FINAL DRAINAGE REPORT FOR Gleneagle Golf Course Residential Infill Development Filing No. 2

PREPARED BY

Michael A. Bartusek, P.E. RESPEC 3520 Austin Bluffs Parkway, Suite 102 Colorado Springs, CO 80918 719-266-5212

PREPARED FOR

G&S DEVELOPMENT, INC. 9800 Pyramid Court, No. 340 Englewood, CO 80112

November 26, 2018 Project Number 03524

VR-18-018





ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the City/County for drainage reports, and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Michael A. Bartusek, P.E. #23329

DEVELOPER'S STATEMENT:

I, the Developer, have read and will comply with all of the requirements specified in this drainage report and plan.

By:

Scott Gratrix

Title: President

Address: G&S Development, Inc. 9800 Pyramid Court, Suite 340 Englewood, CO 80112

Filed in accordance with the El Paso County Land Development Code, Drainage Criteria Manual Volumes 1 and 2, and the Engineering Criteria Manual, as amended.

Jennifer Irvine P.E. County Engineer / ECM Administrator.

Date

Conditions:

FINAL DRAINAGE REPORT GLENEAGLE GOLF COURSE RESIDENTIAL INFILL DEVELOPMENT FILING NO. 2

GENERAL

The Gleneagle Subdivision Filing No. 2 consists of a total of 7.621 acres, of which 0.83 acre will be ROW which previously comprised the Gleneagle Golf Club. The area will be developed with 12 lots and a water quality/detention basin in the western part of the proposed subdivision. The project is located in northwestern El Paso County. It is situated in Sections 6, Township 12 South, Range 67 West of the 6th Principal Meridian, El Paso County, Colorado.

The proposed development was part of the Black Forest Drainage Basin Planning Study, prepared by Wilson and Company in May 1989. The study used storm intervals of ten and 100 years. Our study follows the current City/County Drainage Criteria Manual and uses the five-and 100-year storms.

SOILS

The Soil Conservation Service (NRCS) soil survey for El Paso County has identified three soil types in this study area. They are as follows:

Map Symbol No.	Soil Name	Hydrologic Soil Group
68	Peyton-Pring Complex	В
71	Pring Coarse Sandy Loam	В

FLOODPLAIN STATEMENT

None of the site is located within a 100 year floodplain as determined by FEMA on the Flood Insurance Rate Map (FIRM) Panel 08041 CO287F, dated March 17, 1997.

METHOD OF COMPUTATION

The methodology used for this report is in accordance with the *City/County Drainage Criteria Manual*. The Rational Method for computation of runoff was used for local basin design.

$$Q = cia$$

Where	Q c i	=	Runoff coefficient representing drainage area characteristics
	а	=	Drainage basin size in acres

WETLANDS

No identified wetlands occur within the project area according to the Natural Features and Wetland Report prepared by Ecosystem Services LLC in March 2016.

EXISTING PONDS

No existing ponds are located within the project area. There is a non-jurisdictional stormwater basin located within the western area of the site which is identified on the "Existing Conditions" drainage plan.

WATER QUALITY/DETENTION CONCEPTS

In accordance with current NPDES requirements, stormwater quality BMPs will be incorporated into the development of this project. Water quality facilities will be included in all proposed detention facilities. A water quality/detention basin will be built as part of this project. The new detention basin will be equipped with a 2.5' micro-pool per the DCM Volume 2.

EXISTING DRAINAGE CONDITIONS

As stated previously, the Gleneagle Subdivision Filing No. 2 encompasses approximately 7.62 acres. This study focuses on the development of the 12 lots in the southern part of this development.

This filing of the subdivision drains the southwest area of the Gleneagle Subdivision. This basin drains the area west of the large detention pond from Filing No. 1 and Huntington Beach Dr. and north of Gleneagle Dr.

The basin flows into an existing sump area before it drains overland through existing lots along Westchester Drive. **Basin A** has further been divided into several sub-basins.

Sub-Basin A1 drains the runoff from the homes on Gleneagle Drive just west of Huntington Beach Drive. It produces flows of 1.5 cfs for the five-year storm and 5.4 cfs for the 100-year storm. The runoff then flows into Sub-Basin A2. Some flows from this Sub-Basin enters the adjacent sub-basin through a roadside swale, while most just sheet flows from the street.

Sub-Basin A2 drains the area between the existing sump detention area and Westchester Drive. The mostly undeveloped area produces flows of 3.2 cfs for the fiveyear storm and 22.1 cfs for the 100-year storm. When combined with the flows from Sub-Basin 1 at **DP1** the resulting flows are 4.2 cfs and 25.7 cfs for the five- and 100-year storms, respectively. This runoff currently sheet flows through the existing lots 10 and 11, located mostly on lot 10. These flows continue to the existing ditches along Westchester Drive within Sub-Basin OS1. Calculations show that these flows will split with some flows continuing to the Westchester ditch and some flowing around the back of the house and onto lot 9.

Sub-Basin A3 is a very small area along Gleneagle Drive which sheet flows off of the street and then flows through a small ditch to Westchester Drive. This area produces flows of 1.4 cfs for the five-year storm and 3.9 cfs for the 100-year storm.

Northern?

Sub-Basin OS1 drains the southern developed area of Westchester Drive. It produces flows of 6.9 cfs for the five-year storm and 21.8 cfs for the 100-year storm. These flows and flows from Sub-Basin A3 combine at **DP2** to produce flows of 6.7 cfs and 20.8 cfs for the five- and 100-year storms, respectively. These flows travel north to the existing 30-inch culvert.

Sub-Basin A4 drains the undeveloped area northwest of pond B. It produces flows of 0.3 cfs for the five-year storm and 2.3 cfs for the 100-year storm. These flows then travel along Westchester Drive into Sub-Basin OS2.

Sub-Basin OS2 drains a small area along Westchester Drive, producing flows of 1.3 cfs for the five-year storm and 4.3 cfs for the 100-year storm. These flows and flows from Sub-Basin A4 combine at **DP3** to produce flows of 1.5 cfs and 6.3 cfs for the five- and 100-year storms, respectively. These combined flows then travel south along the Westchester Drive ditch, joining with flows from DP3 at **DP4**. The total combined flows at DP4 are 8.0 cfs and 26.3 cfs for the five- and 100-year storms, respectively.

The combined, total runoff at the existing 30-inch CMP located under Westchester Drive (**DP5**) is 10.7 cfs for the five-year storm and 47.2 cfs for the 100-year storm.

The estimated runoff amounts produced for the project under existing conditions are shown in Table 1 below.

TABLE 1 – EXIST	ING CONDITIONS	
Sub-Basin	Q₅CFS	Q ₁₀₀ CFS
A1	1.5	5.4
A2	3.2	22.1
A3	1.4	3.9
A4	0.3	2.3
OS1	6.9	21.8
OS2	1.3	4.3
DP1(A1+A2)	4.2	25.7
DP2(A3+OS1)	6.7	20.8
DP3(A4+OS2)	1.5	6.3
DP4(DP2+DP3)	8.0	26.3
DP5(DP4+DP1)	10.7	47.2

DEVELOPED DRAINAGE CONDITIONS

A total of 12 lots are proposed within this portion of the previous golf course property. With the average lot size over one-half acre, the resultant increases in flows will be slight. However, a new detention facility will be used to keep flows below historic levels. New ditches and swales will also be added to further reduce the flows that currently flow toward the homes. As a result of the proposed detention basins and other drainage improvements no adverse impacts will result due to this project.

Sub-Basin A1 will remain unchanged and will produce flows of 1.5 cfs for the five-year storm and 5.4 cfs for the 100-year storm. These combined flows will then travel into Sub-Basin A2A.

Sub-Basin A2A will drain the area just west and south of existing Pond B. It will produce flows of 1.6 cfs for the five-year storm and 9.1 cfs for the 100-year storm event. These flows will travel in proposed Swale J. Flows from Sub-Basin A1 and A2A will combine at **DP1** and produce flows of 2.8 cfs and 13.5 cfs for the five- and 100-year storms, respectively.

Sub-Basin A2B will drain the northeast side of Stone Eagle Place. It will produce flows of 1.9 cfs for the five-year storm and 6.6 cfs for the 100-year storm. Flows from this sub-basin and DP1 will combine in a proposed swale at **DP2** to produce total flows of 4.4 cfs and 18.8 cfs for the five- and 100-year storms, respectively. These flows will be directed under Stone Eagle Place into Sub-Basin A2C through a 24-inch RCP culvert.

Sub-Basin A2C will drain the west side of Stone Eagle Place and be directed to a sidewalk chase at the low point and directed into a riprap swale. It will produce flows of 2.7 cfs for the five-year storm and 7.2 cfs for the 100-year storm. Flows from this sub-basin and DP2 will combine at **DP3** to produce total flows of 6.2 cfs and 23.3 cfs for the five- and 100-year storms, respectively. These flows will then be directed into a new detention/water quality facility in Sub-Basin A2D.

Sub-Basin A2D will drain the back areas of the lots located along Stone Eagle Place and portions of the old golf course. It will produce flows of 1.7 cfs for the five-year storm and 9.7 cfs for the 100-year storm. These flows will travel through proposed Swale L with a 12" berm added where the swale makes a 90 degree bend. The combined, undetained flows at the new water quality/ detention basin C (**DP4**) will be 7.0 cfs and 28.9 cfs for the five- and 100-year storms, respectively. The outflow from this proposed detention basin will be 2.8 cfs and 18.0 cfs for the five- and 100-year storms, respectively. Flows from this detention basin will be directed to a proposed 24" private HDPE storm sewer which will be located on Lot 7. In addition the detention overflow swale will also connect to this storm sewer which will discharge into an improved ditch along Westchester Drive.

Sub-Basin A3 is a very small area along Gleneagle Drive and flows through a small ditch to Westchester Drive in Sub-Basin OS4. This area produces flows of 1.4 cfs for the five-year storm and 3.9 cfs for the 100-year storm, which is less than existing conditions.

Sub-Basin OS1 drains the southern developed area of Westchester Drive. It produces flows of 4.5 cfs for the five-year storm and 15.1 cfs for the 100-year storm. These flows and flows from Sub-Basin A3 combine at **DP5** to produce flows of 4.8 cfs and 15.6 cfs for the five- and 100-year storms, respectively. These flows combine with the flows from the detention basin to produce total flows at DP6 in the ditch of 10.9 cfs for the 5-year storm and 41.6 cfs for the 100-year storm. These flows in the riprap-lined ditch along Westchester Drive will be intercepted by a 30" public RCP storm sewer which will take the flows from Westchester Drive to the existing drainage channel located in the Paradise Villas Townhome Subdivision.

Sub-Basin A4 drains the undeveloped area northwest of Pond B. It produces flows of 0.3 cfs for the five-year storm and 2.3 cfs for the 100-year storm which flow toward the existing 30-inch CMP in Westchester Drive. These flows are less than existing conditions and travel along Westchester Drive into Sub-Basin OS2.

Sub-Basin OS2 will remain unchanged and drains a small area along Westchester Drive, producing flows of 3.5 cfs for the five-year storm and 10.7 cfs for the 100-year storm. These flows and flows from Sub-Basin A4 combine at **DP7** to produce flows of 3.5 cfs and 12.0 cfs for the five- and 100-year storms, respectively. These combined flows then travel south along the Westchester Drive ditch to the existing 30" CMP in Westchester Drive.

Please call out the arrangement for Lot 7 to have the Private 24 inch HDPE Pipe. Is there a Drainage easement granted. Identify the owner and maintainer of the easement.

TABLE 2 – DEV	ELOPED CONDITIONS	
Sub-Basin	Q₅CFS	Q ₁₀₀ CFS
OS1	4.5	15.1
OS2	3.5	10.7
A1	1.5	5.4
A2A	1.6	9.1
A2B	1.9	6.6
A2C	2.7	7.2
A2D	1.7	9.7
A3	1.4	3.9
A4	0.3	2.3
DP1 (A1+A2A)	2.8	13.5
DP2 (DP1+A2B)	4.4	18.8
DP3 (DP2+A2B)	6.2	23.3
DP4 (DP3+A4B)	7.0	28.9
DP5 (OS1+A3)	4.8	15.6
DP6 (DP4+DP5)	10.9	41.6
DP7 (OS2+A4)	3.5	12.0

Table 2 shows the estimated runoff produced for the project under developed conditions:

The water quality basin is designed in accordance with current NPDES requirements for extended detention basins. The basin will be constructed with a 2.5-foot permanent micro-pool. Design forms for these basins can be found in *Appendix B*. The design summary is below.

TABLE 3 –	WATER QI	JALITY DESIGN SUN	IMARY	
Location	Depth	Size (SF)	Depth (FT)	Size (SQ IN)
Sub-Basin A2D Detention Basin C	2.66	21,400	0,0.34,0.69	0.86,0.86,0.86

DETENTION BASIN

Developed flows from this project will be reduced to historic levels or below by using detention facilities. The *UDFCD Design for Full Spectrum Detention Basins* is used for the basin design.

	DE	TABLE 4 TENTION BASIN DE	TAILS	
Location	Size (AF)	Pipe Outlet	Outlet Structure	Riprap Weir Width
A2D	0.817	24"	Typical Outlet	13′
			Structure OS-2	

The above detention facility has been designed to reduce the total off-site flows to below historic levels.

PUBLIC DRAINAGE FACILITIES

Item	Unit	Quantity	Unit Cost	Total Cost
24" RCP FES	EA	2	\$600	\$ 1,200.00
30" RCP FES	EA	2	\$700	\$ 1,400.00
24" RCP	LF	100	\$84	\$ 8,400.00
30" RCP	LF	313	\$94	<u>\$29,422.00</u>

PRIVATE DRAINAGE FACILITIES		15% Continger	Sub-Total ncy & Engineering TOTAL	\$40,422.00 <u>\$6,063.30</u> \$46,485.30
Item	Unit	Quantity	Unit Cost	Total Cost
24" HDPE FES	EA	2	\$600	\$ 1,200.00
24" HDPE	LF	226	\$45	\$10,170.00
Type C Inlet	EA	1	\$5,000	\$ 5,000.00
Detention Outlet Structure	EA	1	\$8,000	\$ 8,000.00
Emergency Spillway	EA	1	\$1,500	<u>\$ 1,500.00</u>
			Sub-Total	\$25,870.00
		15% Continger	ıcy & Engineering	<u>\$ 3,880.00</u>
			TOTAL	\$29,750.00

DRAINAGE BASIN FEES

Although the Gleneagle Golf Course Residential Infill Development Filing No. 2 was previously platted under the original subdivision as Tract G, drainage fees must be paid on the impervious acreage of the subdivision.

7.62 Developed Acres x 23% impervious = 1.75 acres 2018 Drainage Fee = \$17,197 per impervious acre x 1.75 = \$30,094.75 2018 Bridge Fee = \$468 per impervious acre x 1.75 = \$795.60

Drainage basin fees for this development will be provided at the existing current fee rate when the final drainage report is submitted at the time of platting.

CONCLUSION

The proposed development and subsequent lot developments follow the "four Step Process" as mandated by the EPA as follows:

Step 1: Employ runoff reduction practices

Runoff has been reduced by disconnecting impervious areas where possible, eliminating "unnecessary" impervious areas and encouraging infiltration into suitable soils.

• Impervious areas have been directed to earth swales to encourage infiltration.

• Gravel will be used in portions of the lots to reduce the impervious of the areas. <u>Step 2: Stabilize drainageways</u>

All drainageways, ditches and channels have been stabilized by the following methods:

- Tributaries have been left in their relatively natural state where possible.
- New drainageways and swales have been stabilized with either riprap or erosion control fabric depending on the erosion potential.
- No new roadside ditches are proposed for the development.
- Step 3: Provide water quality capture volume (WQCV)

The proposed development will disturb approximately 7.6 acres, a WQCV of 0.121 ac-ft will be provided.

Step 4: Consider need for industrial and commercial BMP's.

The development of this project will not affect sensitive waters.

The development of this site will have little impact on downstream properties once the EDB is constructed.

The development of this site will have little impact on downstream properties once the water quality/detention basins are constructed.

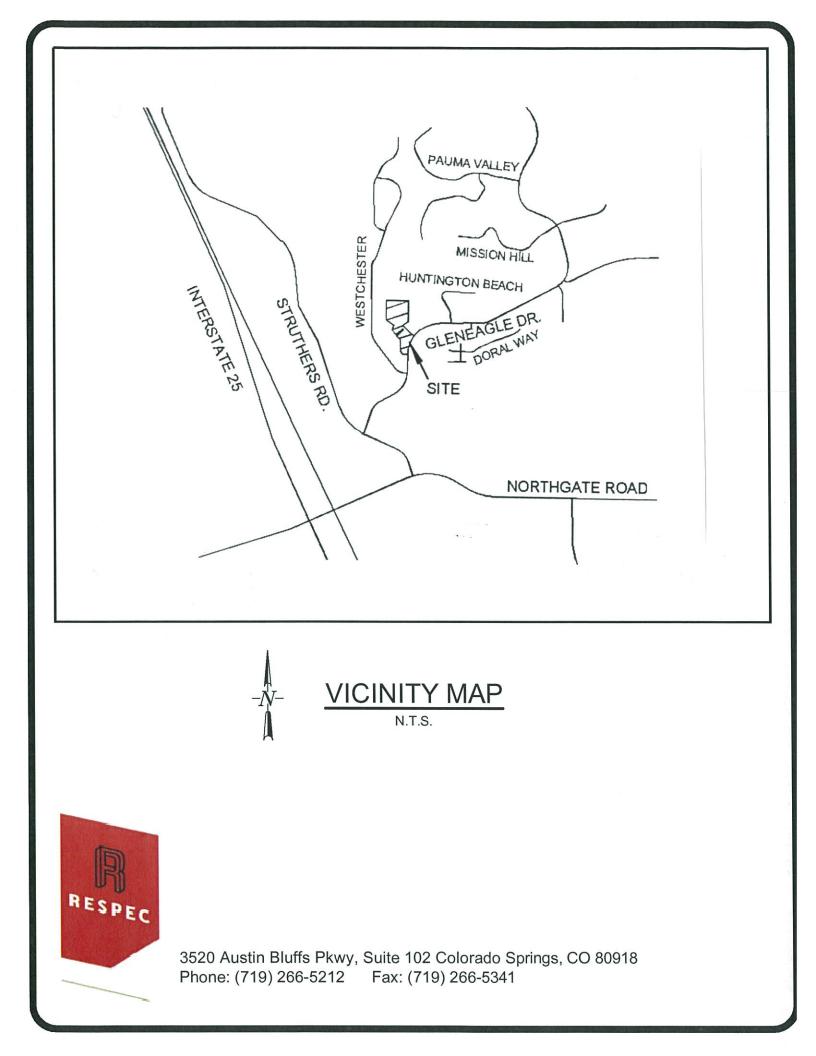
REFERENCES

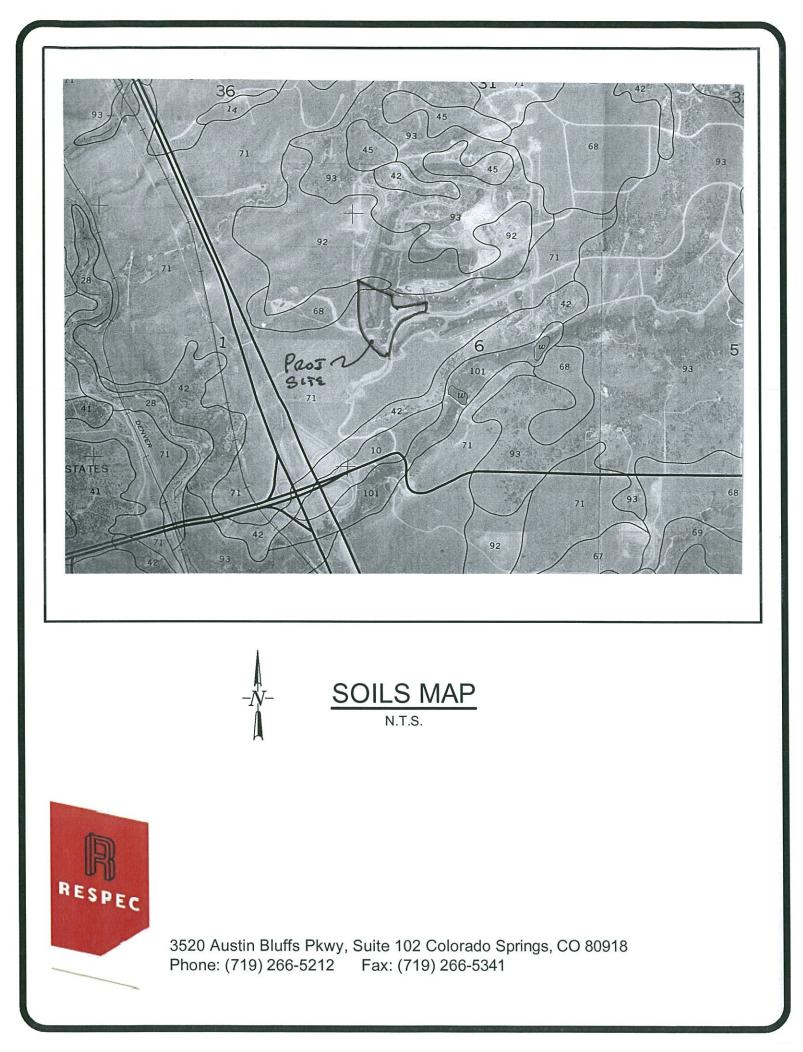
- City of Colorado Springs and El Paso County (1994). *Drainage Criteria Manual Volume* 1 (DCM).
- 2. City of Colorado Springs and El Paso County (1994). *Drainage Criteria Manual Volume II* (DCM).
- 3. Soil Survey of El Paso County Area, Colorado by USDA, NRCS.
- 4. El Paso County (January 2006) Engineering Criteria Manual.
- 5. Urban Drainage and Flood Control District (June 2011). Urban Storm Drainage Criteria Manual, Volume 1-3.
- 6. Gleneagle Golf Course Residential Infill Development Preliminary/Final Drainage Report by Associated Design Professionals, Inc. dated July, 2017.

Clarify who maintains the Extended Detention Basin, All the Swales shown in the tracts the private storm sewer etc. Call out the entity responsible for ownership and maintenance. Also provide this on the Plat.

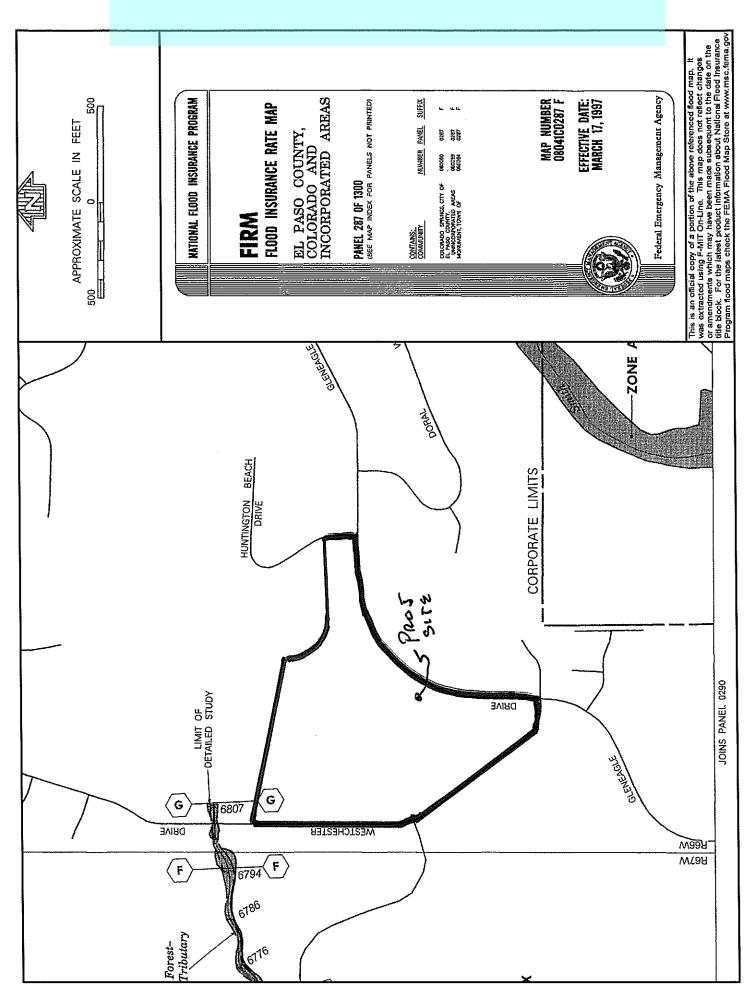
Clarify in the text, that the Roadway and Utility Easement Book 2767 Page 809 will be used as a Public Drainage Easement for the 30 inch storm sewer. Clarify that El Paso County has access to the storm sewer with this easement. **APPENDIX A**

MAPS





Please provide the latest version of the FIRM



APPENDIX B

DESIGN CALCULATIONS

	LE DEVELOP	MENT FILIN	G NO 2			
C FACTOR	CALCULATI	ON SHEET				

EXISTING	CONDITION	S				
RUNOFF (COEFICIENT					
TYPE A/B	SOILS					
LAND USE			5 YR	100 YR		
			······			
UNDEV			0.08	0.35		
STREETS/	DRIVES		0.9	0.96		
ROOFS			0.73	0.81		
	TOTAL	SURFACE C	ONDITION	AREAS	CALCULATE	DC
AREA	AREA	UNDEV	PAVED	ROOFS	5	100
			STREETS	}		
DESIG.	(acre)		& DRIVES		YR	YR
				<u> </u>	i	
A1**	1.66	1.31	0.13	0.22	0.23	0.46
A2**	13.26	13.04		0.22	0.09	0.36
A3	1.07	0.75	0.32		0.33	0.53
A4	1.00	1.00			0.08	0.35
OS1*	6.35	4.76	0.84	0.75	0.27	0.49
OS2*	1.30	0.99	0.14	0.17	0.25	0.48
	e = 2500 sf					
0						
** Ava Hou	se = 3200 sf					
** Avg Hou	se = 3200 sf					
	se = 3200 sf PED CONDIT	IONS				
DEVELOP						·····
DEVELOP RUNOFF	PED CONDIT					
DEVELOP	PED CONDIT COEFICIEN 3 SOILS		5 YR	100 YR		
DEVELOP RUNOFF TYPE A/F	PED CONDIT COEFICIEN 3 SOILS		5 YR	100 YR		
DEVELOP RUNOFF TYPE A/F	PED CONDIT COEFICIEN 3 SOILS		5 YR 0.08			
DEVELOP RUNOFF TYPE A/F LAND USF	PED CONDIT COEFICIEN 3 SOILS			0.35		
DEVELOP RUNOFF TYPE A/E LAND USE	PED CONDIT COEFICIEN 3 SOILS		0.08	0.35		
DEVELOP RUNOFF TYPE A/E LAND USE UNDEV STREETS/	PED CONDIT COEFICIEN 3 SOILS		0.08	0.35		
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A2B**	2.78	2.20	0.28	0.30	0.23	0.46
A2C**	1.82	1.09	0.36	0.37	0.37	0.56
A2D**	4.39	4.17	0.00	0.22	0.11	0.37
A3	1.07	0.75	0.32	0.00	0.33	0.53
A4	1.00	1.00	0.00	0.00	0.08	0.35
OS1*	4.55	3.49	0.60	0.46	0.25	0.48
OS2*	3.10	2.26	0.38	0.46	0.28	0.49
* Avg House	e = 2500 sf				13.26	1.75
** Avg Hous	e = 3200 sf					

Drainage cacoulation sheet file:gleneagle II dr 11/26/18 C5 AREA AREA C5 AREA Area C5 Area 13/26 C5 Area 13/26 C5 Area 13/26 C5 Ara 13/26 C5 Ara 13/26 C5 Ara 13/26 C5 Ara 1.07 C5 Ara 1.07 C5 Ara 1.07 C5 Ara 1.07 C5 Ara 1.00 C5 Ara 1.00 C5 Ara 1.00 C5	0.23													_						
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	0.33	0.53	0.35	10.0	2	2 E0	17.0 1	8	00 V	2.00		10.27	4.01	2.00	6.87	21.77				os1
	0.27	0.49	1.71	3.11	00L	3.3U	17701	-	B,+	8.7		10.61		5.65	6.69	50.79				DP2
		202	2.07	3.68	2	01 0	0 03	500	2 60	1 85	270	11.62		6.63	0.30	2.32	100	1.85	0.90	44
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			0.41	16.0		_					_	12.35	_	K CK		26.30				DP4
			2.47	4.65								70.01		0.02	10.74	17.32				DPS
DP5 24.64			4.05	10.19								23.14		4.03	±	C714				

VELOPED CONDIT			00.0	0.76	50	00 1	7 28	200	_	4 00	2.92	10.20	_	7.02	1.53	5.36				A1
	0.23	0.40	74.0	0.10	3 5	005	2.70	850	4.00	2.00	7.92	15.61	3.31	5.78	1.55	9.13			R	A2A
AZA 4.2/	11.0	10:01	0.41	2.34	3				_			15.61	_	5.78	2.82	13.54				DP1
	0.73	0.46	0.64	1.28	150	5.00	11.72	800	3.00	1.75	7.62	19.33	<u> </u>	5.18	1.90	6.63				A2B
_	}		1.49	3.62								19.33		5.18	4.42	18.77	150	2.00	1.25 E	DP2
	0.37	0.56	0.67	1.02	30	2.00	5.95	250	1.00	1.00	4.17	10.11	4.03	7.04	2.71	7.18			-	AZC
			2.16	4.64								20.58		5.01	6.21	23.26	500	9	3.33	0P3
A2D 4.39	0.11	0.37	0.48	1.62	20	3.50	8.66	350	1.00	1.00	5.83	14.49		5.99	1.66	9./3		101		
			2.65	6.27								23.92	2.64	4.62	00.7	28'92	100 1.55 0.50 D.54 2.55	1.65.1	1 06.0	100 100
14.92			1.06	3.96		Adjusted C Factor for Detention Basin C	stention Bas	<u>د</u>				23.92		4.62	7:20					
			20 1	30.0																
Overflow Pipe assuming clogged outlet structure	ea ourier		07.1	nere																
A3 1.07	0.33	0.53	0.35	0.57	30	2.00	6.27	500	4.00	2.00	4,17	10.44	3.98	6.95	1.40	3.94	600	1.70	5.88 A	A3
-	0.25	0.48	1.14	2.18	100	3.50	10.51	0	4.00	2,00		10.51	_	6.93	4.51	15,13				os1
DP5 5.62			1.49	2.75								16.32			4.82	10.05			<u> </u>	200
DP6 20.54			4.14	9,02							_	23.92	7.04	4.02	10.33	41.04			<u> </u>	
100	80.0	0.35	0.08	0.35	50	3.50	8.92	300	3.50	1.85		11.62		6.63	0.30	2.32	100	1.85	06.0	A4
	0.28	0.49	0.87	1.52	100	3.50	10.14	0	4.00	2.00	0.00	10.14		7.03	3.49	10.68			0	0S2
			0.95	1.87								12.52	3.67	6.41	3.48	11.99				P7
FOREBAY CALCULATIONS		FOREBAY NOTCH CALCULATIONS	OTCH CAL	CULATION	S									_						
2% OF WQV		2% OF 100YR FLOW	R FLOW																	
0.02 X 0.121 = 0.0024 AF = 105 CF		0.02 X 38.8 = 0.78 CFS	- 0.78 CFS											+		T				
		W =Q/(D^1.5XC)	XC)															_		
		W=0.78/(1X3.0)=0.26 FI	3.0)=0.26 F I			{														
												+								

GLENEAGLE DEVELOPMENT												
DITCH CAPACITY CALCULATION SHEET										Riprap		
Swale Location	Q5 cfs	Q100 Cfs	2 %	Bft	Z	D Ét	D ft d100 ft	V fps	Froude #	Size	A sf	Tw ft
	1.7	9.7	1.0	0.0	3:1	1.5	1.0	3.2	0.79		3.2	6.1
X	4.4	18.8	0.5	2.0	4:1	2.0	1.2	2.3	0.49 ECM	ECM	6.7	10.6
	2.8	13.5	1.5	0.0	3:1	1.5	1.1	3.5	0.81		3.5	6.9
Overflow Spillwav M	7.0	28.9	6.5	6.0	3:1	3.0	0.6	5.9	1.47	0.40	4.9	9.7
N	1.2	11.2	3.0	0.0	3:1	1.0	6.0	4.3	1.10 ECM	ECM		
		* <u>H</u>	LEFT Z= 1	I* LEFT Z= 15:1, Right Z= 40:1	Z= 40:1		Riprap Size	ŝe				
			O* LEFT Z=	O* LEFT Z= 5:1, Right Z= 2:1	: Z= 2:1		$D50=((VS^{\circ}0.17)/4.5(2.5-1)^{\circ}0.66))^{2}$	0.17)/4	.5(2.5-1)	^0.66))^2		
			R* LEFT Z=	R* LEFT Z= 6:1, Right Z= 3:1	c Z= 3:1							
Note: In ditches with low velocities & flows but higher Froude Numbers, Erosion Control Mats used in lieu of riprap	cities &	flows but hig	ther Froud	e Numbers,	Erosion C	ontrol N	lats used	in lieu	of riprap			

GLENEAGLE DEVELOPMENT FILING NO 2 DRAINAGE CALCULATION SHEET HGL CALCULATIONS

rlanot t	0100	DC CTA	115 STA	DIA (IN)	Materia	Manning's n	LENGTH (FT)	DS INV		WallT	DS CROWN	US CROWN	US HGL	חסא פר	adoic
		5		()									1 101 60	C 104 J	- FFO C
-	41 G	c	150.5	30	RCP	0.013	150.5	6,781.00	6783.56	0.29	6,783.79	b,/80.35	p,/82.00	7/.00/,0	/TN'N
		>		-					0000				0 701 70	6 700 A1	0,026
, c	116	150 5	328 86	30	RCP	0.013	178.38	6783.56	CZ.88/0	67.0	0,/80.35	0,/31.U4	C/.CO//D	1 74-06/'n	7770
T.7	1 T C		00000											1 405 33	
Currelo	A1 G	32 202	471 55	V-ditch	9" Riorao	0.04	115.34	6788.25	6791.35	,	1	•	D,/3U.1/	0,/33.27	120.0
DWAR		00.070	0017 IL										10001		2000
, ,	0 00	A71 CE	679 54	24	HDPE	0.012	178.38	6791.35	6795.82	0.29	6,793.64	0,/98.11	0,/33.2/	0,/2/,0	C7010
- -	50.1	111111	10.040	1										01 002 7	0000
	0 80	629 54	684 53	74	HDPE	0.012	20	6795.92	6796.5	62.0	6,/98.1/	c/.98/,0	0,/9/.91	0,/30.13	670'0
	707	1													

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

									State of the second			and the second		
		olf Course R	esidential Infil	Project Fil	2									
Basin ID:	Det Basin C			_										
ZONE 3														
100-178	ME1	T	-											
VOLUME EUNY WOCY	1	1		1										
	/	100.70	AR .		Depth Increment =									
PERMANENT ONFIC		OHITIC	•				Optional			-1791.000	Optional			
Pool Example Zone	Configuratio	n (Retention	on Pond)		Stage - Storage	Stage	Override	Length	Width	Area	Override Area (ft*2)	Area	Volume (ft*3)	Volume (ac-ft)
					Description Micropool	(ft)	Stage (ft) 0.00	(ft) 	(ft)	(#*2)	30	(acre) 0.001	(#3)	(ac-n)
Required Volume Calculation Selected BMP Type =	EDB	1			micropoor	-	0.50	-	-	-	4.785	0.109	1,151	0.026
		-									9.525	0.109	4 676	0.107
Watershed Area =	14.92	acres				-	1.00	-	-	-				
Watershed Length =	1,450	ft				-	1.50	-	-	-	19,050	0.437	11,725	0.209
Watershed Slope =	0.025	ft/ft				-	2.00	-	-	-	20,255	0.465	21,539	0.494
Watershed Imperviousness =	15.90%	percent				-	2.50	-	-	-	21,460	0.493	32,170	0.739
Percentage Hydrologic Soil Group A =	0.0%	percent				-	3.00	-	-	-	22,065	0.520	43,201	0.992
Percentage Hydrologic Soil Group B =	100.0%	percent			A SKA DA SA	-	3.50	-	-	-	23,870	0.548	54,835	1.259
Percentage Hydrologic Soil Groups C/D =	0.0%	percent				-	4.00	-	-	-	25,075	0.576	67,071	1.540
Desired WQCV Drain Time =	40.0	hours				-	4.50	-	-	-	26,280	0.603	79,910	1.834
Location for 1-hr Rainfall Depths =						-	5.00	-	-	-	27,485	0.631	93,351	2.143
Water Quality Capture Volume (WQCV) =		acre-feet	Optional Use 1-hr Precipita			-	5.50	-	-	-	28,690	0.659	107,395	2.465
Excess Urban Runoff Volume (EURV) =		acre-feet		-		-	10.000	-	-					\vdash
2-yr Runoff Volume (P1 = 1.19 in.) =	0.173	acre-feet	1.19	inches		-		-	-	-				<u> </u>
5-yr Runoff Volume (P1 = 1.5 in.) =	0.431	acre-feet	1.50	inches		-		-	-	-	1.663.672			
10-yr Runoff Volume (P1 = 1.75 in.) =	0.704	acre-feet	1.75	inches					-		A CONTRACTOR			<u> </u>
25-yr Runoff Volume (P1 = 2 in.) =	1.186	acre-feet	2.00	inches		-		-	-	-	and and a second			
50-yr Runoff Volume (P1 = 2.25 in.) =	1.537	acre-feet	2.25	inches		-		-	-	-				
100-yr Runoff Volume (P1 = 2.52 in.) =	1.949	acre-feet	2.52	inches		-		-	-	-	121123			+
500-yr Runoff Volume (P1 = 3.01 in.) =	2.637	acre-feet	3.01	inches		-		-	-	-	Contraction of the local distribution of the			+
Approximate 2-yr Detention Volume =	0.161	acre-feet				-		-	-					<u> </u>
Approximate 5-yr Detention Volume =	0.354	acre-feet			to the second second second	-		-	-	-				
Approximate 10-yr Detention Volume =		acre-feet				-	5	-	-					
Approximate 25-yr Detention Volume =		acre-feet			And the second second second	-		-	-	-				
Approximate 50-yr Detention Volume =		acre-feet			The second s	-		-	-	-				
Approximate 100-yr Detention Volume =	0.817	acre-feet				2374								
						-		-	-	-		<u> </u>		
Stage-Storage Calculation	0.000	-				-		-	-	-				
Zone 1 Volume (WQCV) =		acre-feet				-	and the second second	-	-	-	1.1.1.1.1.1			
Zone 2 Volume (EURV - Zone 1) =	0.110	acre-feet				-		-	-	-				
Zone 3 Volume (100-year - Zones 1 & 2) =	0.586	acre-feet				-		-	-	-	2.11.			
Total Detention Basin Volume =		acre-feet				100		100 M	10.00	6.255				
Initial Surcharge Volume (ISV) =		ft*3				-			-	-				
Initial Surcharge Depth (ISD) =		ft				-		-	-	-				
Total Available Detention Depth (Htotal)	User	ft				-	S. S. S. S. S. S.	-	-	-				
Depth of Trickle Channel (H _{TC}) =		ft						-	-	-				
Slope of Trickle Channel (S _π) =		ft/ft				-		-	-	-				
Slopes of Main Basin Sides (Smain) =		HIV				-		-	-	-				+
Basin Length-to-Width Ratio (R _{L/W}) =	user					-		-	-	-				
						-			-	-				
Initial Surcharge Area (A _{5v}) =	user	ft*2				-		-	-	-				
Surcharge Volume Length (L _{SV}) =		ft				-		-	-	-			1	+
Surcharge Volume Width (W _{ISV}) = Depth of Basin Floor (H _{FLOOR}) =	user user	ft				-		-	-	-	-		+	+
Depth of Basin Floor (H _{FLOOR}) = Length of Basin Floor (L _{FLOOR}) =	user	R				-		-	-	-	1000		+	+
		ft				-		-	-	-	1.			+
Width of Basin Floor (W _{FLOOR}) = Area of Basin Floor (A _{FLOOR}) =		ft				-	-	-	-	-	-			+
Volume of Basin Floor (V _{FLOOR}) =	user	ft*2 ft*3				-		-	-	-			+	+
Depth of Main Basin (H _{MAIN})						-		-	-	-			1	+
Length of Main Basin (LMAIN)		ft ft				-		-	-	-	1.111	1	1	-
Width of Main Basin (UMAN)	= User	ft				-	1000	-	-	-	1111111		+	+
Area of Main Basin (Aman)		ft*2			-	-	NO STANK	-	-	-		1	1	1
Volume of Main Basin (V _{MAIN})		ft*3				-	Sec. 1	-	-	-	12.3281.01			
Calculated Total Basin Volume (Vtetal)		acre-feet			adama a shared	-		-	-	-				
									-	-	1000000000			
						-		-	-	-				+
						-		-	-	-	AND DO			
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						-		-	-	-			-	+
						-		-	-	-	No Discover			
						-	1 1 1 1 1 1 1	-	-	-		-	-	
						-		-	-	-	1000		+	+
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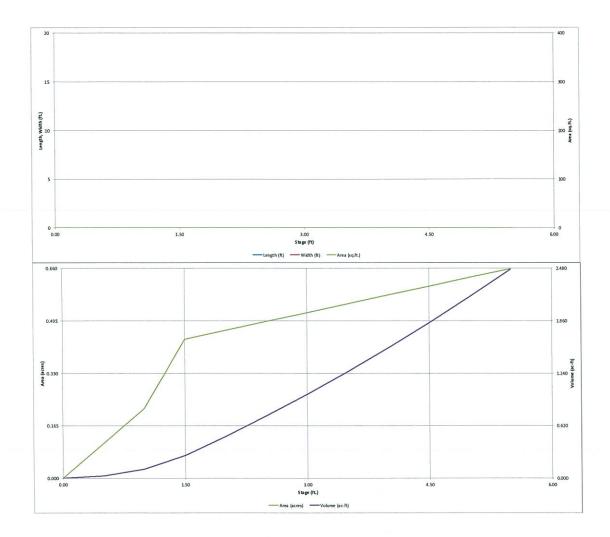
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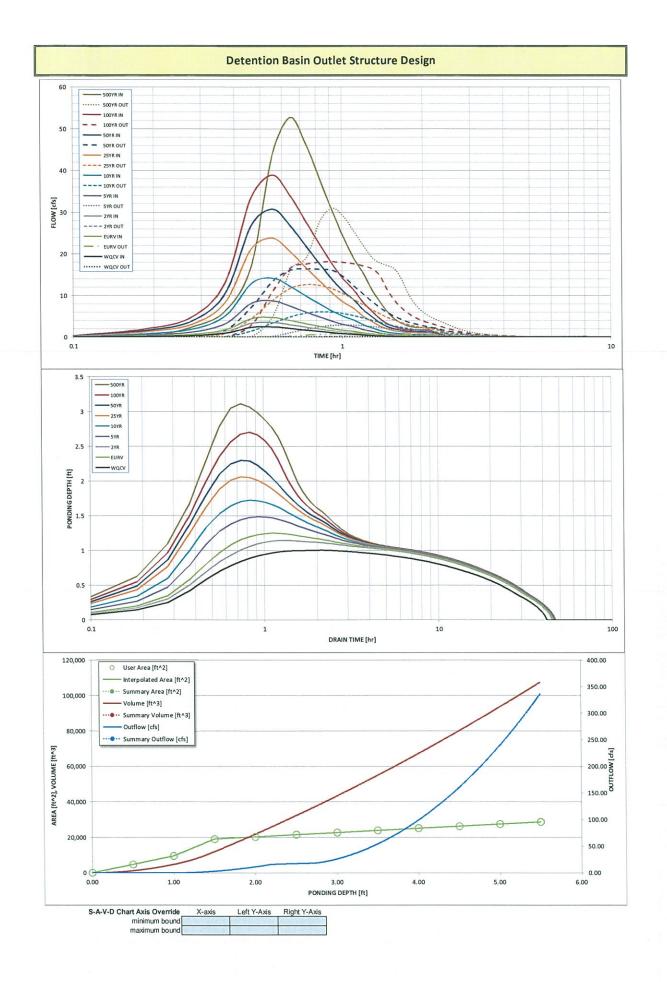
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DETENTION BASIN STAGE-STORAGE TABLE BUILDER



Detention Basin Outlet Structure Design									
Project:	Gleneagle Golf Cour	se Infill Project Fil 2							
	Det Basin C								
ZONE 3									
100-YR ZONE 1				Stage (ft)	Zone Volume (ac-ft)	Outlet Type			
VOLUME EURY WOCY			Zone 1 (WQCV)	1.06	0.121	Orifice Plate			
	100-YEAR ORIFICE		Zone 2 (EURV)	1.40	0.110	Orifice Plate			
PERMANENT ORIFICES	UNIFICE		Zone 3 (100-year)	2.66	0.586	Weir&Pipe (Restrict)			
POOL Example Zone C	Configuration (Rete	ention Pond)			0.817	Total			
User Input: Orifice at Underdrain Outlet (typically us	ed to drain WQCV in	a Filtration BMP)				Calculate	d Parameters for Un	derdrain	
Underdrain Orifice Invert Depth =	N/A	ft (distance below th	e filtration media sur	face)	Unde	rdrain Orifice Area =	N/A	ft ²	
Underdrain Orifice Diameter =	N/A	inches			Underdra	in Orifice Centroid =	N/A	feet	
User Input: Orifice Plate with one or more orifices o Invert of Lowest Orifice =							ated Parameters for		
Depth at top of Zone using Orifice Plate =		ft (relative to basin b ft (relative to basin b				ifice Area per Row = liptical Half-Width =		ft ² feet	
Orifice Plate: Orifice Vertical Spacing =		inches	ottom at otage - o it			tical Slot Centroid =		feet	
Orifice Plate: Orifice Area per Row =		sq. inches (diameter	= 1-1/16 inches)			Elliptical Slot Area =		ft ²	
User Input: Stage and Total Area of Each Orifice R		T							1
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row7 (optional)	Row 8 (optional)	
Stage of Orifice Centroid (ft)	0.00	0.34	0.69						
Orifice Area (sq. inches)	0.86	0.86	0.86	and the second			and the second	AND DECKOPSING.	1
1	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	1
Stage of Orifice Centroid (ft)		(optional)	(optional)	(optional)	(optional)	(optional)	(optional)		
Orifice Area (sq. inches)	A State of the sta		Constant and the	Parent States of Astron			Start Start Start	Service Street	1
User Input: Vertical Orifice (Circ						Calculated	Parameters for Vert	tical Orifice	
	Not Selected	Not Selected					Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A		oottom at Stage = 0 fi	5	ertical Orifice Area =	N/A	N/A	ft ²
Depth at top of Zone using Vertical Orifice = Vertical Orifice Diameter =	N/A N/A		N/A ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Centroid = N/A N/A inches						feet
Vertical Office Diameter -	N/A	N/A	menes						
User Input: Overflow Weir (Dropbox) and G	irate (Flat or Sloped)					Calculated	Parameters for Ove	rflow Weir	
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =		N/A	ft (relative to basin bo	ottom at Stage = 0 ft)		rate Upper Edge, H _t =	2.03	N/A	feet
Overflow Weir Front Edge Length =	4.00	N/A	feet		Over Flow	Weir Slope Length =			
Overflow Weir Slope =	4.00	N/A			- · · · · ·	· · · · · · · · · · · · · · · · · · ·	4.12	N/A	feet
Horiz Longth of Wair Sides -		and the second se	H:V (enter zero for fl	at grate)		100-yr Orifice Area =	4.57	N/A	should be ≥ 4
Horiz. Length of Weir Sides = Overflow Grate Open Area % =	4.00	N/A	feet		Overflow Grate Ope	100-yr Orifice Area = en Area w/o Debris =	4.57 11.54	N/A N/A	should be ≥ 4 ft ²
Horiz. Length of Weir Sides = Overflow Grate Open Area % = Debris Clogging % =		and the second se	a for the second second second second		Overflow Grate Ope	100-yr Orifice Area =	4.57	N/A	should be ≥ 4
Overflow Grate Open Area % =	4.00 70%	N/A N/A	feet %, grate open area/		Overflow Grate Ope	100-yr Orifice Area = en Area w/o Debris =	4.57 11.54	N/A N/A	should be ≥ 4 ft ²
Overflow Grate Open Area % = Debris Clogging % =	4.00 70% 50%	N/A N/A N/A	feet %, grate open area/ %		Overflow Grate Op Overflow Grate O	100-yr Orifice Area = en Area w/o Debris = pen Area w/ Debris =	4.57 11.54	N/A N/A N/A	should be≥4 ft² ft²
Overflow Gate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (C	4.00 70% 50% ircular Orifice, Restri Zone 3 Restrictor	N/A N/A N/A ctor Plate, or Rectan Not Selected	feet %, grate open area/ %		Overflow Grate Op Overflow Grate O	100-yr Orifice Area = en Area w/o Debris = pen Area w/ Debris = Calculated Paramete	4.57 11.54 5.77 rs for Outlet Pipe w/ Zone 3 Restrictor	N/A N/A N/A Flow Restriction Pla Not Selected	should be ≥4 ft ² ft ²
Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (C Depth to Invert of Outlet Pipe =	4.00 70% 50% ircular Orifice, Restri Zone 3 Restrictor 0.33	N/A N/A N/A ctor Plate, or Rectan Not Selected N/A	feet %, grate open area/ % gular Orifice) ft (distance below ba		Overflow Grate Op Overflow Grate O Overflow Grate O	100-yr Orifice Area = en Area w/o Debris = pen Area w/ Debris = Calculated Paramete Outlet Orifice Area =	4.57 11.54 5.77 rs for Outlet Pipe w/ Zone 3 Restrictor 2.53	N/A N/A N/A Flow Restriction Pla Not Selected N/A	should be ≥ 4 ft ² ft ² te ft ²
Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (C Depth to Invert of Outlet Pipe = Outlet Pipe Diameter =	4.00 70% 50% ircular Orifice, Restri Zone 3 Restrictor 0.33 24.00	N/A N/A N/A ctor Plate, or Rectan Not Selected	feet %, grate open area/ % gular Orifice) ft (distance below ba inches	total area sin bottom at Stage = (Overflow Grate Op Overflow Grate O Overflow Grate O () ft) Out	100-yr Orifice Area = en Area w/o Debris = pen Area w/ Debris = Calculated Paramete Outlet Orifice Area = let Orifice Centroid =	4.57 11.54 5.77 rs for Outlet Pipe w/ Zone 3 Restrictor 2.53 0.83	N/A N/A N/A Flow Restriction Pla Not Selected N/A N/A	should be ≥ 4 ft ² ft ² te ft ² ft ²
Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (C Depth to Invert of Outlet Pipe =	4.00 70% 50% ircular Orifice, Restri Zone 3 Restrictor 0.33 24.00	N/A N/A N/A ctor Plate, or Rectan Not Selected N/A	feet %, grate open area/ % gular Orifice) ft (distance below ba	total area sin bottom at Stage = (Overflow Grate Op Overflow Grate O Overflow Grate O	100-yr Orifice Area = en Area w/o Debris = pen Area w/ Debris = Calculated Paramete Outlet Orifice Area = let Orifice Centroid =	4.57 11.54 5.77 rs for Outlet Pipe w/ Zone 3 Restrictor 2.53 0.83	N/A N/A N/A Flow Restriction Pla Not Selected N/A	should be ≥ 4 ft ² ft ²
Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (C Depth to Invert of Outlet Pipe = Outlet Pipe Diameter =	4.00 70% 50% ircular Orifice, Restri Zone 3 Restrictor 0.33 24.00 18.00	N/A N/A N/A ctor Plate, or Rectan Not Selected N/A	feet %, grate open area/ % gular Orifice) ft (distance below ba inches	total area sin bottom at Stage = (Overflow Grate Op Overflow Grate O Overflow Grate O () ft) Out	100-yr Orifice Area = en Area w/o Debris = pen Area w/ Debris = Calculated Paramete Outlet Orifice Area = let Orifice Centroid = rictor Plate on Pipe =	4.57 11.54 5.77 rs for Outlet Pipe w/ Zone 3 Restrictor 2.53 0.83	N/A N/A N/A Flow Restriction Pla Not Selected N/A N/A N/A	should be \geq 4 ft ² ft ² te ft ² ft ²
Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (C Depth to Invert of Outlet Pipe Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert =	4.00 70% 50% ircular Orifice, Restri Zone 3 Restrictor 0.33 24.00 18.00 gular or Trapezoidal)	N/A N/A N/A ctor Plate, or Rectan Not Selected N/A	feet %, grate open area/ % gular Orifice) ft (distance below ba inches inches	total area sin bottom at Stage = 0 Half-	Overflow Grate Op Overflow Grate O Overflow Grate O Overflow Grate O Overflow Grate Overflow Grate Central Angle of Rest	100-yr Orifice Area = en Area w/o Debris = pen Area w/ Debris = Calculated Paramete Outlet Orifice Area = let Orifice Centroid = rictor Plate on Pipe =	4.57 11.54 5.77 rs for Outlet Pipe w/ Zone 3 Restrictor 2.53 0.83 2.09	N/A N/A N/A Flow Restriction Pla Not Selected N/A N/A N/A	should be \geq 4 ft ² ft ² te ft ² ft ²
Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (C Depth to Invert of Outlet Pipe Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectang	4.00 70% 50% ircular Orifice, Restri Zone 3 Restrictor 0.33 24.00 18.00 gular or Trapezoidal) 2.70	N/A N/A N/A ctor Plate, or Rectan Not Selected N/A N/A	feet %, grate open area/ % gular Orifice) ft (distance below ba inches inches	total area sin bottom at Stage = 0 Half-	Overflow Grate Op Overflow Grate Op Overflow Grate Op Off) Out Central Angle of Rest Spillway	100-yr Orifice Area = en Area w/o Debris = pen Area w/ Debris = Calculated Paramete Outlet Orifice Area = let Orifice Centroid = rictor Plate on Pipe = Calcula	4.57 11.54 5.77 rs for Outlet Pipe w/ Zone 3 Restrictor 2.53 0.83 2.09 ated Parameters for 1	N/A N/A N/A Flow Restriction Pla Not Selected N/A N/A N/A Spillway	should be ≥ 4 ft ² ft ² te ft ² ft ²
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Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (C Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectang Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) Calculated Runoff Volume (acre-ft) Inflow Hydrograph Volume (acre-ft) Predevelopment Unit Peak Row, q (cfs/acre) Predevelopment Qets Across Predevelopment Qets Routed Notflow Q (cfs) Peak Outflow Q (cfs) Ratio Peak Outflow To Predevelopment Q Structure Controlling Flows Max Velocity through Grate 2 (fps) Time to Drain 97% of Inflow Volume (fours) = Time to Drain 97% of Inflow Volume (fours)	4.00 70% 50% ircular Orifice, Restri Zone 3 Restrictor 0.33 24.00 18.00 gular or Trapezoidal) 2.70 13.00 4.00 4.00 0.53 0.121 0.00 0.53 0.121 0.00 0.00 0.00 0.121 0.121 0.00 0.121 0.121 0.00 0.121 0	N/A N/A N/A N/A Not Selected N/A N/A N/A It (relative to basin l feet H:V feet URV 1.07 0.231 0.00 0.01 0.231 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.01 0.0231 0.00 0.00 0.01 0.0231 0.0231 0.03 0.04.6 0.9 N/A 38 42	feet %, grate open area/ % gular Orifice) ft (distance below bas inches inches bottom at Stage = 0 ft 0.01 0.172 0.01 0.173 0.01 0.2 3.5 0.4 N/A 0.9 0.174 0.02 N/A 39 42	total area sin bottom at Stage = 0 Half- t) 5 Year 1.50 0.431 0.430 0.17 2.5 8.6 2.8 1.1 0.2 N/A 34 40	Overflow Grate Op Overflow Grate Op Overflow Grate Op Off) Out Central Angle of Rest Spillway Stage a Basin Area a Basin Area a Basin Area a Overflow Grate 1 Overflow Grate 1	100-yr Orifice Area = en Area w/o Debris = pen Area w/o Debris = Calculated Paramete Outlet Orifice Area = let Orifice Centroid = rictor Plate on Pipe = Calcula / Design Flow Depth= at Top of Freeboard = at Top of Freeboard = at Top of Freeboard = 1.184 0.79 1.1.7 1.2.5 1.1 Overflow Grate 1 1.1 N/A 24 35	4.57 11.54 5.77 rs for Outlet Pipe w/ Zone 3 Restrictor 2.53 0.83 2.09 Ated Parameters for 3 0.87 4.57 0.61 50 Year 2.25 1.537 1.536 1.02 15.2 30.7 16.3 1.1 Outlet Plate 1 1.4 N/A 21 33	N/A N/A N/A N/A Not Selected N/A N/A N/A Spillway feet acres 100 Year 2.52 1.949 1.948 1.30 19.4 38.8 18.0 0.9 Spillway 1.6 N/A 31	should be ≥ 4 ft ² ft ² ft ² feet radians
Overflow Grate Open Area % = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (C Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectang Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = Calculated Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Unit Peak Flow, q (cfs/acre) = Predevelopment Verlar Plow q (cfs) = Ratio Peak Outflow to Predevelopment Q Structure Controlling Flow = Max Velocity through Grate 1 (ps) = Max Velocity through Grate 2 (ps) Time to Drain 97% of Inflow Volume (tours)	4.00 70% 50% solutions soluti	N/A N/A N/A N/A N/A Selected N/A N/A ft (relative to basin l feet H:V feet EURV 1.07 0.231 0.245	feet %, grate open area/ % gular Orifice) ft (distance below bas inches inches bottom at Stage = 0 f 2 Year 1.19 0.173 0.172 0.01 0.2 3.5 0.4 N/A Overflow Grate 1 0.02 N/A 39	total area total area Half- t) 5 Year 1.50 0.431 0.430 0.17 2.5 8.6 2.8 1.1 Overflow Grate 1 0.2 N/A 34	Overflow Grate Op Overflow Grate Op Overflow Grate Op Off) Out Central Angle of Rest Spillway Stage a Basin Area a Basin Area a 10 Year 1.75 0.704 0.703 0.34 5.1 14.1 6.0 1.2 Overflow Grate 1 0.5 N/A 30	100-yr Orifice Area = en Area w/o Debris = pen Area w/o Debris = calculated Paramete Outlet Orifice Area = let Orifice Centroid = rictor Plate on Pipe = Calcula v Design Flow Depth= at Top of Freeboard = at Top of Freeboard = 25 Year 2.00 1.186 1.184 0.79 11.7 2.3.7 12.5 1.1 Overflow Grate 1 1.1 N/A 24	4.57 11.54 5.77 rs for Outlet Pipe w/ Zone 3 Restrictor 2.53 0.83 2.09 nted Parameters for 1 0.87 4.57 0.61 1.537 1.536 1.02 15.2 30.7 16.3 1.1 Outlet Plate 1 1.4 N/A 2.1	N/A N/A N/A N/A NA Spillway feet feet acres	should be ≥ 4 ft ² ft ² fcet radians



Detention Basin Outlet Structure Design

Outflow Hydrograph Workbook Filename:

	SOURCE	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK	WORKBOOK
ime Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs
5.55 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00 11111	0:05:33	THE PARAMAN PROPERTY	340352249932225394	AND A DESCRIPTION OF A	Chronic Handwood	Statement of the state	Constraint Party Mathematics	A LOCAL DATE OF STREET, STREET	Contraction of the local sectors of the local secto	100000000000000000000000000000000000000
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ydrograph	0:11:06	0.14	0.27	0.20	0.48	0.75	1.21	1.52	1.86	2.39
Constant 0.900	0:22:12	0.34	0.64	0.48	1.16	1.85 5.11	3.03 8.32	3.86	4.81	6.35 17.26
0.900	0:27:45	2.35	1.76	1.32	8.07	12.87	21.02	26.76	33.30	43.85
	0:33:18	2.35	4.42	3.32 3.46	8.65	12.87	23.69	30.68	38.85	43.83
	0:38:51	2.44	And a reading of the second second	2.90	7.30	12.00	20.38	26.56	33.85	46.15
	0:44:24	1.62	3.90 3.12	2.30	5.87	9.68	16.53	20.50	27.59	37.67
	0:49:57	1.30	2.51	1.86	4.71	7.76	13.24	17.29	22.07	30.11
	0:55:30	1.01	1.96	1.45	3.69	6.10	10.43	13.64	17.44	23.82
2	1:01:03	0.80	1.55	1.15	2.92	4.84	8.27	10.81	13.81	18.84
	1:06:36	0.67	1.29	0.96	2.43	3.99	6.78	8.82	11.23	15.27
	1:12:09	0.47	0.91	0.68	1.73	2.86	4.91	6.43	8.24	11.31
	1:17:42	0.36	0.69	0.51	1.30	2.15	3.67	4.80	6.14	8.38
	1:23:15	0.24	0.47	0.35	0.90	1.49	2.57	3.37	4.32	5.94
	1:28:48	0.18	0.35	0.26	0.65	1.08	1.86	2.43	3.11	4.24
	1:34:21	0.14	0.27	0.20	0.51	0.84	1.44	1.88	2.40	3.28
	1:39:54	0.12	0.22	0.17	0.42	0.69	1.18	1.53	1.95	2.66
	1:45:27	0.10	0.20	0.15	0.38	0.62	1.04	1.35	1.72	2.33
	1:51:00	0.10	0.19	0.14	0.36	0.59	0.99	1.29	1.64	2.22
	1:56:33	0.10	0.19	0.14	0.35	0.58	0.97	1.26	1.60	2.17
	2:02:06	0.10	0.19	0.14	0.35	0.58	0.97	1.26	1.60	2.17
	2:07:39	0.10	0.19	0.14	0.35	0.58	0.97	1.26	1.60	2.17
	2:13:12	0.06	0.12	0.09	0.22	0.37	0.64	0.85	1.09	1.51
	2:18:45	0.03	0.07	0.05	0.13	0.22	0.38	0.50	0.64	0.89
	2:24:18	0.02	0.04	0.03	0.07	0.12	0.21	0.28	0.37	0.51
	2:29:51	0.01	0.02	0.02	0.04	0.07	0.12	0.15	0.20	0.28
	2:35:24	0.00	0.01	0.01	0.02	0.03	0.06	0.08	0.10	0.14
	2:40:57	0.00	0.00	0.00	0.01	0.01	0.02	0.02	0.03	0.04
	2:46:30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:52:03	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:57:36	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:03:09	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:08:42	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:14:15	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:19:48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:21	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:54	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:36:27	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:42:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:47:33	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:53:06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:58:39	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:04:12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:09:45	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:18	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:51	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:26:24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:31:57	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:37:30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:43:03	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:48:36	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:54:09 4:59:42	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:15	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:48	0,00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:16:21	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:21:54	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:27:27 5:33:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:38:33	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:44:06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:49:39	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:45	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:06:18	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:17:24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:22:57	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:28:30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:34:03	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Storm Inflow Hydrographs

Detention Basin Outlet Structure Design

ne user should graphically co	1				-	m it captures all Total	key transition points.
Stage - Storage Description	Stage [ft]	Area [ft^2]	Area [acres]	Volume [ft^3]	Volume [ac-ft]	Outflow [cfs]	
A CONTRACTOR							For best results, include the
							stages of all grade slope
	The second second						changes (e.g. ISV and Floor) from the S-A-V table on
							Sheet 'Basin'.
							Also include the inverts of all
							outlets (e.g. vertical orifice,
							overflow grate, and spillway, where applicable).
							where applicable).
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	REAL PROPERTY						_
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	Impervious	2-γ	ear	5-y	ear	10-1	year	25-y	ear	50 - y	'ear	100-1	year
		HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D	HSG A&B	HSG C&D
usiness													i
Commercial Areas	95	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.87	0.87	0.88	0.88	0.89
Neighborhood Areas	70	0.45	0.49	0.49	0.53	0.53	0.57	0.58	0.62	0.60	0.65	0.62	0.68
Residential		1											
1/8 Acre or less	65	0.41	0.45	0.45	0.49	0,49	0.54	0.54	0.59	0.57	0.62	0.59	0.65
1/4 Acre	40	0,23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.45	0.54	0,50	0.58
1/3 Acre	30	0.18	0.22	0.25	0.30	0.32	0.38	0.39	0.47	0.43	0.52	0.47	0.57
1/2 Acre	25	0.15	0.20	0.22	0.28	0.30	0.36	0.37	0.45	0.41	0.51	0.46	0.56
1 Acre	20	0.12	0.17	0.20	0.26	0.27	0.34	0.35	0,44	0,40	0.50	0.44	0.55
Industrial				<u> </u>	1	<u> </u>			1				
Ught Areas	80	0.57	0.50	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
Heavy Areas	90	0.71	0.73	0.73	0.75	0.75	0.77	0.78	0.80	0.80	0.82	0.81	0.83
Parks and Cerneteries	7	0.05	0.09	0.12	0.19	0.20	0.29	0.30	0.40	0.34	0.46	0.39	0.52
Playgrounds	13	0.07	0.13	0.16	0.23	0.24	0.31	0.32	0.42	0.37	0.48	0.41	0.54
Railroad Yard Areas	40	0.23	0.28	0.30	0.35	0.36	0.42	0.42	0.50	0.46	0.54	0.50	0.58
Undeveloped Areas													+
Historic Flow Analysis- Greenbelts, Agriculture	2	0.03	0.05	0.09	0.16	0.17	0.25	0.26	0.38	0.31	0.45	0.36	0.51
Pasture/Meadow	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Forest	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	0.35	0.50
Exposed Rock	100	0.89	0.89	0.90	0.90	0.92	0.92	0.94	0.94	0.95	0.95	0.96	0.96
Offsite Flow Analysis (when landuse is undefined)	45	0.26	0.31	0.32	0.37	0,38	0.44	0.44	0.51	0.48	0.55	0.51	0.59
Streets													
Paved	100	0.89	0.89	0.90	0.90	0.92	0,92	0.94	0.94	0.95	0.95	0.96	0.96
Gravel	80	0.57	0.60	0.59	0.63	0.63	0.66	0.66	0.70	0.68	0.72	0.70	0.74
en a di astronomia										_			
Drive and Walks	100	0.89	0.89	0.90									
Roofs	90	0.71	0.73	0.73									0.8
Lawns	0	0.02	0.04	0.08	0.15	0.15	0.25	0.25	0.37	0.30	0.44	1 0.35	0.5

Table 6-6. Runoff Coefficients for Rational Method(Source: UDFCD 2001)

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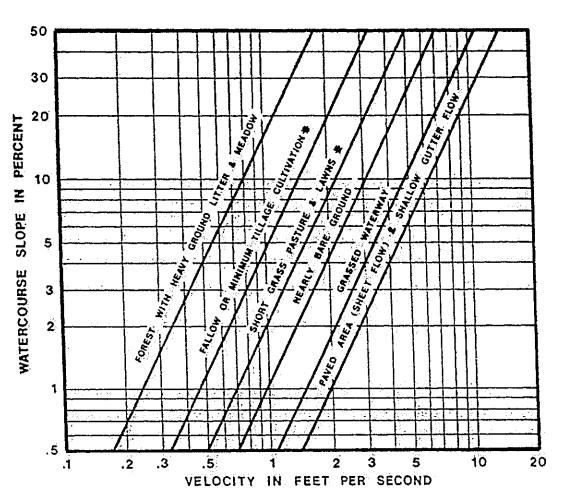


Figure 6-25. Estimate of Average Concentrated Shallow Flow

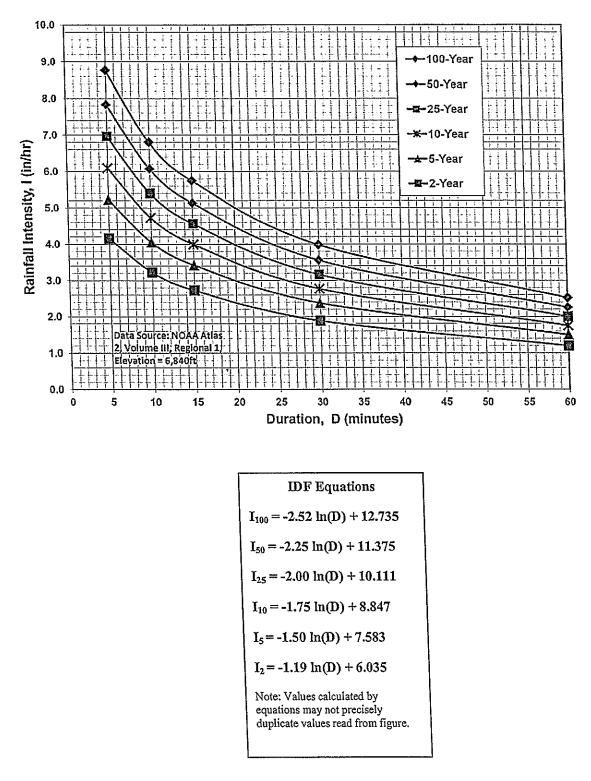
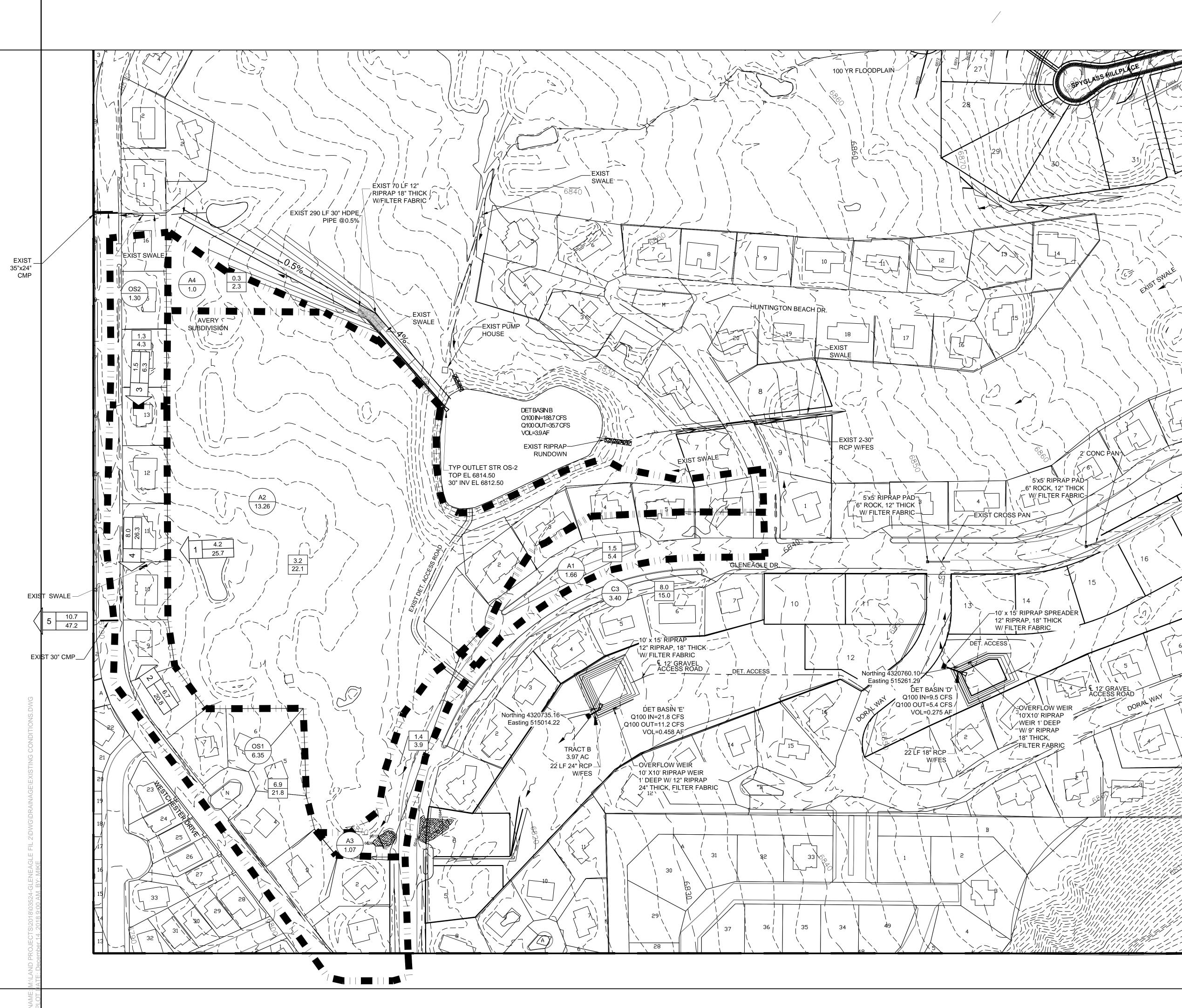
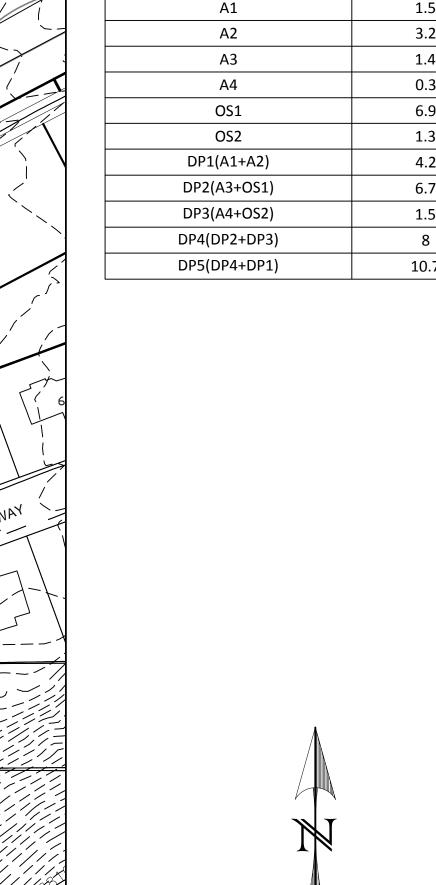


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency



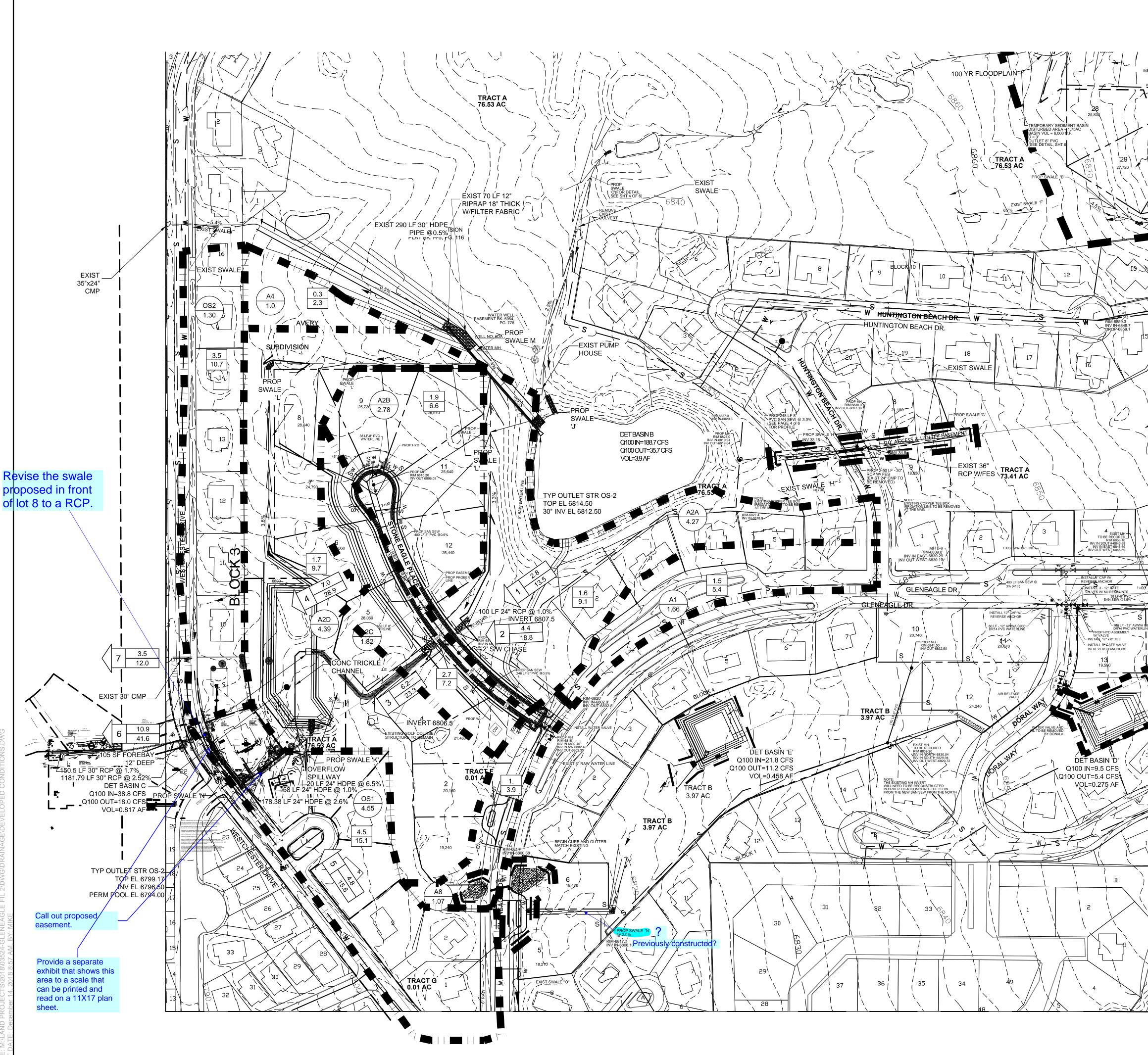
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	Know what's below. Call before you dig. PROJ NO. 03524 DWG NM. 03524-Dev-Fil2
5	Guman & Associates, LLC 731 N Weber St, Suite 10 COLORADO SPRINGS, CO. 80903
	GLENEAGLE SUBDIVISION, FIL #2
	EXISTING CONDITIONS
	DRAWING NUMBER: C SHEET 1

TABLE 1 – EX	ISTING CONDITIONS	
Sub-Basin	Q5CFS	Q100 CFS
A1	1.5	5.4
A2	3.2	22.1
A3	1.4	3.9
A4	0.3	2.3
OS1	6.9	21.8
OS2	1.3	4.3
DP1(A1+A2)	4.2	25.7
DP2(A3+OS1)	6.7	20.8
DP3(A4+OS2)	1.5	6.3
DP4(DP2+DP3)	8	26.3
DP5(DP4+DP1)	10.7	47.2
	•	



GRAPHIC SCALE

(IN FEET) 1 inch = 100 ft.





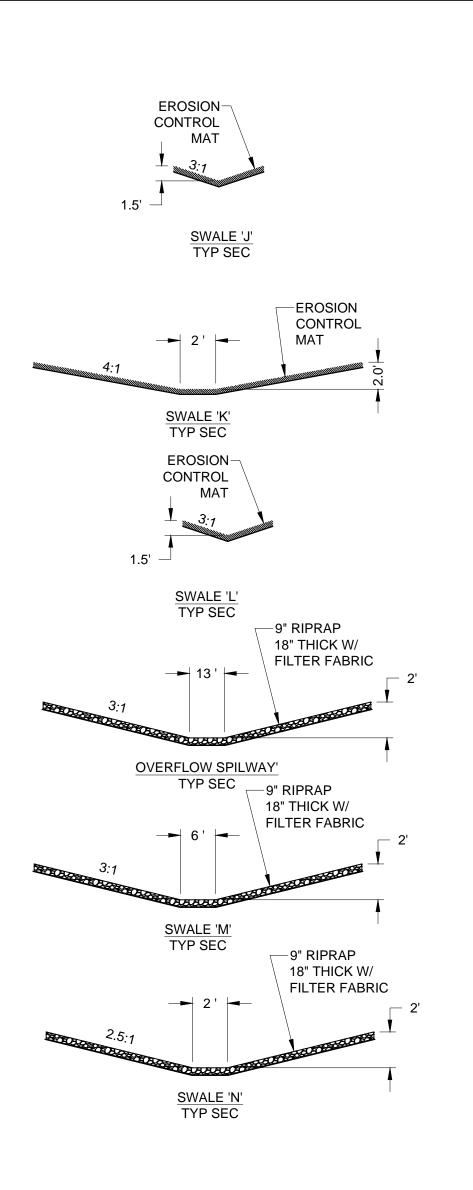
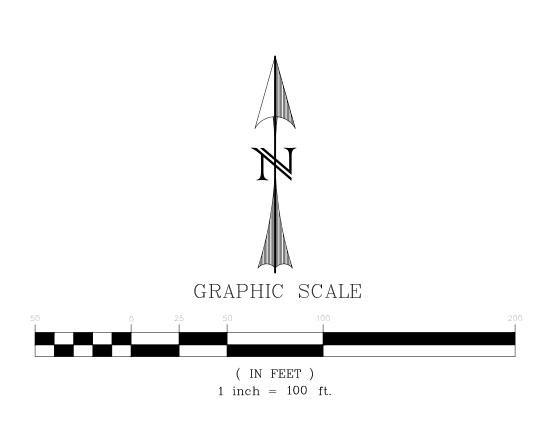
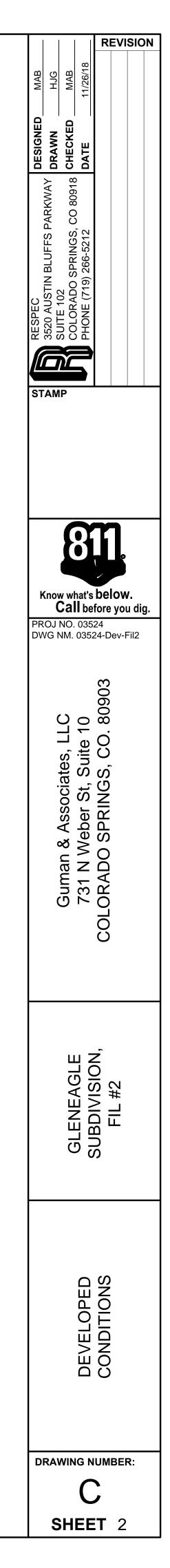


TABLE 2 – DEV	/ELOPED CONDITIONS	
Sub-Basin	Q5CFS	Q100 CFS
OS1	4.5	15.1
OS2	3.5	10.7
A1	1.5	5.4
A2A	1.6	9.1
A2B	1.9	6.6
A2C	2.7	7.2
A2D	1.7	9.7
A3	1.4	3.9
A4	0.3	2.3
DP1 (A1+A2A)	2.8	13.5
DP2 (DP1+A2B)	4.4	18.8
DP3 (DP2+A2B)	6.2	23.3
DP4 (DP3+A4B)	7	28.9
DP5 (OS1+A3)	4.8	15.6
DP6 (DP4+DP5)	10.9	41.6
DP7 (OS2+A4)	3.5	12





Markup Summary

Steve Kuehster	(21)	
Revise the swale proposed in front of lot 8 to a RCP.	Subject: text box Page Label: 30 Author: Steve Kuehster Date: 1/28/2019 10:41:08 AM Color:	Revise the swale proposed in front of lot 8 to a RCP.
	Subject: arrow & box Page Label: 30 Author: Steve Kuehster Date: 1/28/2019 10:43:53 AM Color:	Call out proposed easement.
	Subject: arrow & box Page Label: 30 Author: Steve Kuehster Date: 1/28/2019 11:28:33 AM Color:	Provide a separate exhibit that shows this area to a scale that can be printed and read on a 11X17 plan sheet.
	Page Label: 4 Author: Steve Kuehster Date: 1/28/2019 11:47:50 AM	
rea produces ^{I.} Northern? e. It produces m These flows	Subject: text box Page Label: 4 Author: Steve Kuehster Date: 1/28/2019 11:48:27 AM Color:	Northern?
PROD SWALE TN 92,005 RIM-6917.3 INV IN-6505.10	Subject: Highlight Page Label: 30 Author: Steve Kuehster Date: 1/28/2019 12:29:21 PM Color:	
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Jennifer Irvine P.E. County Engi / ECM Administrator. Conditions:	Subject: text box Page Label: 2 Author: Steve Kuehster Date: 1/29/2019 1:05:27 PM Color:	/ ECM Administrator.
Previous a	Subject: text box Page Label: 30 Author: Steve Kuehster Date: 1/29/2019 1:09:38 PM Color:	Previously constructed?
	Subject: Arrow Page Label: 30 Author: Steve Kuehster Date: 1/29/2019 1:11:06 PM Color:	
A the strate the the the the the the the the the t	Subject: text box Page Label: 6 Author: Steve Kuehster Date: 1/29/2019 12:33:12 PM Color:	Please call out the arrangement for Lot 7 to have the Private 24 inch HDPE Pipe. Is there a Drainage easement granted. Identify the owner and maintainer of the easement.
	Subject: text box Page Label: 13 Author: Steve Kuehster Date: 1/29/2019 12:34:29 PM Color:	Please provide the latest version of the FIRM

 a.g., and a set of the set of t	Subject: text box Page Label: 9 Author: Steve Kuehster Date: 1/29/2019 12:44:06 PM Color:	Clarify who maintains the Extended Detention Basin, All the Swales shown in the tracts the private storm sewer etc. Call out the entity responsible for ownership and maintenance. Also provide this on the Plat.
 A start and an and a start of the start of t	Subject: text box Page Label: 9 Author: Steve Kuehster Date: 1/29/2019 12:48:29 PM Color:	Clarify in the text, that the Roadway and Utility Easement Book 2767 Page 809 will be used as a Public Drainage Easement for the 30 inch storm sewer. Clarify that El Paso County has access to the storm sewer with this easement.
VR-18-018	Subject: text box Page Label: 1 Author: Steve Kuehster Date: 1/29/2019 12:54:56 PM Color:	VR-18-018