

#### **Minor Components**

#### Blakeland

Percent of map unit: 5 percent Landform: Interfluves, hills Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Crest, side slope Down-slope shape: Linear, convex Across-slope shape: Linear, convex Ecological site: R049XB210CO - Sandy Foothill Hydric soil rating: No

#### Bresser

Percent of map unit: 5 percent Landform: Interfluves, terraces Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Ecological site: R049XB210CO - Sandy Foothill Hydric soil rating: No

#### Urban land

Percent of map unit: 2 percent Hydric soil rating: No

#### Ellicott, occasionally flooded

Percent of map unit: 1 percent Landform: Flood plains, drainageways

## Custom Soil Resource Report

*Down-slope shape:* Linear *Across-slope shape:* Linear, concave *Ecological site:* R067BY031CO - Sandy Bottomland *Hydric soil rating:* No

# **Soil Information for All Uses**

# **Soil Properties and Qualities**

The Soil Properties and Qualities section includes various soil properties and qualities displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each property or quality.

## **Soil Erosion Factors**

Soil Erosion Factors are soil properties and interpretations used in evaluating the soil for potential erosion. Example soil erosion factors can include K factor for the whole soil or on a rock free basis, T factor, wind erodibility group and wind erodibility index.

## K Factor, Whole Soil (Mayberry Master Drainage Plan)

Erosion factor K indicates the susceptibility of a soil to sheet and rill erosion by water. Factor K is one of six factors used in the Universal Soil Loss Equation (USLE) and the Revised Universal Soil Loss Equation (RUSLE) to predict the average annual rate of soil loss by sheet and rill erosion in tons per acre per year. The estimates are based primarily on percentage of silt, sand, and organic matter and on soil structure and saturated hydraulic conductivity (Ksat). Values of K range from 0.02 to 0.69. Other factors being equal, the higher the value, the more susceptible the soil is to sheet and rill erosion by water.

"Erosion factor Kw (whole soil)" indicates the erodibility of the whole soil. The estimates are modified by the presence of rock fragments.

Factor K does not apply to organic horizons and is not reported for those layers.


MAP INFORMATION

# MAP LEGEND



Table—K Factor,	Whole Soil	(Mayberry	Master	Drainage	Plan)
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Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	.10	930.4	61.7%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	.10	29.7	2.0%
28	Ellicott loamy coarse sand, 0 to 5 percent slopes	.17	29.4	1.9%
95	Truckton loamy sand, 1 to 9 percent slopes	.24	519.2	34.4%
Totals for Area of Intere	est		1,508.7	100.0%

# Rating Options—K Factor, Whole Soil (Mayberry Master Drainage Plan)

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher Layer Options (Horizon Aggregation Method): Surface Layer (Not applicable)

# **Soil Qualities and Features**

Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

# Hydrologic Soil Group (Mayberry Master Drainage Plan)

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.





# Table—Hydrologic Soil Group (Mayberry Master Drainage Plan)

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	930.4	61.7%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	A	29.7	2.0%
28	Ellicott loamy coarse sand, 0 to 5 percent slopes	A	29.4	1.9%
95	Truckton loamy sand, 1 to 9 percent slopes	A	519.2	34.4%
Totals for Area of Intere	st		1,508.7	100.0%

# Rating Options—Hydrologic Soil Group (Mayberry Master Drainage Plan)

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

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	SPECIAL FLOO	D HAZARD AREAS (SFHAS) SUBJECT TO
The 1% annu	INUNDATION B	Y THE 1% ANNUAL CHANCE FLOOD -year flood), also known as the base flood, is the flood
that has a 1% Hazard Area i Special Flood Elevation is th	<ul> <li>chance of being eq</li> <li>is the area subject</li> <li>Hazard include Zone</li> <li>water-surface eleva</li> </ul>	Jualed or exceeded in any given year. The Special Flood to flooding by the 1% annual chance flood. Areas of the A, AE, AH, AO, AR, A99, V, and VE. The Base Flood ation of the 1% annual chance flood.
ZONE AE ZONE AH	Base Flood Elevation Flood depths of 1	ns determined. Is determined. It to 3 feet (usually areas of ponding); Base Flood
ZONE AO	Elevations determin Flood depths of 1 to	o 3 feet (usually sheet flow on sloping terrain); average
ZONE AR	depths determined determined. Special Flood Hazar flood by a flood con	nd Area Formerly protected from the 1% annual chance
ZONE A99	indicates that the fiprotection from the Area to be protect	ormer flood control system is being restored to provide 1% annual chance or greater flood. ted from 1% annual chance flood by a Federal flood
ZONE V	protection system determined.	under construction; no Base Flood Elevations
ZONE V	Elevations determin Coastal flood zone	e with velocity hazard (wave action); no Base Flood led. e with velocity hazard (wave action); Base Flood
7777	Elevations determin	ed. EAS IN ZONE AE
The floodway kept free of e	is the channel of a sencroachment so that	stream plus any adjacent floodplain areas that must be at the 1% annual chance flood can be carried without
substantial inc	OTHER FLOOD	ARFAS
ZONE X	Areas of 0.2% annu	ual chance flood; areas of 1% annual chance flood with
·	average depths of square mile; and ar	less than 1 foot or with drainage areas less than 1 reas protected by levees from 1% annual chance flood.
	OTHER AREAS	o be outside the 0.2% annual chance floodplain
ZONE D	Areas in which floor	d hazards are undetermined, but possible.
[[]]	COASTAL BARR	IER RESOURCES SYSTEM (CBRS) AREAS
	OTHERWISE PR	ROTECTED AREAS (OPAs)
CBRS areas ar	Floodp	plain boundary
		vay boundary D Boundary
•••••	CBRS a	and OPA boundary
E10	Bound Flood	ary dividing Special Flood Hazard Areas of different Base Elevations, flood depths or flood velocities.
EL 987	) Base F Base F elevati	Flood Elevation line and value; elevation in reet* Flood Elevation value where uniform within zone; ion in feet*
* Referenced	to the North America	in Vertical Datum of 1988 (NAVD 88)
(A) (22)	- A Cross	section line
97° 07' 30.	00" Geogra	aphic coordinates referenced to the North American
32° 22' 30.	00" Datum N 1000-r	n of 1983 (NAD 83) meter Universal Transverse Mercator grid ticks,
6000000	zone 1 FT 5000-f	3 foot grid ticks: Colorado State Plane coordinate
	system Lambe	n, central zone (FIPSZONE 0502), ert Conformal Conic Projection
DX5510	× Bench this FI	mark (see explanation in Notes to Users section of RM panel)
M1.5	River	Mile
	NVCI I	The
	Refer to	MAP REPOSITORIES Map Repositories list on Map Index
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# **APPENDIX B – HYDROLOGIC CALCULATIONS**

### **EXISTING C VALUES**

Designer	r: LAO		51			Glob	al Parameters <sup>1</sup>				Sumn	nary				
Company	R&R Engineers-Surveyo	rs			Li	and Use	% Imp.	C <sub>5</sub>	C <sub>100</sub>		Total Area (ac)	589.00				
Date	: 5/2/2023				SF LOTS (1/6 A	AC)*	65	0.45	0.59	*Using 1/8 fo	Composite Impervious	12.6%				
Project	: MAYBERRY SKETCH PLA	N		RSR	Commercial		95	0.81	0.88							
Location	EL PASO COUNTY, COLC	RADO			Multi-Family		95	0.81	0.88				1	From Table	6-3 in MHFD	Volume 1
			ENGIN	EERS	Pasture/Meado	ws	1	0.08	0.35				2	From Table	6-4 in MHFD	Volume 1
			SURVE	YORS							Cells of this color are fo	or required user-input				
											Cells of this color are fo	or optional user-input				
Basin Name	Area	NRCS Hydrologic Soil Group	SF LOT	S (1/6 AC)*	Co	mmercial	Multi-Fa	amily	Pasture/	Meadows	% Check	Percent Imperviousness		Runoff Coe	efficient, C <sup>2</sup>	
Basin Name	Area (ac)	NRCS Hydrologic Soil Group	SF LOT	S (1/6 AC)*	Co Area (ac)	ommercial %	Multi-Fa Area (ac)	amily %	Pasture/ Area (ac)	Meadows %	% Check	Percent Imperviousness	2-yr	Runoff Coe 5-yr	efficient, C <sup>2</sup> 10-yr	100-yr
Basin Name OFF-1	Area (ac) 44.00	NRCS Hydrologic Soil Group A	SF LOT Area (ac) 0.00	S (1/6 AC)* % 0.0%	Co Area (ac) 0.00	ommercial % 0.0%	Multi-Fa Area (ac) 0.00	amily % 0.0%	Pasture/ Area (ac) 44.00	Meadows % 100.0%	% Check	Percent Imperviousness	2-yr	Runoff Coe 5-yr 0.08	efficient, C <sup>2</sup> 10-yr	<b>100-yr</b> 0.35
Basin Name OFF-1 EX-A	Area (ac) 44.00 44.00	NRCS Hydrologic Soil Group A A	SF LOT: Area (ac) 0.00 31.69	S (1/6 AC)* % 0.0% 72.0%	Co Area (ac) 0.00 0.00	mmercial % 0.0% 0.0%	Multi-Fa Area (ac) 0.00 12.31	amily % 0.0% 28.0%	Pasture/ Area (ac) 44.00 0.00	Meadows % 100.0% 0.0%	% Check 100.00% 100.00%	Percent Imperviousness 1.0% 73.4%	2-yr	Runoff Coe 5-yr 0.08 0.55	efficient, C <sup>2</sup> 10-yr	<b>100-yr</b> 0.35 0.67
Basin Name OFF-1 EX-A EX-B	Area (ac) 44.00 44.00 100.00	NRCS Hydrologic Soil Group A A A	SF LOT: Area (ac) 0.00 31.69 36.80	S (1/6 AC)* % 0.0% 72.0% 36.8%	Co Area (ac) 0.00 0.00 14.20	mmercial % 0.0% 0.0% 14.2%	Multi-Fa Area (ac) 0.00 12.31 0.00	amily % 0.0% 28.0% 0.0%	Pasture/ Area (ac) 44.00 0.00 49.00	Meadows % 100.0% 0.0% 49.0%	% Check 100.00% 100.00% 100.00%	Percent Imperviousness 1.0% 73.4% 37.9%	2-yr	Runoff Coe 5-yr 0.08 0.55 0.32	efficient, C <sup>2</sup>	<b>100-yr</b> 0.35 0.67 0.51
Basin Name OFF-1 EX-A EX-B EX-C	Area (ac) 44.00 44.00 100.00 135.00	NRCS Hydrologic Soil Group A A A A	SF LOT Area (ac) 0.00 31.69 36.80 0.00	S (1/6 AC)* 0.0% 72.0% 36.8% 0.0%	Co Area (ac) 0.00 0.00 14.20 0.00	mmercial % 0.0% 0.0% 14.2% 0.0%	Multi-Fa Area (ac) 0.00 12.31 0.00 0.00	amily % 0.0% 28.0% 0.0% 0.0%	Pasture/ Area (ac) 44.00 0.00 49.00 135.00	Meadows % 100.0% 0.0% 49.0% 100.0%	% Check 100.00% 100.00% 100.00%	Percent Imperviousness 1.0% 73.4% 37.9% 1.0%	2-yr	Runoff Coe 5-yr 0.08 0.55 0.32 0.08	efficient, C <sup>2</sup>	<b>100-yr</b> 0.35 0.67 0.51 0.35
Basin Name OFF-1 EX-A EX-B EX-C EX-D	Area (ac) 44.00 44.00 100.00 135.00 185.00	NRCS Hydrologic Soil Group A A A A A A	SF LOT: Area (ac) 0.00 31.69 36.80 0.00 0.00	S (1/6 AC)* 0.0% 72.0% 36.8% 0.0% 0.0%	Co Area (ac) 0.00 0.00 14.20 0.00 0.00	mmercial % 0.0% 0.0% 14.2% 0.0% 0.0%	Multi-Fr Area (ac) 0.00 12.31 0.00 0.00 0.00	%           0.0%           28.0%           0.0%           0.0%	Pasture/ Area (ac) 44.00 0.00 49.00 135.00 185.00	Meadows % 100.0% 0.0% 49.0% 100.0%	% Check 100.00% 100.00% 100.00% 100.00%	Percent Imperviousness 1.0% 73.4% 37.9% 1.0% 1.0%	2-yr	Runoff Coe 5-yr 0.08 0.55 0.32 0.08 0.08	efficient, C <sup>2</sup>	<b>100-yr</b> 0.35 0.67 0.51 0.35 0.35
Basin Name OFF-1 EX-A EX-B EX-C EX-D EX-E	Area (ac) 44.00 44.00 100.00 135.00 185.00 59.00	NRCS Hydrologic Soil Group	SF LOT.           Area (ac)           0.00           31.69           36.80           0.00           0.00           0.00	S (1/6 AC)* 0.0% 72.0% 36.8% 0.0% 0.0%	Co Area (ac) 0.00 0.00 14.20 0.00 0.00 0.00	mmercial % 0.0% 0.0% 14.2% 0.0% 0.0% 0.0%	Multi-Fr Area (ac) 0.00 12.31 0.00 0.00 0.00 0.00	%           0.0%           28.0%           0.0%           0.0%           0.0%           0.0%	Pasture/ Area (ac) 44.00 0.00 49.00 135.00 185.00 59.00	%           100.0%           0.0%           49.0%           100.0%           100.0%	% Check 100.00% 100.00% 100.00% 100.00% 100.00%	Percent Imperviousness 1.0% 73.4% 37.9% 1.0% 1.0% 1.0%	2-yr	S-yr           0.08           0.55           0.32           0.08           0.08	efficient, C <sup>2</sup> 10-yr	100-yr 0.35 0.67 0.51 0.35 0.35 0.35

## TIME OF CONCENTRATION

Designer Company Date Project Location	: LAO : R&R Enginee : 5/2/2023 : MAYBERRY S : EL PASO CO	ers-Surveyors SKETCH PLAN UNTY, COLORAD			$t_i = \frac{0.399}{60}$ $t_t = \frac{1}{60}$ Regional	$\frac{\frac{5(1.1 - C_5)}{S_i^{0.33}}}{\frac{L_t}{K\sqrt{S_t}} = \frac{L}{60}}$ $t_e = (26 - 1)$	$\frac{\sqrt{L_i}}{V_t}$	Computed $t_c = t$ elected $t_c = max$ $\frac{L_t}{(4i+9)\sqrt{S_t}}$	$t_{i} + t_{t}$ $t_{n}$ $t_{n}$	ninimum = 5 (urb ninimum = 10 (no nin(Computed to Cells of this c	on-urban) t <sub>c</sub> , Regional t <sub>c</sub> ) olor are for require	} ed user-input			RER ENGINEERS SURVEYORS
	Subbasi	n Data		Overla	nd (Initial) Fl	ow Time		Channe	elized (Travel) F	ow Time			Time of C	oncentration	
Basin	Area	% Impervious	C5	Overland Flow Length L <sub>i</sub> (ft)	Overland Flow Slope S <sub>i</sub> (ft/ft)	Overland Flow Time t <sub>i</sub> (min)	Channelized Flow Length L <sub>+</sub> (ft)	Channelized Flow Slope S. (ft/ft)	NRCS Conveyance	Channelized Flow Velocity	Channelized Flow Time	Computed t <sub>c</sub> (min)	Regional t <sub>c</sub> (min)	Selected t <sub>c</sub> (min)	Remarks
<b>E</b> 1/ A		4				1		5t (10/10)	Factor K	v <sub>t</sub> (it/sec)	<b>c</b> t (iiiii)				
EX-A	44.00	73.4%	0.55	36.00	0.020	4.73	1000.00	0.010	20	2.00	8.33	13.07	22.17	13.07	
EX-A EX-B	44.00	73.4% 37.9%	0.55	36.00 36.00	0.020	4.73 6.72	1000.00 1500.00	0.010 0.010	20 20	2.00 2.00	8.33 12.50	13.07 19.22	22.17 37.03	13.07 19.22	
EX-A EX-B EX-C	44.00 100.00 135.00	73.4% 37.9% 1.0%	0.55 0.32 0.08	36.00 36.00 500.00	0.020 0.020 0.010	4.73 6.72 41.18	1000.00 1500.00 1000.00	0.010 0.010 0.010	20 20 7	2.00 2.00 0.70	8.33 12.50 23.81	13.07 19.22 64.99	22.17 37.03 44.06	13.07 19.22 44.06	
EX-A EX-B EX-C EX-D	44.00 100.00 135.00 185.00	73.4% 37.9% 1.0% 1.0%	0.55 0.32 0.08 0.08	36.00 36.00 500.00 500.00	0.020 0.020 0.010 0.010	4.73 6.72 41.18 41.18	1000.00 1500.00 1000.00 1500.00	0.010 0.010 0.010 0.010 0.010	20 20 7 7 7	2.00 2.00 0.70 0.70	8.33 12.50 23.81 35.71	13.07 19.22 64.99 76.89	22.17 37.03 44.06 53.18	13.07 19.22 44.06 53.18	
EX-A EX-B EX-C EX-D EX-E	44.00 100.00 135.00 185.00 59.00	73.4% 37.9% 1.0% 1.0% 1.0%	0.55 0.32 0.08 0.08 0.08	36.00 36.00 500.00 500.00 500.00	0.020 0.020 0.010 0.010 0.010	4.73 6.72 41.18 41.18 41.18	1000.00 1500.00 1000.00 1500.00 1200.00	0.010 0.010 0.010 0.010 0.010	20 20 7 7 7 7 7	2.00 2.00 0.70 0.70 0.70	8.33 12.50 23.81 35.71 28.57	13.07 19.22 64.99 76.89 69.75	22.17 37.03 44.06 53.18 47.71	13.07 19.22 44.06 53.18 47.71	

#### STORM DRAINAGE SYSTEM DESIGN - 5-YEAR DESIGN STORM

Designer: Company: Date: Project: Location:	LAO R&R Engineers-Survey 5/2/2023 MAYBERRY SKETCH PL EL PASO COUNTY, COL	ors AN .ORADO				-	Cells o	of this colo of this colo	r are for ree r are for op	quired use	r-input r-input	16=-1.5	50 ln(D) +	7.583										ENGINEERS SURVEYORS
	STREET/ DIRECT RUNOFF 1							OTAL RUNC	DFF			STREET	BYPASS			PIPE		1	TRAVEL TIM	1E				
DESGIN POINT	CONTRIBUTING	Basin Name	Area	Coeff	Тс	C*A	I.	Q	Тс	Sum Area	Sum C*A	1	Q	Street Q	Street Slope	Length	Street Tt	Design Q	Slope	PIPE	L	VEL	Tt	Remarks
	BASINS		(ac)	с	(min)	(ac)		(cfs)	(min)	(ac)	(ac)	in/hr	cfs	cfs	%	ft	min	cfs	%	SIZE	ft	ft/sec	min	
		EX-A	44	0.55	13.1	24.23	6.26	151.7										151.7					1	
1																								
		EX-B	100	0.32	19.2	31.98	3.01	96.3										96.3						
2																								
		EX-C	135	0.08	44.1	10.80	1.86	20.1										20.1						
3																								
		EX-D	185	0.08	53.2	14.80	1.64	24.3										24.3						
4																								
		EX-E	59	0.08	47.7	4.72	1.76	8.3										8.3						
5																								
		EX-F	22	0.08	34.9	1.76	2.15	3.8										3.8						
6								-					. —											

#### STORM DRAINAGE SYSTEM DESIGN - 100-YEAR DESIGN STORM

Designer: Company: Date: Project: Location:	LAO R&R Engineers-Survey 5/2/2023 MAYBERRY SKETCH PL EL PASO COUNTY, COL	ors AN .ORADO				=	Cells Cells	of this colo of this colo	r are for re r are for o	equired use	er-input er-input	I <sub>19</sub>	= -2.52 1	n(D) + 12.	735									ENGINEERS SURVEYORS
	SGIN STREET/ Basin									T	OTAL RUNG	DFF			STREET	BYPASS			PIPE		T	RAVEL TIN	AE .	
DESGIN POINT	CONTRIBUTING	Basin Name	Area	Coeff	Тс	C*A	1	Q	Тс	Sum Area	Sum C*A	1	Q	Street Q	Street Slope	Length	Street Tt	Design Q	Slope	PIPE	L	VEL	Tt	Remarks
	DASINS		(ac)	с	(min)	(ac)		(cfs)	(min)	(ac)	(ac)	in/hr	cfs	cfs	%	ft	min	cfs	%	SIZE	ft	ft/sec	min	
		EX-A	44	0.67	13.1	29.53	6.26	184.8										184.8						
1																								
		EX-B	100	0.51	19.2	51.36	5.29	271.5										271.5						
2																								
		EX-C	135	0.35	44.1	47.25	3.20	151.0										151.0						
3																								
		EX-D	185	0.35	53.2	64.75	2.72	176.2										176.2						
4																								
		EX-E	59	0.35	47.7	20.65	2.99	61.8										61.8						
5																								
		EX-F	22	0.35	34.9	7.70	3.78	29.1										29.1						
6				1		1		1																

#### POST-DEVELOPMENT C VALUES

Designer:	LAO		51	1		Globa	al Parameters1						Summ	nary				
Company:	R&R Engineers-Surveyor	S			Li	and Use	% Imp.	C <sub>5</sub>	C <sub>100</sub>				Total Area (ac)	849.10				
Date:	6/29/2023				SF LOTS (1/6 A	C)*	65	0.45	0.59	*Using 1/8 fo	r conservative	ness	Composite Impervious	51.0%				
Project:	MAYBERRY SKETCH PLAN	4		<b>B</b> SB	Commercial		95	0.81	0.88									
Location:	FL PASO COUNTY, COLOR	RADO		NOIN	Multi-Family		95	0.81	0.88						1	From Table (	ô-3 in MHFD	Volume 1
	,		ENGIN	EERS =	Neighborhood A	reas	70								2	From Table (	6-4 in MHFD	Volume 1
			SURVE	YORS	Park		7						Cells of this color are fo	r required user-input	1	Troni Tubic (		volume 1
					I dik		,						Cells of this color are fo	r optional user-input				
					I .									optional user-input				
Basin Name	Area	NRCS Hydrologic Soil Group	SF LOT:	5 (1/6 AC)*	Co	mmercial	Multi-Fa	mily	Neighborh	lood Areas	Pa	rk	% Check	Percent Imperviousness		Runoff Coe	fficient, C <sup>2</sup>	
	(ac)		Area (ac)	%	Area (ac)	%	Area (ac)	%	Area (ac)	%	Area (ac)	%			2-yr	5-yr	10-yr	100-yr
А	81.00	A	0.00	0.0%	14.90	18.4%	29.70	36.7%	20.50	25.3%	15.90	19.6%	100.00%	71.4%		0.45		0.48
В	106.00	A	74.63	70.4%	0.00	0.0%	26.17	24.7%	5.20	4.9%	0.00	0.0%	100.00%	72.7%		0.52		0.63
D	110.00	A	95.50	86.8%	14.50	13.2%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	69.0%		0.50	,	0.63
E	73.00	A	49.29	67.5%	23.71	32.5%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	74.7%		0.57	,	0.68
F	75.00	A	53.40	71.2%	0.00	0.0%	21.60	28.8%	0.00	0.0%	0.00	0.0%	100.00%	73.6%		0.55		0.67
G	160.00	A	132.70	82.9%	27.30	17.1%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	70.1%		0.51		0.64
Channel G	64.40	A	46.10	71.6%	0.00	0.0%	18.30	28.4%	0.00	0.0%	0.00	0.0%	100.00%	73.5%		0.55		0.67
Channel A	11.60	A	0.00	0.0%	0.00	0.0%	11.60	100.0%	0.00	0.0%	0.00	0.0%	100.00%	95.0%		0.81	,	0.88
Channel F	24.00	A	24.00	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	65.0%		0.45	,	0.59
Culvert 4	7.80	A	0.00	0.0%	0.00	0.0%	7.80	100.0%	0.00	0.0%	0.00	0.0%	100.00%	95.0%		0.81		0.88
Culvert 5	36.50	A	22.00	60.3%	0.00	0.0%	14.50	39.7%	0.00	0.0%	0.00	0.0%	100.00%	76.9%		0.59		0.71
Culvert 6	64.40	A	49.90	77.5%	0.00	0.0%	14.50	22.5%	0.00	0.0%	0.00	0.0%	100.00%	71.8%		0.53		0.66
Culvert 7	15.70	A	15.70	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	65.0%		0.45		0.59
Culvert 8	19.70	A	19.70	100.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	0.00	0.0%	100.00%	65.0%		0.45		0.59

## TIME OF CONCENTRATION

Designer	: LAO			] [	$t_i = \frac{0.395}{1000}$	5(1.1 - C <sub>5</sub> ) S <sup>0.33</sup>	$\frac{1}{\sqrt{L_i}}$	Computed t <sub>c</sub> = t	$t_i + t_t$ $t_i$	<sub>minimum</sub> = 5 (urb <sub>minimum</sub> = 10 (n	oan) on-urban)				
Date	: 6/29/2023	SKETCH PLAN			$t_t = \frac{1}{60}$	$\frac{L_t}{K\sqrt{S_t}} = \frac{1}{60}$	DV <sub>t</sub> S	elected $t_c = matrix$	x{t <sub>minimum</sub> , 1	nin(Computed	t <sub>c</sub> , Regional t <sub>c</sub> )	)}			RER
Location	EL PASO CO	UNTY, COLORAD	0		Regional	t <sub>e</sub> = (26 -	$17i) + \frac{1}{60(1)}$	$\frac{L_t}{(4i+9)\sqrt{S_t}}$		Cells of this of	olor are for requir	ed user-input	]		ENGINEERS SURVEYORS
	Subbasii	n Data		Overla	nd (Initial) Fl	ow Time		Chann	elized (Travel) F	low Time			Time of (	Concentration	
Basin	Area	% Impervious	C5	Overland Flow Length L <sub>i</sub> (ft)	Overland Flow Slope S <sub>i</sub> (ft/ft)	Overland Flow Time t <sub>i</sub> (min)	Channelized Flow Length L <sub>t</sub> (ft)	$ \begin{array}{c c} \mbox{annelized} \\ \mbox{w Length} \\ \mbox{L}_t(ft) \\ \mbox{S}_t(ft/ft) \\ \mbox{S}_t(ft/ft) \\ \mbox{Flow Slope} \\ \mbox{S}_t(ft/ft) \\ \mbox{Flow Slope} \\ \mbox{Flow Velocity} \\ \mbox{Flow Velocity} \\ \mbox{V}_t(ft/sec) \\ \mbox{V}_t(ft/sec) \\ \mbox{V}_t(ft/sec) \\ \mbox{Flow Velocity} \\ \mbox{Flow Velocity} \\ \mbox{V}_t(ft/sec) \\ \mbox$			Channelized Flow Time t <sub>t</sub> (min)	Computed t <sub>c</sub> (min)	Regional t <sub>c</sub> (min)	Selected t <sub>c</sub> (min)	Remarks
А	81.00	71.4%	0.45	36.00	0.020	5.64	2705.00	0.005	20	1.41	31.88	37.51	47.43	37.51	
В	106.00	72.7%	0.52	36.00	0.020	5.03	2900.00	0.005	15	1.06	45.57	50.60	49.30	49.30	
D	110.00	69.0%	0.50	36.00	0.020	5.19	1358.00	0.005	15	1.06	21.34	26.53	31.44	26.53	
E	73.00	74.7%	0.57	36.00	0.020	4.59	1500.00	0.005	15	1.06	23.57	28.16	31.46	28.16	
F	75.00	73.6%	0.55	36.00	0.020	4.71	3000.00	0.005	15	1.06	47.14	51.85	50.10	50.10	
G	160.00	70.1%	0.51	36.00	0.020	5.07	2100.00	0.005	15	1.06	33.00	38.07	40.38	38.07	
Channel G	64.40	73.5%	0.55	300.00	0.020	13.63	3200.00	0.005	20	1.41	37.71	51.34	52.59	51.34	
Channel F	24.00	65.0%	0.45	300.00	0.010	20.33	1680.00	0.005	20	1.41	19.80	40.13	36.83	36.83	
Channel A	11.60	95.0%	0.81	300.00	0.010	9.07	1800.00	0.010	20	2.00	15.00	24.07	23.30	23.30	
Culvert 4	7.80	95.0%	0.81	300.00	0.010	9.07	617.00	0.005	20	1.41	7.27	16.34	16.37	16.34	
Culvert 5	36.50	76.9%	0.59	300.00	0.010	15.85	2200.00	0.005	20	1.41	25.93	41.78	39.15	39.15	
Culvert 6	64.40	71.8%	0.53	300.00	0.010	17.79	2200.00	0.005	20	1.41	25.93	43.72	41.03	41.03	
Culvert 7	15.70	65.0%	0.45	300.00	0.010	20.33	1200.00	0.005	20	1.41	14.14	34.47	30.58	30.58	
Culvert 8	19.70	65.0%	0.45	300.00	0.010	20.33	2000.00	0.005	20	1.41	23.57	43.90	40.99	40.99	

Designer: Company: Date: Project:	LAO R&R Engineers-Surveys 6/29/2023 MAYBERRY SKETCH PL	Drs					Cells	of this colo	r are for re	quired use	r-input				20									RER
Location:	EL PASO COUNTY, COL	ORADO				1	Cells	of this colo	r are for op	tional use	r-input	1,	e -1,50 la	i(D) + 7.58	3									ENGINEERS SURVEYORS
	STREET /			DIR	ECT RUNO	FF				T	OTAL RUNC	)FF			STREET	BYPASS			PIPE		1	RAVEL TIN	AE .	
DESGIN	CONTRIBUTING	Basin Name	Area	Coeff	Тс	C*A	- 1	Q	Тс	Sum	Sum C*A	-	Q	Street Q	Street	Length	Street Tt	Design Q	Slope	PIPE	L	VEL	Tt	Remarks
	BASINS		(ac)	с	(min)	(ac)		(cfs)	(min)	(ac)	(ac)	in/hr	cfs	cfs	%	ft	min	cfs	%	SIZE	ft	ft/sec	min	
		A	81	0.45	37.5	36.13	2.15	77.5										77.5						
1				0.50	10.0	54.70	4.74	05.4																
2		в	106	0.52	49.5	54.76	1.74	95.1										95.1						
-		D	110	0.50	26.5	54.72	2.67	145.9										145.9						
3																								
		E	73	0.57	28.2	41.39	2.58	106.6										106.6						
4				0.55		44.53	4.74	74.4																
5		F	75	0.55	50.1	41.53	1./1	/1.1										/1.1						
,		6	160	0.51	38.1	81.83	2.12	173.8										173.8						
6																								
		Channel G	64.4	0.55	51.3	35.57	1.68	59.6										59.6						
		Channel F	24	0.45	36.8	10.80	2.1/	23.5										23.5						
		Channel A	11.6	0.81	23.3	9.40	2.86	26.9										26.9						
						0.10																		
		Culvert 4	7.8	0.81	16.3	6.32	3.39	21.4										21.4						
		Culvert 5	36.5	0.59	39.2	21.65	2.08	45.1										45.1						
		Culvert 6	64.4	0.53	41.0	34.20	2.01	68.8										68.8						
		amarto	21.4	2.35	.1.0	220		23.0										23.0						
		Culvert 7	15.7	0.45	30.6	7.07	2.45	17.3										17.3						
		Culvert 8	19.7	0.45	41.0	8.87	2.01	17.8		_								17.8						
					1																			

#### STORM DRAINAGE SYSTEM DESIGN - 5-YEAR DESIGN STORM

Designer: Company: Date: Project: Location:	LAO R&R Engineers-Survey 6/29/2023 MAYBERRY SKETCH PL EL PASO COUNTY, COL	AN ORADO					Cells Cells	of this cold	or are for re	quired use	er-input er-input	I <sub>100</sub> =	-2.52 In(I	0) + 12.73:	5									ENGINEERS SURVEYORS
	STREET/			DIR	ECT RUNC	DFF				т	OTAL RUN	OFF			STREET	BYPASS			PIPE		Т	RAVEL TIN	1E	
POINT	CONTRIBUTING	Basin Name	Area	Coeff	Tc (min)	C*A	1	Q (cfs)	Tc (min)	Sum Area	Sum C*A	l in/hr	Q	Street Q	Street Slope	Length ft	Street Tt	Design Q	Slope %	PIPE	L ft	VEL ft/sec	Tt	Remarks
	ļ	А	81	0.48	37.5	39.25	3.60	141.3	()	(30)	(ac)	/10	- 15	cis	78			141.3	~	SILL		ity set		
1																								
		В	106	0.63	49.3	67.06	2.91	195.3										195.3						
2																								
		D	110	0.63	26.5	69.11	4.47	309.1										309.1						
3																								
		E	73	0.68	28.2	49.95	4.32	215.9										215.9						
4		F	75	0.67	50.1	50.51	2.87	145.1										145.1						
5			13	0.07	50.1	50.51	2.07	140.1			1							140.1						
,		G	160	0.64	38.1	102.32	3.56	364.6										364.6						
6																								
		Channel G	64.4	0.67	51.3	43.30	2.81	121.7										121.7						
		Channel F	24	0.59	36.8	14.16	3.65	51.6			1							51.6						
				0.00		40.24	4.00	40.0																
		Channel A	11.6	0.88	23.3	10.21	4.80	49.0										49.0						
		Culvert 4	7.8	0.88	16.3	6.86	5.70	39.1			-							39.1						
		CUIVEIL4	7.0	0.00	10.5	0.00	5.70	33.1										33.1						
		Culvert 5	36.5	0.71	39.2	25.74	3.49	89.9										89.9						
			1			1			1															
		Culvert 6	64.4	0.66	41.0	42.20	3.38	142.4										142.4						
		Culvert 7	15.7	0.59	30.6	9.26	4.12	38.1			1							38.1						
		Culvert 8	19.7	0.59	41.0	11.62	3.38	39.3	<u> </u>									39.3						
		1	L	1	L	1		1						1										

#### STORM DRAINAGE SYSTEM DESIGN - 100-YEAR DESIGN STORM

MAYBERRY COMMUNITIES MASTER DEVELOPMENT DRAINAGE PLAN

# APPENDIX C – HYDRAULIC CALCULATIONS C.1 DETENTION VOLUMES

- 17 -

Depth Increment =

Stage - Storage Description

1.19

1.50

1.75

2.00

2.52

3.14 inch Stage (ft)

#### Project: MAYBERRY SKETCH PLAN Basin ID: POND A (Stage 0 = 6057)

	ZONE 3	
100-YR	1 Cover 1	
TOCOMET BORN T MOCH		
	ZONE 1 AND 2 ORIFICE	
POOL	Example Zone Configuration (Retention Pond)	

Watershed Information

leisneu miornauon		
Selected BMP Type =	EDB	
Watershed Area =	81.00	acres
Watershed Length =	2,784	ft
Watershed Length to Centroid =	1,392	ft
Watershed Slope =	0.010	ft/ft
Watershed Imperviousness =	72.00%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

# After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded colorado orbannyard	graphinoceae	
Water Quality Capture Volume (WQCV) =	1.919	acre-feet
Excess Urban Runoff Volume (EURV) =	7.447	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	5.451	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	7.108	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	8.438	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	10.083	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	11.692	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	13.606	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	17.814	acre-feet
Approximate 2-yr Detention Volume =	4.867	acre-feet
Approximate 5-yr Detention Volume =	6.346	acre-feet
Approximate 10-yr Detention Volume =	7.613	acre-feet
Approximate 25-yr Detention Volume =	9.101	acre-feet
Approximate 50-yr Detention Volume =	9.985	acre-feet
Approximate 100-yr Detention Volume =	10.851	acre-feet

#### Define Zones and Basin Geometry

1.919 acre-feet	Zone 1 Volume (WQCV) =
5.528 acre-feet	Zone 2 Volume (EURV - Zone 1) =
4.364 acre-feet	Zone 3 (100yr + 1 / 2 WQCV - Zones 1 & 2) =
11.811 acre-feet	Total Detention Basin Volume =
user ft <sup>3</sup>	Initial Surcharge Volume (ISV) =
user ft	Initial Surcharge Depth (ISD) =
user ft	Total Available Detention Depth (H <sub>total</sub> ) =
user ft	Depth of Trickle Channel (H <sub>TC</sub> ) =
user ft/ft	Slope of Trickle Channel (S <sub>TC</sub> ) =
user H:V	Slopes of Main Basin Sides (Smain) =
user	Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =

Initial Surcharge Area (A <sub>ISV</sub> ) =	user	ft <sup>2</sup>
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor (A <sub>FLOOR</sub> ) =	user	ft <sup>2</sup>
Volume of Basin Floor (V <sub>FLOOR</sub> ) =	user	ft <sup>3</sup>
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin ( $W_{MAIN}$ ) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft <sup>2</sup>
Volume of Main Basin (V <sub>MAIN</sub> ) =	user	ft <sup>3</sup>
Calculated Total Basin Volume (Vtotal) =	user	acre-feet

		Top of Micropool		0.00				7,906	0.181		
		6058		1.00				31 540	0 774	19 777	0.453
		0050	-	1.00	-	-	-	51,545	0.724	13,121	0.133
		6059		2.00				65,600	1.506	68,302	1.568
		6060		3.00				85,864	1.971	144,034	3.307
		6061		4.00				95 845	2 200	734 999	5 302
		0001		4.00			-	93,843	2.200	234,000	3.392
		6062		5.00				101,259	2.325	333,440	/.655
		6063		6.00				106,891	2.454	437,515	10.044
		6064		7,00				112.752	2,588	547,337	12,565
		6007		0.00				110.040	2.000	CC1 (22)	15 222
		6065		8.00				118,840	2.728	003,133	15.223
		6066		9.00				125,155	2.873	785,130	18.024
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					-						
ional User	Overrides										
	acre-reet						-				
	acre-feet		-		-		-				
1.19	inches										
1.50	inches										
1.75	in ches										
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Width (ft)

Length (ft)

tage (ft

Area (ft<sup>2</sup>)

Area (acre)

Volume (ft<sup>3</sup>)

Volume (ac-ft)

MHFD-Detention, Version 4.06 (July 2022)





ZONE 1 AND 2 ORIFICES

Depth Increment = 100-YEAR Example Zone Configuration (Retention Pond)

### Watershed Information

PERMA

Selected BMP Type =	EDB	
Watershed Area =	106.00	acres
Watershed Length =	2,700	ft
Watershed Length to Centroid =	1,350	ft
Watershed Slope =	0.010	ft/ft
Watershed Imperviousness =	73.00%	percen
Percentage Hydrologic Soil Group A =	100.0%	percen
Percentage Hydrologic Soil Group B =	0.0%	percen
Percentage Hydrologic Soil Groups C/D =	0.0%	percen
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

# After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

	2	
Water Quality Capture Volume (WQCV) =	2.555	acre-feet
Excess Urban Runoff Volume (EURV) =	9.919	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	7.278	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	9.483	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	11.247	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	13.420	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	15.544	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	18.063	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	23.605	acre-feet
Approximate 2-yr Detention Volume =	6.486	acre-feet
Approximate 5-yr Detention Volume =	8.454	acre-feet
Approximate 10-yr Detention Volume =	10.136	acre-feet
Approximate 25-yr Detention Volume =	12.107	acre-feet
Approximate 50-yr Detention Volume =	13.275	acre-feet
Approximate 100-yr Detention Volume =	14.411	acre-feet

Define Zones	and	Basin	Geom	etry
	ź	Zone 1	Volume	e (WQ

Zone 1 Volume (WQCV) =	2.555	acre-feet
Zone 2 Volume (EURV - Zone 1) =	7.364	acre-feet
Zone 3 (100yr + 1 / 2 WQCV - Zones 1 & 2) =	5.770	acre-feet
Total Detention Basin Volume =	15.689	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H <sub>total</sub> ) =	user	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	user	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	user	1
		•

Initial Surcharge Area $(A_{ISV}) =$	user	ft <sup>2</sup>
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor (A <sub>FLOOR</sub> ) =	user	ft <sup>2</sup>
Volume of Basin Floor ( $V_{FLOOR}$ ) =	user	ft <sup>3</sup>
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin (W <sub>MAIN</sub> ) =	user	ft
Area of Main Basin (A <sub>MAIN</sub> ) =	user	ft <sup>2</sup>
Volume of Main Pasin (V) =	usor	A 3

Volume of Main Basin (V<sub>MAIN</sub>) = user ft <sup>3</sup> Calculated Total Basin Volume (V<sub>total</sub>) = **user** acre-feet

				Ontional				Ontional			
ion Pond)		Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
ionii onia,		Description	(ft)	Stage (ft)	(ft)	(ft)	(ft <sup>2</sup> )	Area (ft <sup>2</sup> )	(acre)	(ft 3)	(ac-ft)
		Top of Micropool		0.00	-			6,967	0.160		
		6041		1.00				27 989	0.643	17 478	0.401
		60.12		2.00				27,505	4.450	62.055	0.101
		6042		2.00	-		-	63,165	1.450	63,055	1.448
		6043		3.00	-		-	106,519	2.445	147,897	3.395
		6044		4.00	-			138,250	3.174	270,281	6.205
		6045		5.00	-			156,165	3.585	417,489	9.584
		6046		6.00			-	169,255	3.886	580,199	13.320
		6047		7.00	-			170 055	4 131	754 804	17 328
		6049		7.00				100.074	4.350	020 710	21.520
		0040		8.00	-		-	109,074	4.359	939,/18	21.573
					-		-				
					-		-				
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	acre-leet				-		-				
	acre-feet				-		-				
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1.50	inches				-						
1.75	inches										
2.00	inches				-		-				
2.25	inches										
2.52	inches				-		-				
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MHFD-Detention, Version 4.06 (July 2022)



Depth Increment :

Stage - Storage Stage

Option Overri

ride

Length

Width

Area Override Area

Volume Volume

Project: Mayberry Filing 3 Basin ID: Pond D



Watershed Information

cres
t
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t/ft
percent
ercent
percent
ercent
nours

# After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded colorado orban nyard	graphinoccu	iic.
Water Quality Capture Volume (WQCV) =	2.480	acre-fee
Excess Urban Runoff Volume (EURV) =	9.577	acre-fee
2-yr Runoff Volume (P1 = 1.19 in.) =	7.035	acre-fee
5-yr Runoff Volume (P1 = 1.5 in.) =	9.194	acre-fee
10-yr Runoff Volume (P1 = 1.75 in.) =	10.931	acre-fee
25-yr Runoff Volume (P1 = 2 in.) =	13.128	acre-fee
50-yr Runoff Volume (P1 = 2.25 in.) =	15.280	acre-fee
100-yr Runoff Volume (P1 = 2.52 in.) =	17.863	acre-fee
500-yr Runoff Volume (P1 = 3.14 in.) =	23.531	acre-fee
Approximate 2-yr Detention Volume =	6.247	acre-fee
Approximate 5-yr Detention Volume =	8.155	acre-fee
Approximate 10-yr Detention Volume =	9.802	acre-fee
Approximate 25-yr Detention Volume =	11.750	acre-fee
Approximate 50-yr Detention Volume =	12.913	acre-fee
Approximate 100-yr Detention Volume =	14.083	acre-fee

#### Define Zones and Basin Geometry

acre-feet	2.480	Zone 1 Volume (WQCV) =
acre-feet	7.097	Zone 2 Volume (EURV - Zone 1) =
acre-feet	5.746	Zone 3 (100yr + 1 / 2 WQCV - Zones 1 & 2) =
acre-feet	15.324	Total Detention Basin Volume =
ft <sup>3</sup>	user	Initial Surcharge Volume (ISV) =
ft	user	Initial Surcharge Depth (ISD) =
ft	user	Total Available Detention Depth (H <sub>total</sub> ) =
ft	user	Depth of Trickle Channel (H <sub>TC</sub> ) =
ft/ft	user	Slope of Trickle Channel (S <sub>TC</sub> ) =
H:V	user	Slopes of Main Basin Sides (Smain) =
	user	Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =

Initial Surcharge Area (A <sub>ISV</sub> ) =	user	ft ²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width (W <sub>ISV</sub> ) =	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor (A <sub>FLOOR</sub> ) =	user	ft <sup>2</sup>
Volume of Basin Floor (V <sub>FLOOR</sub> ) =	user	ft <sup>3</sup>
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin ( $W_{MAIN}$ ) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft <sup>2</sup>
Volume of Main Basin ( $V_{MAIN}$ ) =	user	ft <sup>3</sup>
Calculated Total Basin Volume (Vtotal) =	user	acı

re-feet

		Description	(ft)	Stage (ft)	(ft)	(ft)	(ft <sup>2</sup> )	Area (ft <sup>2</sup> )	(acre)	(ft 3)	(ac-ft)
		Top of Micropool		0.00				38	0.001		
		6076		0.20				1 967	0.042	206	0.007
		6026		0.30	-		-	1,007	0.045	200	0.007
		6026.2		0.50				4,584	0.105	931	0.021
		6026.5		0.80				10.635	0,244	3.213	0,074
			-	0.00			-	20,000	0.671	42.00	0.0/7
		6027		1.30				26,196	0.601	12,421	0.285
		6027.5		1.80				47,640	1.094	30,880	0.709
		6028		2 30				63 718	1 463	58 719	1 348
				2.50				05,710	1.105	50,715	1.510
		6028.5		2.80				//,666	1.783	94,065	2.159
		6029		3.30				90,791	2.084	136,180	3.126
		6020 E		2 90				101 440	2 220	104 327	4 220
		0029.5		3.00				101,440	2.329	104,237	4.230
		6030		4.30				108,842	2.499	236,808	5.436
		6030 5		4.80	_			113 378	2 603	202 363	6 712
		0030.3		4.00				115,570	2.005	252,505	0.712
		6031		5.30				117,742	2.703	350,143	8.038
		6031.5		5.80				122,145	2.804	410.115	9.415
and the second states		6022		6.20				100 500	3.000	472,200	10.042
ptional User	r Overrides	6032		6.30	-			126,588	2.906	472,298	10.842
	acre-feet	6032.5		6.80				131,071	3.009	536,713	12.321
	acro-foot	6033		7 30	-			135 710	3 115	603 408	13.852
	acresieer	0033		7.30	-			155,710	3.113	003,408	13.832
1.19	inches	6033.5		8.80	-			141,840	3.256	811,570	18.631
1.50	inches										
1 75	inches										
1.75	litutes				-						
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3.14	inches										
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MHFD-Detention, Version 4.06 (July 2022)



Depth Increment =

1.19

1.50

1.75

2.00

2.52

3.14

Opt Ove

#### Project: Mayberry Sketch Plan Basin ID: Pond E

	20NE 3 /20NE 2
T rout Mach	IOUYEAR
PERMANEN	ZONE 1 AND 2 ORIFICE
POOL	Example Zone Configuration (Retention Pond)

Water

tershed Information		
Selected BMP Type =	EDB	
Watershed Area =	73.00	acres
Watershed Length =	2,800	ft
Watershed Length to Centroid =	1,400	ft
Watershed Slope =	0.040	ft/ft
Watershed Imperviousness =	75.00%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

# After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded colorado orbannyare	graphinocea	un en
Water Quality Capture Volume (WQCV) =	1.822	acre-feet
Excess Urban Runoff Volume (EURV) =	7.072	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	5.124	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	6.666	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	7.901	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	9.395	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	10.854	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	12.577	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	16.373	acre-feet
Approximate 2-yr Detention Volume =	4.630	acre-feet
Approximate 5-yr Detention Volume =	6.030	acre-feet
Approximate 10-yr Detention Volume =	7.220	acre-feet
Approximate 25-yr Detention Volume =	8.610	acre-feet
Approximate 50-yr Detention Volume =	9.430	acre-feet
Approximate 100-yr Detention Volume =	10.216	acre-feet

#### Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	1.822	acre-feet
Zone 2 Volume (EURV - Zone 1) =	5.250	acre-feet
Zone 3 (100yr + 1 / 2 WQCV - Zones 1 & 2) =	4.056	acre-feet
Total Detention Basin Volume =	11.128	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (Htotal) =	user	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	user	ft
Slope of Trickle Channel (STC) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	user	
		-

Initial Surcharge Area (A <sub>ISV</sub> ) =	user	ft <sup>2</sup>
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor (A <sub>FLOOR</sub> ) =	user	ft <sup>2</sup>
Volume of Basin Floor (V <sub>FLOOR</sub> ) =	user	ft <sup>3</sup>
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin ( $W_{MAIN}$ ) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft²
Volume of Main Basin ( $V_{MAIN}$ ) =	user	ft <sup>3</sup>
Calculated Total Basin Volume (Vtotal) =	user	acre-feet
		-

				Optional				Optional			
ond)		Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
		Description	(ft)	Stage (ft)	(ft)	(ft)	(ft²)	Area (ft *)	(acre)	(ft 3)	(ac-ft)
		Top of Micropool		0.00				16	0.000		
		6019		0.80				4 460	0 102	1 700	0.041
		0015		0.00				-1,-100	0.102	1,750	0.041
		6020		1.80				18,435	0.423	13,238	0.304
		6021		2.80				38 284	0.879	41 597	0.955
				2.00				50/201	0.075	12,557	0.555
		6022		3.80				57,822	1.327	89,650	2.058
		6023		4.80				75,326	1.729	156,224	3.586
		6024		5.80				90.171	2.070	238.973	5.486
		6025		6.00				00,200	2 212	222.242	7 ( ) 7
		0025		0.00				90,309	2.212	332,243	7.627
		6026		7.80				98,485	2.261	429,670	9.864
		6027		8.80				103,229	2.370	530,527	12.179
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MHFD-Detention, Version 4.06 (July 2022)



Depth Increment

nal User O ad ac 1.19

1.50

1.75 2.00 2.25

2.52

3.14 in

#### Project: Mayberry Sketch Plan Basin ID: Pond F



od Info .... Waters

tersned Information		
Selected BMP Type =	EDB	
Watershed Area =	75.00	acres
Watershed Length =	2,785	ft
Watershed Length to Centroid =	1,393	ft
Watershed Slope =	0.010	ft/ft
Watershed Imperviousness =	74.00%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

# After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

olume (WQCV) = 1.839 acre-feet	Water Quality Capture Volume (
/olume (EURV) = 7.142 acre-feet	Excess Urban Runoff Volume (
(P1 = 1.19 in.) = 5.210 acre-fee	2-yr Runoff Volume (P1 = 1
e (P1 = 1.5 in.) = 6.783 acre-fee	5-yr Runoff Volume (P1 =
(P1 = 1.75 in.) = 8.047 acre-fee	10-yr Runoff Volume (P1 = 1
me (P1 = 2 in.) = 9.588 acre-fee	25-yr Runoff Volume (P1 =
(P1 = 2.25 in.) = 11.093 acre-fee	50-yr Runoff Volume (P1 = 2
(P1 = 2.52 in.) = 12.873 acre-fee	100-yr Runoff Volume (P1 = 2
(P1 = 3.14 in.) = 16.793 acre-fee	500-yr Runoff Volume (P1 = 3
tention Volume = 4.673 acre-fee	Approximate 2-yr Detention \
tention Volume = 6.088 acre-fee	Approximate 5-yr Detention \
tention Volume = 7.294 acre-fee	Approximate 10-yr Detention
tention Volume = 8.706 acre-fee	Approximate 25-yr Detention \
tention Volume = 9.540 acre-fee	Approximate 50-yr Detention \
tention Volume = 10.346 acre-fee	Approximate 100-vr Detention V

#### Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	1.839	acre-feet
Zone 2 Volume (EURV - Zone 1) =	5.302	acre-feet
Zone 3 (100yr + 1 / 2 WQCV - Zones 1 & 2) =	4.124	acre-feet
Total Detention Basin Volume =	11.266	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (Htotal) =	user	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	user	ft
Slope of Trickle Channel (STC) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	user	
		-

Initial Surcharge Area $(A_{ISV}) =$	user	ft <sup>2</sup>
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor (W <sub>FLOOR</sub> ) =	user	ft
Area of Basin Floor (A <sub>FLOOR</sub> ) =	user	ft <sup>2</sup>
Volume of Basin Floor (V <sub>FLOOR</sub> ) =	user	ft <sup>3</sup>
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin ( $W_{MAIN}$ ) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft <sup>2</sup>
Volume of Main Basin ( $V_{MAIN}$ ) =	user	ft <sup>3</sup>
Calculated Total Basin Volume ( $V_{total}$ ) =	user	acre-feet

	Stage - Storage	Stage	Optional Override	Length	Width	Area	Override	Area	Volume	Volume
	Description	(ft)	Stage (ft)	(ft)	(ft)	(ft²)	Area (ft <sup>2</sup> )	(acre)	(ft 3)	(ac-ft)
	6049		0.40				1.745	0.040	359	0.008
	6050		1.40				16.626	0.382	9,544	0.219
	6051		2.40				35,675	0.819	35,694	0.819
	6052		3.40				52,181	1.198	79,622	1.828
	6053		4.40	-			66,143	1.518	138,784	3.186
	6054		5.40				77,732	1.784	210,722	4.838
	6055		6.40 7.40				88,692	2.036	293,934	6./48 8.908
	6057		8.40	-			110.114	2.528	492,824	11.314
	6058		9.40				120,573	2.768	608,167	13.962
	6058.5		9.90	-		-	125,740	2.887	669,746	15.375
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MHFD-Detention, Version 4.06 (July 2022)



Depth Increment =

Stage - Storage

1.19 1.50

1.75

2.00

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3.14 inche Optio Overr

ride

Width

Length

Area

Override

Area

Volume Volume

Stage

Project: Mayberry Sketch Plan Basin ID: Pond G

ZONE 3 ZONE 2 ZONE 1 ORIFICE

ZONE 1 AND 2 PERM Example Zone Configuration (Retention Pond)

### Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	160.00	acres
Watershed Length =	3,625	ft
Watershed Length to Centroid =	1,822	ft
Watershed Slope =	0.010	ft/ft
Watershed Imperviousness =	70.00%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

# After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded colorado orban nyard	graphinoccu	iic.
Water Quality Capture Volume (WQCV) =	3.667	acre-fee
Excess Urban Runoff Volume (EURV) =	14.190	acre-fee
2-yr Runoff Volume (P1 = 1.19 in.) =	10.426	acre-fee
5-yr Runoff Volume (P1 = 1.5 in.) =	13.616	acre-fee
10-yr Runoff Volume (P1 = 1.75 in.) =	16.175	acre-fee
25-yr Runoff Volume (P1 = 2 in.) =	19.390	acre-fee
50-yr Runoff Volume (P1 = 2.25 in.) =	22.536	acre-fee
100-yr Runoff Volume (P1 = 2.52 in.) =	26.302	acre-fee
500-yr Runoff Volume (P1 = 3.14 in.) =	34.568	acre-fee
Approximate 2-yr Detention Volume =	9.261	acre-fee
Approximate 5-yr Detention Volume =	12.085	acre-fee
Approximate 10-yr Detention Volume =	14.516	acre-fee
Approximate 25-yr Detention Volume =	17.386	acre-fee
Approximate 50-yr Detention Volume =	19.095	acre-fee
Approximate 100-yr Detention Volume =	20.801	acre-fee

#### Define Zones and Basin Geometry

Zone 1 Volume (WQCV) =	3.667	acre-feet
Zone 2 Volume (EURV - Zone 1) =	10.523	acre-feet
Zone 3 (100yr + 1 / 2 WQCV - Zones 1 & 2) =	8.445	acre-feet
Total Detention Basin Volume =	22.634	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H <sub>total</sub> ) =	user	ft
Depth of Trickle Channel (H <sub>TC</sub> ) =	user	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =	user	

Initial Surcharge Area (A <sub>ISV</sub> ) =	user	ft <sup>2</sup>
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor (A <sub>FLOOR</sub> ) =	user	ft <sup>2</sup>
Volume of Basin Floor (V <sub>FLOOR</sub> ) =	user	ft <sup>3</sup>
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin ( $W_{MAIN}$ ) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft <sup>2</sup>
Volume of Main Basin (V <sub>MAIN</sub> ) =	user	ft <sup>3</sup>
Calculated Total Basin Volume (Vtotal) =	user	acre-feet

		Top of Micropool	(10)	0.00	(10)	(10)	(10)	470	0.011	(10)	(ac-it)
				0.00				970	0.011	4.024	0.444
		6026		1.00	-			9,193	U.211	4,831	0.111
		6027		2.00	-		-	47,523	1.091	33,189	0.762
		6028		3.00	-			105,030	2.411	109,465	2.513
		6029		4.00	-			167,485	3.845	245,723	5.641
		6030		5.00				220,930	5.072	439,930	10.099
		6031		6.00	-		-	255,650	5.869	678,220	15.570
		6032		7.00				277,365	6.367	944,728	21.688
		6033		8.00				300,965	6.909	1,233.893	28.326
		6034		9,00				332,445	7,632	1,550,598	35,597
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MHFD-Detention, Version 4.06 (July 2022)



MAYBERRY COMMUNITIES MASTER DEVELOPMENT DRAINAGE PLAN

# APPENDIX C – HYDRAULIC CALCULATIONS C.2 OPEN CHANNELS

- 18 -

# **Channel Report**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, May 2 2023

# Channel A - 5 YEAR

## Trapezoidal

Trapezoidal		Highlighted	
Bottom Width (ft)	= 8.00	Depth (ft) =	0.84
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs) =	26.90
Total Depth (ft)	= 2.50	Area (sqft) =	9.54
Invert Elev (ft)	= 1.00	Velocity (ft/s) =	2.82
Slope (%)	= 0.60	Wetted Perim (ft) =	14.93
N-Value	= 0.030	Crit Depth, Yc (ft) =	0.64
		Top Width (ft) =	14.72
Calculations		EGL (ft) =	0.96
Compute by:	Known Q		
Known Q (cfs)	= 26.90		



Reach (ft)

# **Channel Report**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, May 2 2023

# Channel A - 100 YEAR

## Trapezoidal

Trapezoidal		Highlighted	
Bottom Width (ft)	= 8.00	Depth (ft)	= 1.15
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs)	= 49.00
Total Depth (ft)	= 2.50	Area (sqft)	= 14.49
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 3.38
Slope (%)	= 0.60	Wetted Perim (ft)	= 17.48
N-Value	= 0.030	Crit Depth, Yc (ft)	= 0.90
		Top Width (ft)	= 17.20
Calculations		EGL (ft)	= 1.33
Compute by:	Known Q		
Known Q (cfs)	= 49.00		



Reach (ft)

# **Channel Report**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

# Channel B (Offsite) - 5 YEAR

# Trapezoidal

Trapezoidal		Highlighted	
Bottom Width (ft)	= 8.00	Depth (ft) =	0.80
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs) =	24.41
Total Depth (ft)	= 3.50	Area (sqft) =	8.96
Invert Elev (ft)	= 1.00	Velocity (ft/s) =	2.72
Slope (%)	= 0.60	Wetted Perim (ft) =	14.60
N-Value	= 0.030	Crit Depth, Yc (ft) =	0.60
		Top Width (ft) =	14.40
Calculations		EGL (ft) =	0.92
Compute by:	Known Q		
Known Q (cfs)	= 24.41		



Reach (ft)
Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, May 1 2023

## Channel B (Offsite) - 100 YEAR

#### Trapezoidal

Trapezoidal		Highlighted	
Bottom Width (ft)	= 8.00	Depth (ft)	= 2.02
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs)	= 149.50
Total Depth (ft)	= 3.50	Area (sqft)	= 32.48
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 4.60
Slope (%)	= 0.60	Wetted Perim (ft)	= 24.66
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.68
		Top Width (ft)	= 24.16
Calculations		EGL (ft)	= 2.35
Compute by:	Known Q		
Known Q (cfs)	= 149.50		



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

#### **Channel D - 5 YEAR FLOW**

#### Trapezoidal

Trapezoidal		Highlighted	
Bottom Width (ft)	= 8.00	Depth (ft) =	1.39
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs) =	57.50
Total Depth (ft)	= 4.00	Area (sqft) =	18.85
Invert Elev (ft)	= 1.00	Velocity (ft/s) =	3.05
Slope (%)	= 0.40	Wetted Perim (ft) =	19.46
N-Value	= 0.030	Crit Depth, Yc (ft) =	0.99
		Top Width (ft) =	19.12
Calculations		EGL (ft) =	1.53
Compute by:	Known Q		
Known Q (cfs)	= 57.50		



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, May 1 2023

## Channel D - 100 YEAR

#### Trapezoidal

Trapezoidal		Highlighted	
Bottom Width (ft)	= 8.00	Depth (ft)	= 2.02
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs)	= 121.60
Total Depth (ft)	= 4.00	Area (sqft)	= 32.48
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 3.74
Slope (%)	= 0.40	Wetted Perim (ft)	= 24.66
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.50
		Top Width (ft)	= 24.16
Calculations		EGL (ft)	= 2.24
Compute by:	Known Q		
Known Q (cfs)	= 121.60		



Monday, May 1 2023

#### Channel E (Offsite & Pond D) - 5 YEAR

#### Trapezoidal

Bottom Width (ft)	= 8.00	Depth (ft)	= 0.69
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs)	= 18.70
Total Depth (ft)	= 3.50	Area (sqft)	= 7.42
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 2.52
Slope (%)	= 0.60	Wetted Perim (ft)	= 13.69
N-Value	= 0.030	Crit Depth, Yc (ft)	= 0.51
		Top Width (ft)	= 13.52
Calculations		EGL (ft)	= 0.79
Compute by:	Known Q		
Known Q (cfs)	= 18.70		

Highlighted



Monday, May 1 2023

#### Channel E (Offsite & Pond D) - 100 YEAR

= 8.00
= 4.00, 4.00
= 3.50
= 1.00

= 3.50 = 1.00 = 0.60 = 0.030

#### Calculations

Slope (%)

N-Value

Compute by:	Known Q
Known Q (cfs)	= 177.50

Highlighted	
Depth (ft)	
Q (cfs)	
Area (sqft)	

EGL (ft)

Area (sqft)	=	36.96
Velocity (ft/s)	=	4.80
Wetted Perim (ft)	=	26.14
Crit Depth, Yc (ft)	=	1.84
Top Width (ft)	=	25.60
EGL (ft)	=	2.56

= 2.20

= 177.50



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, May 2 2023

#### **Channel F - 5 YEAR**

#### Trapezoidal

Trapezoidal		Highlighted	
Bottom Width (ft)	= 8.00	Depth (ft) =	0.82
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs) =	23.50
Total Depth (ft)	= 2.50	Area (sqft) =	9.25
Invert Elev (ft)	= 1.00	Velocity (ft/s) =	2.54
Slope (%)	= 0.50	Wetted Perim (ft) =	14.76
N-Value	= 0.030	Crit Depth, Yc (ft) =	0.59
		Top Width (ft) =	14.56
Calculations		EGL (ft) =	0.92
Compute by:	Known Q		
Known Q (cfs)	= 23.50		



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, May 2 2023

## Channel F - 100 YEAR

#### Trapezoidal

Trapezoidal		Highlighted	
Bottom Width (ft)	= 8.00	Depth (ft)	= 1.24
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs)	= 51.60
Total Depth (ft)	= 2.50	Area (sqft)	= 16.07
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 3.21
Slope (%)	= 0.50	Wetted Perim (ft)	= 18.23
N-Value	= 0.030	Crit Depth, Yc (ft)	= 0.93
		Top Width (ft)	= 17.92
Calculations		EGL (ft)	= 1.40
Compute by:	Known Q		
Known Q (cfs)	= 51.60		



Reach (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, May 2 2023

## Channel G - 5 YEAR

#### Trapezoidal

Trapezoidal		Highlighted	
Bottom Width (ft)	= 8.00	Depth (ft) =	1.28
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs) =	59.60
Total Depth (ft)	= 3.00	Area (sqft) =	16.79
Invert Elev (ft)	= 1.00	Velocity (ft/s) =	3.55
Slope (%)	= 0.60	Wetted Perim (ft) =	18.56
N-Value	= 0.030	Crit Depth, Yc (ft) =	1.01
		Top Width (ft) =	18.24
Calculations		EGL (ft) =	1.48
Compute by:	Known Q		
Known Q (cfs)	= 59.60		



Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, May 2 2023

## Channel G - 100 YEAR

#### Trapezoidal

Trapezoidal		Highlighted	
Bottom Width (ft)	= 8.00	Depth (ft)	= 1.83
Side Slopes (z:1)	= 4.00, 4.00	Q (cfs)	= 121.70
Total Depth (ft)	= 3.00	Area (sqft)	= 28.04
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 4.34
Slope (%)	= 0.60	Wetted Perim (ft)	= 23.09
N-Value	= 0.030	Crit Depth, Yc (ft)	= 1.50
		Top Width (ft)	= 22.64
Calculations		EGL (ft)	= 2.12
Compute by:	Known Q		
Known Q (cfs)	= 121.70		





Figure 9-37. Low tailwater riprap basin

MAYBERRY COMMUNITIES MASTER DEVELOPMENT DRAINAGE PLAN

## APPENDIX C – HYDRAULIC CALCULATIONS C.3 CULVERT SIZING

- 19 -

# **Culvert Report**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, May 2 2023

## **CULVERT 1 - OFFSITE F1**

Invert Elev Dn (ft)	= 6040.70	Calculations	
Pipe Length (ft)	= 140.00	Qmin (cfs)	= 49.50
Slope (%)	= 0.50	Qmax (cfs)	= 149.50
Invert Elev Up (ft)	= 6041.40	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 36.0		
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 149.50
No. Barrels	= 1	Qpipe (cfs)	= 60.39
n-Value	= 0.013	Qovertop (cfs)	= 89.11
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 8.89
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 8.54
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 6043.45
		HGL Up (ft)	= 6044.62
Embankment		Hw Elev (ft)	= 6046.31
Ton Flowetian (ft)			- 1 6 1

Top Elevation (ft) Top Width (ft) Crest Width (ft)

=	6045.50
=	40.00
=	40.00

Qtotal (cfs)	=	149.50
Qpipe (cfs)	=	60.39
Qovertop (cfs)	=	89.11
Veloc Dn (ft/s)	=	8.89
Veloc Up (ft/s)	=	8.54
HGL Dn (ft)	=	6043.45
HGL Up (ft)	=	6044.62
Hw Elev (ft)	=	6046.31
Hw/D (ft)	=	1.64
Flow Regime	=	Inlet Control



Tuesday, May 2 2023

### CULVERT 2 - OFFSITE F1 & Pond B

Invert Elev Dn (ft)	= 6038.00	Calculations	
Pipe Length (ft)	= 150.00	Qmin (cfs)	= 85.70
Slope (%)	= 0.50	Qmax (cfs)	= 185.70
Invert Elev Up (ft)	= 6038.75	Tailwater Élev (ft)	= (dc+D)/2
Rise (in)	= 36.0		, , , , , , , , , , , , , , , , , , ,
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 185.70
No. Barrels	= 1	Qpipe (cfs)	= 79.29
n-Value	= 0.013	Qovertop (cfs)	= 106.41
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 11.37
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 11.22
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 6040.88
		HGL Up (ft)	= 6042.92
Embankment		Hw Elev (ft)	= 6045.76
Top Elevation (ft)	= 6044.85	Hw/D (ft)	= 2.34

Top Width (ft) Crest Width (ft)

=	6044.85
=	40.00
=	40.00

Qpipe (cts)	= 79.29
Qovertop (cfs)	= 106.41
Veloc Dn (ft/s)	= 11.37
Veloc Up (ft/s)	= 11.22
HGL Dn (ft)	= 6040.88
HGL Up (ft)	= 6042.92
Hw Elev (ft)	= 6045.76
Hw/D (ft)	= 2.34
Flow Regime	= Inlet Control
-	



Tuesday, May 2 2023

#### **CULVERT 3 - OFFSITE F3 & POND D**

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft)	= 6026.00 = 140.00 = 0.50 = 6026.70	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 77.50 = 177.50 = (dc+D)/2
Rise (in)	= 36.0		
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 177.50
No. Barrels	= 1	Qpipe (cfs)	= 72.50
n-Value	= 0.013	Qovertop (cfs)	= 105.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 10.46
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 10.26
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 6028.84
		HGL Up (ft)	= 6030.45
Embankment		Hw Elev (ft)	= 6032.89
Top Elevation (ft)	= 6032.00	Hw/D (ft)	= 2.06

Т Top Width (ft) Crest Width (ft)

=	6032.00
=	40.00
=	40.00

Veloc Dn (ft/s)	=	10.46
Veloc Up (ft/s)	=	10.26
HGL Dn (ft)	=	6028.84
HGL Up (ft)	=	6030.45
Hw Elev (ft)	=	6032.89
Hw/D (ft)	=	2.06
Flow Regime	=	Inlet Control
-		



Tuesday, May 2 2023

## **CULVERT 4 - PORTION OF BASIN G**

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft)	= 6053.00 = 90.00 = 0.50 = 6053.45	<b>Calculations</b> Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 21.40 = 39.10 = (dc+D)/2
Rise (in)	= 18.0 = Circulor		
		Highlighted	00.40
Span (in)	= 18.0	Qtotal (cfs)	= 38.40
No. Barrels	= 1	Qpipe (cfs)	= 18.29
n-Value	= 0.013	Qovertop (cfs)	= 20.11
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 10.39
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 10.35
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 6054.48
		HGL Up (ft)	= 6057.09
Embankment		Hw Elev (ft)	= 6058.72
Top Elevation (ft)	= 6058.45	Hw/D (ft)	= 3.51
Top Width (ft)	= 40.00	Flow Regime	= Inlet Conti

Т Top Width (ft) Crest Width (ft)

=	6058.45
=	40.00
=	10 00

40.00

= Inlet Control



Tuesday, May 2 2023

## **CULVERT 5 - PORTION OF BASIN G**

Invert Elev Dn (ft)	= 6040.00	Calculations	
Pipe Length (ft)	= 80.00	Qmin (cfs)	= 45.10
Slope (%)	= 0.50	Qmax (cfs)	= 89.90
Invert Elev Up (ft)	= 6040.40	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0		
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 89.10
No. Barrels	= 1	Qpipe (cfs)	= 28.76
n-Value	= 0.013	Qovertop (cfs)	= 60.34
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 9.28
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 9.15
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 6041.92
		HGL Up (ft)	= 6043.17
Embankment		Hw Elev (ft)	= 6045.07
Top Flowation (ft)	- 6044 50		- 2.24

E Top Elevation (ft)

Top Width (ft) Crest Width (ft)

=	6044.50
=	40.00
_	10 00

= 40.00

Qtotal (cfs)	=	89.10
Qpipe (cfs)	=	28.76
Qovertop (cfs)	=	60.34
Veloc Dn (ft/s)	=	9.28
Veloc Up (ft/s)	=	9.15
HGL Dn (ft)	=	6041.92
HGL Up (ft)	=	6043.17
Hw Elev (ft)	=	6045.07
Hw/D (ft)	=	2.34
Flow Regime	=	Inlet Control



Tuesday, May 2 2023

## **CULVERT 6 - PORTION OF BASIN G**

Invert Elev Dn (ft) Pipe Length (ft) Slope (%)	= 6030.00 = 80.00 = 0.50	<b>Calculations</b> Qmin (cfs) Qmax (cfs)	= 68.80 = 142.40
Invert Elev Up (ft) Rise (in)	= 6030.40 = 30.0	Tailwater Elev (ft)	= (dc+D)/2
Shape	= Circular	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 141.80
No. Barrels	= 1	Qpipe (cfs)	= 47.49
n-Value	= 0.013	Qovertop (cfs)	= 94.31
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 9.84
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 9.68
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 6032.38
		HGL Up (ft)	= 6033.44
Embankment		Hw Elev (ft)	= 6035.79
Top Elevation (ft)	= 6035.00	Hw/D (ft)	= 2.16
Top Width (ft)	= 40.00	Flow Regime	= Inlet Cont

Top Width (ft) Crest Width (ft)

=	6035.00
=	40.00
=	10 00

40.00

6032.38
6033.44
6035.79
2.16

= Inlet Control



# **Culvert Report**

Crest Width (ft)

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

= 40.00

Tuesday, May 2 2023

## **CULVERT 7 - PORTION OF BASIN F**

Invert Elev Dn (ft)	= 6055.80	Calculations	
Pipe Length (ft)	= 80.00	Qmin (cfs)	= 17.30
Slope (%)	= 0.50	Qmax (cfs)	= 38.10
Invert Elev Up (ft)	= 6056.20	Tailwater Élev (ft)	= (dc+D)/2
Rise (in)	= 24.0		ζ ,
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 37.30
No. Barrels	= 1	Qpipe (cfs)	= 23.31
n-Value	= 0.013	Qovertop (cfs)	= 13.99
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 7.66
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 7.42
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 6057.66
		HGL Up (ft)	= 6058.51
Embankment		Hw Elev (ft)	= 6059.73
Top Elevation (ft)	= 6059.50	Hw/D (ft)	= 1.76
Top Width (ft)	= 40.00	Flow Regime	= Inlet Control

Elev (ft) CULVERT 7 - PORTION OF BASIN F Hw Depth (ft) 6060.00 - 3.80 Inlet control 6059.00 2.80 6058.00 1.80 6057.00 0.80 6056.00 -0.20 6055.00 -1.20 6054.00 --2.20 'n 10 20 30 40 50 60 70 80 90 100 110 120 Circular Culvert HGL Embank Reach (ft)

Tuesday, May 2 2023

## **CULVERT 8 - PORTION OF BASIN F**

Invert Elev Dn (ft)	= 6054.60	Calculations	
Pipe Length (ft)	= 80.00	Qmin (cfs)	= 17.80
Slope (%)	= 0.50	Qmax (cfs)	= 39.30
Invert Elev Up (ft)	= 6055.00	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0		. ,
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 38.80
No. Barrels	= 1	Qpipe (cfs)	= 28.81
n-Value	= 0.013	Qovertop (cfs)	= 9.99
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 9.29
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 9.17
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 6056.52
		HGL Up (ft)	= 6057.77
Embankment		Hw Elev (ft)	= 6059.68
Top Elevation (ft)	= 6059.50	Hw/D (ft)	= 2.34

Top Width (ft) Crest Width (ft)

=	6059.50
=	40.00
=	40.00

Figniightea		
Qtotal (cfs)	=	38.80
Qpipe (cfs)	=	28.81
Qovertop (cfs)	=	9.99
Veloc Dn (ft/s)	=	9.29
Veloc Up (ft/s)	=	9.17
HGL Dn (ft)	=	6056.52
HGL Up (ft)	=	6057.77
Hw Elev (ft)	=	6059.68
Hw/D (ft)	=	2.34
Flow Regime	=	Inlet Control



## **APPENDIX D – DRAINAGE MAPS**



BASIN	
EX-A	
EX-B	
EX-C	
EX-D	
EX-E	
EX-F	
OFF-1	

# BASIN SUMMARY TABLE

AREA (AC)	5-YR (CFS)	100-YR (CFS)
44.00	151.65	184.80
100.00	169.04	271.50
135.00	34.51	151
185.00	40.27	176.20
59.00	14.14	61.80
22.00	6.65	29.10
44.00	5.90	25.80

provide a design point summary table with 5 and 100yr flows

Design point summary table has been provided.

	BY DATE		
	REVISION		
	Ö		
		1635 WEST 13TH AVENUE, SUITE 310 STATE 310	DENVER, COLORADO 80204 333 PHONE: 303-753-6730 301 33
	1AYBERRY SKETCH PLAN	MAYBERRY, COLORADO SPRINGS EL PASO COUNTY	MAYBERRY COMMUNITIES, LLC 3296 DEVINE HEIGHTS #208 COLORADO SPRINGS, CO 80922
		TE ADDRESS:	EPARED FOR:
		EXHIBI	T.
	JOB NO. ORG. SUB DWN:	MC222 M. DATE GWH	208 <sup>HKD:</sup> _CJD
1200'	DRA	HISTO	RIC E PLAN
	NO.	DF	<b>R1</b>

## DESCRIPTION

PROPERTY LINE

MAJOR CONTOUR

MINOR CONTOUR

PROPOSED

\_\_\_\_\_

- 5825-

- 5822-

°C−1\*

-

1\*\*

 5822	

EXISTING

DRAINAGE BASIN LABEL \* BASIN LABEL \*\* TRIBUTARY AREA (AC)

FLOW ARROW

DESIGN POINT

DRAINAGE AREA BOUNDARY

SCALE: 1" = 400'











## **APPENDIX E – REFERENCED DRAINAGE REPORTS**





## MASTER DEVELOPMENT DRAINAGE PLAN FOR ELLICOTT TOWN CENTER

**Prepared for:** 

Accretive Capital Partners, LLC 3655 Nobel Drive, Suite 650 San Diego, CA 92122

August 25, 2005 Revised October 31, 2005 Revised November 22, 2005

Prepared by:



19 East Willamette Avenue Colorado Springs, CO 80903 (719)-477-9429 (719)-471-0766 FAX

JPS Project No. 030502





<u>LEGEND</u>

DRAINAGE BASIN

AREA (AC)

DESIGN POINT

05 / 0100 (CFS)

MAJOR BASIN LINE

BASIN LINE

1005



#### ELLICOTT TOWN CENTER **RATIONAL METHOD - DRAINAGE CALCULATIONS**

#### DEVELOPED FLOWS

				С	OVERLAND			CHANNEL	CONVEYANCE		SCS <sup>(2)</sup>		TOTAL	INTE	NSITY <sup>(5)</sup>	PEAK	FLOW
BASIN	DESIGN	AREA	5-YEAR(7)	100-YEAR (7)	LENGTH	SLOPE	Tco <sup>(1)</sup>	LENGTH	COEFFICIENT	SLOPE	VELOCITY	Tt <sup>(3)</sup>	Tc (4)	5-YR	100-YR	Q5 <sup>(0)</sup>	Q100 <sup>(0)</sup>
	POINT	(AC)	1		(FT)	(%)	(MIN)	(FT)	к	. (%)	_(FT/\$)	(MIN)	(MIN)	(IN/HB)	(IN/HR)	(CFS)	(CFS)
OA2		15.1	0.250	0.350									26.5	2.50	4.50	9,44	23.78
OA1		66.8	0.250	0.350	1000	0.5	60.9	2300	1.50	0.9	1.42	26.9	87.9_	1.50	2.65	25.05	61.96
A		60.0	0.468	0.568			0.0	2400	1.50	1.0	1.50	26.7	26.7	1.70	3.15	47.72	107.32
OA2,OA1, A	1	141.9	0.342	0.442									141.0	1.50	2,65	72.78	166.18
EC12		_30,3	0.250	0.350						_			33.0	2.20	3.80	16.67	40.30
OB1		33.7	0.250	0.350	700	1.4	36.2	0				0.0	36.2	2.10	3.70	17.69	43.64
B1	l	97.0	_0.591	0.671			0.0	2000	1.50	1.1	1.57	21.2	21.2	1.50	2.65	85.96	172.41
B2		85.3	0.522	0.622			0.0	2600	1.50	1,1	1.57	27.5	27.5	1.50	2.65	66.79	140.60
EC12,OB1,B1,B2	B2	246.3	0.479	0.571									117.9	1.50	2.65	176.94	372.63
BB		20.3	0.520	0.620	1000	2.8	23.4	300	1.50	1.0	1.50	3.3	26.8	2.00	3.50	21.11	_44.05
B3		59,1	0.507	0.607			0.0	1300	1.50	1.3	1.71	12.7	12.7				
EC12,OB1,B1-B3,BB	3	325.7	0.486	0.580									130.6	1.50	2.65	237.41	500.54
			<u> </u>													5.00	40.00
B4	4	4.5	0.550	0.650	300	1.0	17.1	800	1.50	0.5	1.06	12.6	29.7	2.35	4.20	5.82	12.29
EC11		000	0.050	0.250	1000	1.0	<u> </u>	6195	1.50	1 2	1 71	60.9	109.2	1.50	265	111.00	274 54
	·	1607	0.230	0.330	1000	1.0	40.4	3000	1.50	1.0	1.7	47.0	47.0	1.50	2.00	127.30	265.16
<u> </u>		59.62	0.522	0.013	200	1.0	17.5	3900	2.00	0.9	1.30	97.0	47.0	1.50	2.00	47 39	00.26
EC12 EC11 OP1 B C		50.02	0.559	0.035	300	1.0	17.5	3000	2.00	0.03	1.02	21.4	165.0	1.50	2.05	295 56	639.20
		517.3	0.300	0.400									100.2	1.50	2.00	200.00	0.00.04
EC10		1427	0.250	0.350	1000	10	48.4	6300	1.50	11	1.57	66.7	115.1	1.50	2.65	53 51	132.35
F		84	0.200	0.575	1000	1.0	0.0	1300	1 50	0.9	1.39	15.6	15.6	1.50	2.65	6.00	12.83
EC10,E	6	151.1	0.263	0.363	<u> </u>						1.55		130.7	2.00	3.65	79.49	200.23

1) OVERLAND FLOW Tco = (1.87\*(1.1-RUNOFF COEFFICIENT)\*(OVERLAND FLOW LENGTH~(0.5)/(SLOPE~(0.333))

2) SCS VELOCITY = K \* ((SLOPE(%))^0.5)

K = 0.25 FOR MEADOW

K = 1.0 FOR BARE SOIL

K = 1.5 FOR GRASS CHANNEL

K = 2.0 FOR PAVEMENT

3) CHANNEL / SWALE / GUTTER FLOW, Tt = (CHANNEL LENGTH/ SCS VELOCITY) / 60 SEC 4) Tc = Tco + Tt

\*\*\* IF TOTAL TIME OF CONCENTRATION IS LESS THAN 5 MINUTES, THEN 5 MINUTES IS USED 5) INTENSITY BASED ON I-D-F CURVE IN EL PASO COUNTY DRAINAGE CRITERIA MANUAL

6) Q = CIA

7) WEIGHTED AVERAGE C VALUES FOR COMBINED BASINS

## FINAL DRAINAGE REPORT for MAYBERRY, COLORADO SPRINGS – FILING NO. 1A REPLAT

**Prepared for:** 

Mayberry Communities, LLC PO Box 675725 Rancho Santa Fe, CA 92067

November 19, 2021 Revised February 22, 2022 Revised April 8, 2022

**Prepared by:** 



19 East Willamette Avenue Colorado Springs, CO 80903 (719)-477-9429 www.jpsengr.com

JPS Project No. 030502 PCD File No. VR2113

#### MAYBERRY, COLORADO SPRINGS (fka "ELLICOTT TOWN CENTER")

HISTORIC FLOWS									Ove	erland Flo	w				Channel f	low			Time of	Total	Total	Peak Flo	w
				RUNOFF	CURVE			PERCENT				HIGH	LOW		CHANNEL	CHANNEL			Concentration	Lag Time	Lag Time	S	cs
BASIN	DESIGN	AREA	AREA	COEFFICIENT	No.			IMPERVIOUS	LENGTH	SLOPE	Tco <sup>(1)</sup>	ELEV.	ELEV.	н	LENGTH	LENGTH	SLOPE	Tt (1)	Tc (2)	TI <sup>(2)</sup>	TI <sup>(2)</sup>	Q5 <sup>(3)</sup>	Q100 <sup>(3)</sup>
	POINT	(AC)	(SM)	(C5)	(CN)	S	la	(%)	(FT)	(%)	(MIN)	(FT)	(FT)	(FT)	(FT)	(MI)	(%)	(MIN)	(MIN)	(HR)	(MIN)	(CFS)	(CFS)
EC11	EC11	353.6	0.55	0.08	61	6.39	1.28	2	1000	6.0	32.0	6180	6067	113	8945	1.69	1.3%	46.37	78.34	0.78	47.00	24.4	149.5
D		154.6	0.24	0.08	61	6.39	1.28	2			0.0	6067	6028	39	3850	0.73	1.0%	26.38	26.38	0.26	15.83	20.3	141.5
EC11,D	5	508.2	0.79																104.72	1.05	62.83	30.6	174.9
EC10	EC10	317.3	0.50	0.08	61	6.39	1.28	2	1000	1.0	58.1	6140	6052	88	8100	1.53	1.1%	45.53	103.59	1.04	62.15	18.9	110.6
E		7.4	0.01	0.08	61	6.39	1.28	2			0.0	6052	6040	12	1200	0.23	1.0%	10.80	10.80	0.11	6.48	1.4	9.1
EC10,E	6	324.74	0.51																114.39	1.14	68.63	19.1	111.4

DEVELOPED FLOWS									Ove	erland Flo	w				Channel f	flow			Time of	Total	Total	Peak Flo	w
				RUNOFF	CURVE			PERCENT				HIGH	LOW		CHANNEL	CHANNEL			Concentration	Lag Time	Lag Time	sc	CS
BASIN	DESIGN	AREA	AREA	COEFFICIENT	No.			IMPERVIOUS	LENGTH	SLOPE	Tco <sup>(1)</sup>	ELEV.	ELEV.	н	LENGTH	LENGTH	SLOPE	Tt (1)	Tc <sup>(2)</sup>	TI <sup>(2)</sup>	TI <sup>(2)</sup>	Q5 <sup>(3)</sup>	Q100 <sup>(3)</sup>
	POINT	(AC)	(SM)	(C5)	(CN)	S	la	(%)	(FT)	(%)	(MIN)	(FT)	(FT)	(FT)	(FT)	(MI)	(%)	(MIN)	(MIN)	(HR)	(MIN)	(CFS)	(CFS)
EC11	EC11	353.6	0.55	0.08	61	6.39	1.28	2	1000	6.0	32.0	6180	6067	113	8945	1.69	1.3%	46.37	78.34	0.78	47.00	24.4	149.5
C1-C3,D		159.3	0.25	0.331	77.879	2.84	0.57	44.2			0.0	6067	6028	39	3850	0.73	1.0%	26.38	26.38	0.26	15.83	225.0	456.3
EC11,D	5	512.87	0.80																104.72	1.05	62.83	226.6	461.4
EC10	EC10	317.3	0.50	0.08	61	6.39	1.28	2	1000	1.0	58.1	6140	6052	88	8100	1.53	1.1%	45.53	103.59	1.04	62.15	18.9	110.6
E		2.4	0.00	0.114	63.165	5.83	1.17	6.0			0.0	6052	6040	12	1450	0.27	0.8%	13.44	13.44	0.13	8.07	0.9	4.0
EC10,E	6	319.67	0.50																117.03	1.17	70.22	19.0	111.0

FULLY DEVELOPED FL	OWS - FO	R UPST	REAM E	EMERGENCY C	ONDITIO	NS AN	ALYS	IS ONLY	Ov	erland Fl	ow	Channel flow						Time of	Total	Total	Peak Flc	w	
				RUNOFF	CURVE			PERCENT				HIGH	LOW		CHANNEL	CHANNEL			Concentration	Lag Time	Lag Time	S	cs
BASIN	DESIGN	AREA	AREA	COEFFICIENT	No.			IMPERVIOUS	LENGTH	SLOPE	Tco <sup>(1)</sup>	ELEV.	ELEV.	н	LENGTH	LENGTH	SLOPE	Tt (1)	Tc (2)	TI <sup>(2)</sup>	TI (2)	Q5 <sup>(3)</sup>	Q100 <sup>(3)</sup>
	POINT	(AC)	(SM)	(C5)	(CN)	S	la	(%)	(FT)	(%)	(MIN)	(FT)	(FT)	(FT)	(FT)	(MI)	(%)	(MIN)	(MIN)	(HR)	(MIN)	(CFS)	(CFS)
EC11	EC11	353.6	0.55	0.08	63	5.87	1.17	7	1000	6.0	32.0	6180	6067	113	8945	1.69	1.3%	46.37	78.34	0.78	47.00	49.2	196.0

DETAINED FLOWS								Ov	erland Fl	ow				Channel	flow			Time of	Total	Total	Peak Flo	ow	
				RUNOFF	CURVE			PERCENT				HIGH	LOW		CHANNEL	CHANNEL			Concentration	Lag Time	Lag Time	S	CS
BASIN	DESIGN	AREA	AREA	COEFFICIENT	No.			IMPERVIOUS	LENGTH	SLOPE	Tco <sup>(1)</sup>	ELEV.	ELEV.	н	LENGTH	LENGTH	SLOPE	Tt (1)	Tc (2)	TI (2)	TI (2)	Q5 <sup>(3)</sup>	Q100 <sup>(3)</sup>
	POINT	(AC)	(SM)	(C5)	(CN)	S	la	(%)	(FT)	(%)	(MIN)	(FT)	(FT)	(FT)	(FT)	(MI)	(%)	(MIN)	(MIN)	(HR)	(MIN)	(CFS)	(CFS)
EC11	EC11	353.6	0.55	0.08	61	6.39	1.28	2	1000	6.0	32.0	6180	6067	113	8945	1.69	1.3%	46.37	78.34	0.78	47.00	24.4	149.5
CULVERT EC11												6180	6067	113	8945	1.69	1.3%	46.37	46.37	0.46	27.82		
C (C1.1-C1.10)	C1.10A	44.8	0.07	0.375	81.4	2.29	0.46	51.7											35.9	0.36	21.54		
POND C1 DISCHARGE		44.8	0.07																			1.0	9.7
CHANNEL C1												6048	6028	20	2800	0.53	0.7%	23.61	23.61	0.24	14.17		
REACH EC11												6180	6028	152	11745	2.22	1.3%	56.66	56.66	0.57	34.00		
C2,C3,D		113.2	0.18	0.329	58.2	7.18	1.44	43.1											62.6	0.63	37.56		
POND D DISCHARGE		113.2	0.18																			1.7	11.4
EC11,C,D - DETAINED	5d	511.6	0.80																			27.1	170.6

\* Tc from Rational Method Calculation Spreadsheet \*\* Pond Discharge Flows from MHFD-Detention Calculations

1) OVERLAND FLOW Tco = (1.8\*(1.1-RUNOFF COEFFICIENT)\*(OVERLAND FLOW LENGTH^(0.5)/(SLOPE^(0.333)) 2) TRAVEL TIME, Tt = ((11.9\*L^3)/H)^(0.385)

3) To = To  $r = 0.6 \times Tt$ 4) SCS LAG TIME, TI = 0.6 \* Tt 5) PEAK FLOWS CALCULATED BY HEC-HMS 4.8 (TYPE 2 STORM; 5-YR; 24-HR RAINFALL = 2.6 IN; 100-YR; 24-HR RAINFALL = 4.4 IN)

#### Kernel Content and Content and

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💷 🧽 C1-C3,D	^	Global Summary Results for Ru	ın "Run 2"			
🕀 🖶 Reach-D					Project: ETC_D Simula	ation Run: Run 2
DP5 ⊕ ⊕ E ⊕ ⊎ Reach-E ⊕ ⊕ EC10				S E (	Start of Run: 01Jan3000, 01:00 End of Run: 02Jan3000, 01:30 Compute Time:10Sep2019, 21:18:23	Basin Model: Basin 1 Meteorologic Model: Met 2 Control Specifications:Control 1
DP6		Show Elements: All Elements $ \smallsetminus $			Volume Units: (	IN ( AC-FT
Met 1 Mypothetical Storm		Hydrologic	Drainage Area	Peak Discharge	Time of Peak	Volume (AC-ET)
Met 2	~	EC11 Brack D	0.55	24.4 24.4	01Jan3000, 13:52	7.9
Components Compute Results		C1-C3,D	0.35	24.4	01Jan3000, 14:07 01Jan3000, 13:08	21.6
Unathetical Starm		EC10	0.80	226.6	01Jan3000, 13:08 01Jan3000, 14:13	29.4
Hypothetical Storm		Reach-E	0.50	18.9	01Jan3000, 14:19	7.0
Mat Nama, Mat 2		E	0.00	0.9	01Jan3000, 13:04	0.1
Met Name. Met 2		DP6	0.50	19.0	01Jan3000, 14:18	7.1
Method: SCS Type 2	~					
Point Depth (IN) 2.6						
Area Reduction:None	~					
		NOTE 40043: The basin model "Basin 1" conta	ins 2 elements with no downstream connectio	n: DP5, DP6		
		NOTE 40043: The basin model "Basin 1" contain NOTE 15301: Began computing simulation run	ins 2 elements with no downstream connection	n: DP5, DP6		
		NOTE 20364: Found no parameter problems in	meteorologic model "Met 1".			
		NOTE 40040: The basin model contains 2 outle	ets: DP5, DP6			
		NOTE 40049: Found no parameter problems in NOTE 41743: Initial abstraction ratio for subb	i basin model "Basin 1". asin "EC11" is 0.2002.			
		NOTE 41743: Initial abstraction ratio for subb	asin "C1-C3,D" is 0.2007.			
		NOTE 41743: Initial abstraction ratio for subb	asin "EC10" is 0.2002.			
		NOTE 41/43: Initial abstraction ratio for subb NOTE 42413: Unit hydrograph volume for sub	asin "E-1s 0.2006. basin "EC11" is 1.0000 in.			
		NOTE 42413: Unit hydrograph volume for sub	basin "C1-C3,D" is 1.0000 in.			
		NOTE 42413: Unit hydrograph volume for sub	basin "EC10" is 1.0000 in.			
		NOTE 15302: Finished computing simulation ru	n "Run 1" at time 10Sep2019, 21:12:11.			
		NOTE 40043: The basin model "Basin 1" conta	ins 2 elements with no downstream connection	n: DP5, DP6		
		NOTE 40043: The basin model "Basin 1" contained and the second se	ins 2 elements with no downstream connection	n: DP5, DP6		
		NOTE 20364: Found no parameter problems in	meteorologic model "Met 2".			
		NOTE 40040: The basin model contains 2 outle	ets: DP5, DP6			
		NOTE 40049: Found no parameter problems in	basin model "Basin 1".			
		NOTE 41743: Initial abstraction ratio for subba	asin EC11 IS 0.2002. asin "C1-C3.D" is 0.2007.			
		NOTE 41743: Initial abstraction ratio for subb	asin "EC10" is 0.2002.			
		NOTE 41743: Initial abstraction ratio for subb	asin "E" is 0.2006.			
		NOTE 42413: Unit hydrograph volume for sub	basin "EC11" is 1.0000 in.			
		NOTE 42413: Unit hydrograph volume for sub	basin "EC10" is 1.0000 in.			

#### Kernel Content and Content and

File Edit View Components GIS Parameters Compute Results Tools Help

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Basin Models	^	🖾 Global Summary Results for Run "Ru	n 1"			
🖨 💋 Basin 1					Project: ETC_D Simul	ation Run: Run 1
⊕ Keach-D ⊕ EC11 ⊕ DP5 ⊕ E				S E (	Start of Run: 01Jan3000, 01:00 End of Run: 02Jan3000, 01:30 Compute Time:10Sep2019, 21:12:10	Basin Model: Basin 1 Meteorologic Model: Met 1 Control Specifications:Control 1
⊕ 🔄 Reach-E ⊕ 🚔 EC10		Show Elements: All Elements $ \smallsetminus $			Volume Units:	IN () AC-FT
DP6		Hydrologic Element	Drainage Area (MI2)	Peak Discharge (CFS)	Time of Peak	Volume (AC-FT)
Hypothetical Storm	~	EC11 Reach-D	0.55	149.5	01Jan3000, 13:46	31.6
Components Compute Results		C1-C3,D	0.25	456.3	01Jan3000, 13:08	42.3
Hypothetical Storm		EC10	0.50	110.6	01Jan3000, 14:04	28.5
		Reach-E	0.50	110.6	01Jan3000, 14:10	28.4
Met Name: Met 1		E	0.00	4.0	01Jan3000, 13:02	0.3
Method: SCS Type 2	$\sim$	DP6	0.50	111.0	01Jan3000, 14:10	28.7
*Point Depth (IN) 4.4						
Area Reduction:None	~					
		NOTE 42413: Unit hydrograph volume for subbasin "D	" is 1.0000 in.			
		NOTE 42413: Unit hydrograph volume for subbasin "El NOTE 42413: Unit hydrograph volume for subbasin "El	C11" is 1.0000 in. ' is 1.0000 in			
		NOTE 42413: Unit hydrograph volume for subbasin "E	210" is 1.0000 in.			
		NOTE 15302: Finished computing simulation run "Run 2 NOTE 40043: The basin model "Basin 1" contains 2 ele	" at time 10Sep2019, 20:56:09.	DP5 DP6		
		NOTE 40043: The basin model "Basin 1" contains 2 ele	ments with no downstream connection	n: DP5, DP6		
		NOTE 40043: The basin model "Basin 1" contains 2 ele	ments with no downstream connection	1: DP5, DP6 * at time 10Sep2019 21:04:34		
		NOTE 10187: Closed project "ETC-H" at time 10Sep20	19, 21:04:35.	at and 105cp2015, 21.0 1.5 1.		
		NOTE 10023: Finished copying project "ETC_D" to dire	ctory "G:\jpsprojects\030502.etc\ET( " at time 10Sep2019 21:05:25	C_D" at time 10Sep2019, 21:04:36.		
		NOTE 40043: The basin model "Basin 1" contains 2 ele	ments with no downstream connection	n: DP5, DP6		
		NOTE 40043: The basin model "Basin 1" contains 2 ele	ments with no downstream connection	1: DP5, DP6		
		NOTE 40043: The basin model "Basin 1" contains 2 ele	ments with no downstream connection	n: DP5, DP6		
		NOTE 40043: The basin model "Basin 1" contains 2 ele	ments with no downstream connection	n: DP5, DP6		
		NOTE 20364: Found no parameter problems in meteor	ologic model "Met 1".			
		NOTE 40040: The basin model contains 2 outlets: DP5	, DP6			
		NOTE 40049: Found no parameter problems in basin m NOTE 41743: Initial abstraction ratio for subbasin "EC	odel "Basin 1". 11" is 0.2002.			
		NOTE 41743: Initial abstraction ratio for subbasin "C1	C3,D" is 0.2007.			
		NOTE 41743: Initial abstraction ratio for subbasin "EC	10" is 0.2002.			
		NOTE 42413: Unit hydrograph volume for subbasin "E"	s 0.2006. 211" is 1.0000 in.			
		NOTE 42413: Unit hydrograph volume for subbasin "C	1-C3,D <sup>®</sup> is 1.0000 in.			
		NOTE 42413: Unit hydrograph volume for subbasin "E	210° is 1.0000 in.			



DECION O5 O100	
<u>POINT (CFS) (CFS)</u>	
EC11 24.4 149.5	
C1.1 5.4 18.0	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
C1.4 6.3 15.3	
C1.5 6.2 15.6	
C1.6 3.8 9.4	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
C1.8 7.5 18.4	
C1.9A 13.7 33.3 C1.9B 35.7 87.0	



## **FINAL DRAINAGE REPORT**

For

## MAYBERRY, COLORADO SPRINGS – FILING NO. 3

**PREPARED FOR:** 

COLORADO SPRINGS MAYBERRY, LLC 3296 DEVINE HEIGHTS #208 COLORADO SPRINGS, CO 80922

**PREPARED BY:** 

R & R ENGINEERS - SURVEYORS, INC. 1635 W. 13<sup>™</sup> AVE, SUITE 310 DENVER, CO 80204 CONTACT: CLIF DAYTON, P.E. (303) 753-6730

> R&R JOB #MC22110 EPC PROJECT NO. SF2219

ORIGINAL SUBMITTAL: MAY 2022 2<sup>ND</sup> SUBMITTAL: SEPTEMBER 2022 3RD SUBMITTAL: JANUARY 2023 4TH SUBMITTAL: APRIL 2023

1635 West 13<sup>th</sup> Avenue - Suite 310, Denver, Colorado 80204 Phone - (303) 753-6730 Fax - (303) 753-6568

# Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	18.43	1	772	262 007				EC10
2	SCS Runoff	1 349	1	734	6 442				OS-1
3	SCS Runoff	8.399	1	737	76.243				EX-D1
4	SCS Runoff	1.367	1	728	9.340				EX-D2
5	Combine	9.557	1	735	85,583	3, 4			TOTAL ONSITE FLOW
6	Combine	23.73	1	755	344,692	1, 2, 3,			DP EX-5
7	SCS Runoff	6.054	1	745	62,432				EX-E
8	SCS Runoff	3.682	1	729	15,373				EX-LOG
9	Combine	30.51	1	752	422,497	6, 7, 8			DP EX-6
10	SCS Runoff	8.146	1	742	76,284				EX-Z
11	Combine	38.16	1	751	498,780	9, 10			DP EX-7
## Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

#### Hyd. No. 1

SCS Runoff	Peak discharge	= 18.43 cfs
5 yrs	Time to peak	= 772 min
1 min	Hyd. volume	= 262,007 cuft
320.000 ac	Curve number	= 61
0.0 %	Hydraulic length	= 0 ft
TR55	Time of conc. (Tc)	= 63.00 min
2.60 in	Distribution	= Type II
24 hrs	Shape factor	= 484
	SCS Runoff 5 yrs 1 min 320.000 ac 0.0 % TR55 2.60 in 24 hrs	SCS RunoffPeak discharge5 yrsTime to peak1 minHyd. volume320.000 acCurve number0.0 %Hydraulic lengthTR55Time of conc. (Tc)2.60 inDistribution24 hrsShape factor



# Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	144 67	1	755	1 185 497				FC10
2	SCS Runoff	4.333	1	733	18,356				OS-1
3	SCS Runoff	76.23	1	732	344,975				EX-D1
4	SCS Runoff	12.54	1	725	42,259				EX-D2
5	Combine	86.19	1	731	387,234	3, 4			TOTAL ONSITE FLOW
6	Combine	183.85	1	749	1,548,829	1, 2, 3,			DP EX-5
7	SCS Runoff	53.32	1	736	282,485				EX-E
8	SCS Runoff	6.317	1	729	27,009				EX-LOG
9	Combine	231.35	1	745	1,858,321	6, 7, 8			DP EX-6
10	SCS Runoff	63.40	1	736	328,266				EX-Z
11	Combine	289.85	1	740	2,186,588	9, 10			DP EX-7

# Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

#### Hyd. No. 1

#### EC10

Hydrograph type	= SCS Runoff	Peak discharge	<ul> <li>= 144.67 cfs</li> <li>= 755 min</li> <li>= 1,185,497 cuft</li> <li>= 61</li> <li>= 0 ft</li> <li>= 63.00 min</li> </ul>
Storm frequency	= 100 yrs	Time to peak	
Time interval	= 1 min	Hyd. volume	
Drainage area	= 320.000 ac	Curve number	
Basin Slope	= 0.0 %	Hydraulic length	
Tc method	= TR55	Time of conc. (Tc)	
Basin Slope	= 0.0 %	Hydraulic length	= 0  ft
Tc method	= TR55	Time of conc. (Tc)	= 63.00 min
Total precip	= 4.40 in		= Type II
Storm duration	= 24 hrs	Shape factor	= 484



Thursday, 01 / 5 / 2023



ATH: \\192.168.100.23\PROJECTS\MC22110 MAYBERRY FILING NO. 3\ENGINEERING\4 DRAWINGS\PLANS\DRAINAGE MAPS\MC22110-XP-DRNG MAP DTL.DWG, PLOT DATE: 1/5/2023 2:50:24 PM, BY:LIZ JONES

### V1\_Master Development Drainage Plan (MDDP).pdf Markup Summary



This offsite flow (EC12 and OFF-1) will now be channelized. Erssion and downstream impacts should be addressed. basin C 	Subject: Contractor Page Label: 10 Author: Christina Prete Date: 11/15/2023 11:48:39 AM Status: Color: Layer: Space:	This offsite flow (EC12 and OFF-1) will now be channelized. Erosion and downstream impacts should be addressed.
C, designed and construc ine. Pond B will discharge 1. Discuss Plunge Pool 3 orner of drainage Basin D. I and is 15.5 acre-feet. Pon-	Subject: Contractor Page Label: 11 Author: Christina Prete Date: 11/15/2023 12:15:07 PM Status: Color: Layer: Space:	Discuss Plunge Pool 3
Channel F? (see SF2219) E, co	Subject: Contractor Page Label: 12 Author: Christina Prete Date: 11/15/2023 12:14:14 PM Status: Color: Layer: Space:	Channel F? (see SF2219)
d on the tributary land- l discharge into Channel [0. Discuss Plunge Pool 4] Based on the tributary ad E will discharge into	Subject: Contractor Page Label: 12 Author: Christina Prete Date: 11/15/2023 12:18:48 PM Status: Color: Layer: Space:	Discuss Plunge Pool 4
	Subject: Contractor Page Label: [1] MC22110-DEVELOPED DRN PLAN-OVERALL Author: Christina Prete Date: 11/15/2023 11:54:17 AM Status: Color: ■ Layer: Space:	Channel E (see SF2219)
CHANNEL E Channel F? (see SF2219)	Subject: Contractor Page Label: [1] MC22110-DEVELOPED DRN PLAN-OVERALL Author: Christina Prete Date: 11/15/2023 11:54:24 AM Status: Color: ■ Layer: Space:	Channel F? (see SF2219)

	Subject: Contractor Page Label: [1] MC22110-DEVELOPED DRN PLAN-OVERALL Author: Christina Prete Date: 11/15/2023 11:56:56 AM Status: Color: Layer: Space:	text states 110 acres
	Subject: Contractor Page Label: [1] MC22110-DEVELOPED DRN PLAN-OVERALL Author: Christina Prete Date: 11/15/2023 12:09:25 PM Status: Color: ■ Layer: Space:	Approved Plans already call out a Channel F onsite
	Subject: Contractor Page Label: [1] MC22110-DEVELOPED DRN PLAN-OVERALL Author: Christina Prete Date: 11/15/2023 12:11:32 PM Status: Color: ■ Layer: Space:	call out Pond C (Interim Condition)
	Subject: Contractor Page Label: [1] MC22110-DEVELOPED DRN PLAN-OVERALL Author: Christina Prete Date: 11/15/2023 1:43:09 PM Status: Color: ■ Layer: Space:	Show Telephone Exchange and Ellicott Consolidated drainage basin limits
Daniel Torres (1	7)	
avroos, NC. 1. Set 10 vros, N. 7739 5739 68. 3030 69. 3030	Subject: Callout Page Label: 1 Author: Daniel Torres Date: 11/14/2023 10:57:08 AM Status: Color: Layer: Space:	SKP236
<text></text>	Subject: Callout Page Label: 10 Author: Daniel Torres Date: 11/14/2023 3:19:30 PM Status: Color: Layer: Space:	should this be EC10 as this offsite flow is on the eastern side of filing 3& 4?

Subject: Callout Please identify where this flow will be directed if Page Label: 10 prevented from entering the site as done in historic Author: Daniel Torres conditions. Provide design points and flows of the Date: 11/14/2023 5:57:27 PM offsite basins entering the development. Status: Color: Layer: Space: Subject: Callout pool 3 is adjacent to pond B Page Label: 13 Author: Daniel Torres Date: 11/14/2023 2:29:06 PM Status: Color: Layer: Space: . . . . . . . . . . . . . . . Subject: Callout plunge pool 4 Page Label: 13 Author: Daniel Torres Date: 11/14/2023 2:32:32 PM Status: Color: Layer: Space: of Pond E and West of Log Road of Basin EC10 before discharging 'ool 3 is located south of Pond F ocated south of Pond G and wil Subject: Callout 1 Page Label: 13 Author: Daniel Torres - 1 Date: 11/14/2023 2:33:10 PM Status: Color: Layer: Space: коай. Нипве ной эльлоса Subject: Callout unge Pool 4 is located soutl 2 Page Label: 13 Author: Daniel Torres 2 Date: 11/14/2023 2:33:07 PM Status: Color: Layer: Space: Subject: Text Box Please discuss the downstream conditions of each Page Label: 14 of the design points where flows are conveyed Author: Daniel Torres offsite. Discuss the ultimate outfall for these flows. Date: 11/15/2023 7:44:37 AM For example is Log Rd ditch anticipated to need Status: improvements; will the flows from DP 4 continue Color: south and cross handle Rd ultimately ending up at Layer: Black Squirrel Creek? please address Space:

e dranage fulfities throughout the development. He next the proposed detection in collises will immersion and the proposed detection in collises will immersion benefitied and maintained by the formesourer's association Address water quality for the almost	Subject: Text Box Page Label: 14 Author: Daniel Torres Date: 11/14/2023 5:50:15 PM Status: Color: Layer: Space:	Address water quality for the site.
er prover prove and neutrance of you have been at associe e dente.	Subject: Text Box Page Label: 14 Author: Daniel Torres Date: 11/14/2023 5:53:44 PM Status: Color: Layer: Space:	please include in the narrative the total flows at the design points. These will be the basis for future final drainage reports
and and a second s	Subject: Text Box Page Label: [1] DR1 HISTORIC DRAINAGE MAP Author: Daniel Torres Date: 11/14/2023 11:52:09 AM Status: Color: Layer: Space:	label the locations of the existing CMP on the northern boundary conveying off-site flow onto the site.
an a	Subject: Text Box Page Label: [1] DR1 HISTORIC DRAINAGE MAP Author: Daniel Torres Date: 11/14/2023 4:03:04 PM Status: Color: Layer: Space:	please also show offsite basins with flow arrows on the existing drainage maps
provide a design point summary table with 5 and 100yr flows	Subject: Text Box Page Label: [1] DR1 HISTORIC DRAINAGE MAP Author: Daniel Torres Date: 11/14/2023 5:31:20 PM Status: Color: Layer: Space:	provide a design point summary table with 5 and 100yr flows
	Subject: Text Box Page Label: [1] MC22110-DEVELOPED DRN PLAN-OVERALL Author: Daniel Torres Date: 11/14/2023 5:55:09 PM Status: Color: Layer: Space:	label the locations of the existing CMP on the northern boundary conveying off-site flow onto the site and provide design points with runoff values.

Subject: Callout please identify in the narrative how this offsite flow Page Label: [1] MC22110-DEVELOPED DRN from EC10 will be conveyed to the south to PLAN-OVERALL channel E. Filing 3 indicated a channel and series Author: Daniel Torres of culverts. Will this be piped under what appears Date: 11/14/2023 5:46:32 PM to be a roadway? please address and provide the Status: appropriate analysis for the conveyance. Please Color: also address the emergency overflow Layer: conveyances through the site per ECM 6.2.12.0 Space: Subject: Callout The road names have changed in the Sketch plan. Page Label: [1] MC22110-DEVELOPED DRN PLAN-OVERALL Author: Daniel Torres Date: 11/14/2023 3:27:48 PM Status: Color: 📘 Layer: Space: Subject: Text Box provide a design point summary table with 5 and Page Label: [1] MC22110-DEVELOPED DRN 100yr flows PLAN-OVERALL Author: Daniel Torres Date: 11/14/2023 5:31:29 PM Status: Color:

> Layer: Space: