# DHIC Falcon Master Traffic Impact Study 

(LSC \#S224400)


## Traffic Engineer's Statement

This traffic report and supporting information were prepared under my responsible charge and they comport with the standard of care. So far as is consistent with the standard of care, said report was prepared in general conformance with the criteria established by the County for traffic reports.


## Developer's Statement

I, the Developer, have read and will comply with all commitments made on my behalf within this report.


# DHIC Falcon 

## Master Traffic Impact Study

Prepared for:<br>Brandon Hoch<br>DHI Communities, a D.R. Horton Company<br>9555 Kingston Ct<br>Englewood, CO 80112

AUGUST 4, 2022

LSC Transportation Consultants, Inc.
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RE: DHIC Falcon<br>El Paso County, CO<br>Master Traffic Impact Study<br>LSC \#S224400

Dear Mr. Hoch,

LSC Transportation Consultants, Inc. has prepared this Master Traffic Impact Study for the DHIC Falcon residential development with 214 single-family-attached dwelling units in El Paso County, CO. Located generally northeast of the intersection of Eastonville Road/Judge Orr Road (El Paso County parcel ID 4232302003), the 13.72 -acre site is currently vacant. Access to the site is proposed to Judge Orr Road (south access) and Eastonville Road (west access). No direct access is proposed to US Highway 24 (US 24). This report has been prepared for submittal to El Paso County.

Note: LSC previously completed a traffic study for this site, dated February 5, 2021 (PCD File No. SKP203). The land use studied in that report was commercial.

## REPORT CONTENTS

The preparation of this report included the following:

- An inventory of existing roadway and traffic conditions on major thoroughfares adjacent to the site, including surface conditions, functional classification, widths, pavement markings, traffic-control signs, posted speed limits, intersection and access spacing, roadway and intersection alignments, roadway grades, and auxiliary turn lanes;
- Weekday peak-hour turning-movement traffic counts at the intersections of Judge Orr Road/Meridian Ranch Road/Eastonville Road and US 24/Judge Orr Road;
- Estimated average weekday traffic (AWT) volumes adjacent to the proposed development on Judge Orr Road, Eastonville Road, Meridian Ranch Road, and US 24;
- Projections of 20-year background traffic volumes on Judge Orr Road, Eastonville Road, Meridian Ranch Road, and US 24;
- The proposed site land use and access plan;
- Estimates of average weekday and weekday peak-hour trip generation for the proposed development and the estimated directional distribution of site-generated vehicle trips on roadways and intersections adjacent to and in the vicinity of the site;
- Projected site-generated and resulting total peak-hour intersection traffic volumes at the following study-area intersections: Judge Orr Road/Meridian Ranch Road/Eastonville Road and US 24/Judge Orr Road;
- Projected total daily and peak-hour traffic volumes at the study-area intersections;
- Intersection level of service (LOS) analysis at the study-area intersections;
- Evaluation of short- and long-term projected intersection volumes to determine potential requirements for any auxiliary right-/left-turn lanes at the proposed site access points, based on the criteria in El Paso County's Engineering Criteria Manual (ECM). Also included are potential long-term lane requirements; and
- Findings and recommendations for submittal to El Paso County.


## LIST OF OTHER TRAFFIC REPORTS USED IN THE PREPARATION OF THIS REPORT

The following previously-completed traffic reports are located adjacent to the proposed Judge Orr Eastonville Commercial Center and were used to provide reference and background information

- "Meadowlake Ranch" - dated May 29, 2019
- "Falcon Crossing" - dated February 5, 2007
- "Liberty Tree Academy" - dated September 19, 2020
- "Meridian Ranch" - several reports
- "Grandview Reserve" - dated December 15, 2020
- "Judge Orr/Eastonville Commercial Center" - dated February 5, 2021


## LAND USE AND ACCESS

## Proposed Land Uses

Figure 1 shows the site location relative to the adjacent and nearby roadways. Located generally northeast of the intersection of Eastonville Road/Judge Orr Road (El Paso County parcel ID 4232302003), the site is currently vacant. Anticipated land uses for the 13.72-acre site include 214 single-family-attached dwelling units.

## Proposed Site-Access Locations

Figure 1 shows the area circulation and access points to the adjacent public roads, while Figure 2 contains the proposed site plan showing the proposed land uses, on-site circulation, and proposed access points. The access points may be private street/driveway connections or they may be developed as public streets. This will be determined later, but this report and the
deviations treat them as potential public street connections. Two full-movement access points/potential public street intersections are proposed:

- With Judge Orr Road - located approximately 1,040 feet east of Eastonville Road
- With Eastonville Road - future extension of Copenhagen Road

Per Standard 2.2.5.C of the ECM, $1 / 4$-mile ( 1,320 feet) is required on Urban Minor Arterials between public street intersections. The following proposed public street intersection spacings are currently shown on the conceptual site plan, as shown in Deviation Exhibit 1:

- 860 feet - on Eastonville Road between Judge Orr Road and the existing intersection of Eastonville/Copenhagen Road. The north site street connection is proposed to tie into this existing intersection.
- 360 feet - on Eastonville Road between the existing Eastonville/Tex Tan Road intersection and existing intersection of Eastonville/Copenhagen Road intersection. The north street connection for this site is proposed to tie into this latter existing intersection.
- 1,235 feet - along Judge Orr Road between Eastonville Road and the proposed south site street connection (which has been shifted, with this submittal, to align with the anticipated future street proposed for the property south of Judge Orr Road).
- 770 feet - along Judge Orr Road between the Meadowlake Ranch main entry street the proposed intersection of Judge Orr Road/the south site street connection/the anticipated future street proposed for the property south of Judge Orr Road

The proposed public street intersection spacings are less than one-quarter mile along both adjacent roads, which does not meet ECM criteria for intersection spacing. As such, deviation request(s) would be required for the proposed site public street intersection locations.

## SIGHT DISTANCE

## Sight Distance Field Measurements

Sight distance field measurements utilized a driver's eye height of 3.5 feet and a height of 3.5 feet for a vehicle traveling along Judge Orr Road and Eastonville Road. The following analysis corresponds to field-measured sight distances for the proposed site-access intersections. Field-measured sight distances for passenger vehicles are as follows:

- Proposed north site access on Eastonville Road
- To the northeast: greater than 1,000 feet
- To the southwest: unobstructed to Judge Orr/Eastonville/Meridian Hills
- Proposed south access on Judge Orr Road
- To the east: greater than 1,000 feet
- To the west: unobstructed to Judge Orr/Eastonville/Meridian Hills

Please refer to Figure 9 for detailed sight-distance analysis diagrams.

With a 35-mph posted speed limit on Eastonville Road, the field-measured sight distances for the proposed north site access would exceed the ECM-prescribed requirement for intersection sight distance for passenger vehicles, as shown in the ECM Table 2-21.

## South Access

With a 45-mph posted speed limit on Judge Orr Road, the field-measured sight distances on both approaches for the proposed south site access to Judge Orr Road would exceed the ECM-prescribed requirement for entering sight distance for passenger vehicles, as shown in ECM Table 2-21. Therefore, intersection sight distance would be acceptable at the proposed south site access location.

## Sight Distance Along a Roadway

Site-access points/driveways must meet ECM standards for sight distance along the roadway contained in Table 2-33 of the ECM.

## North Access

Based on the field measurements, the sight distance along a roadway at the proposed north site-access intersection is greater than 1,000 feet approaching the access from the north along Eastonville Road and unobstructed to Judge Orr/Eastonville/Meridian Ranch from the south. The sight distance along a roadway would exceed the 470-foot County standard in both directions for stopping sight distance at a posted speed of 35 mph .

## South Access

Based on the field measurements, the sight distance along a roadway at the proposed south site-access intersection is greater than 1,000 feet approaching the access from the east along Judge Orr Road and unobstructed to Judge Orr/Eastonville/Meridian Ranch from the west. The sight distance along a roadway would exceed the 555 -foot County/AASHTO standard in both directions for stopping sight distance at a posted speed of 45 mph .

## ROAD AND TRAFFIC CONDITIONS AND MTCP CLASSIFICATION

Figure 1 shows the roads adjacent to and in the vicinity of the site. Adjacent roads serving the site are identified below followed by a brief description of each:

US Highway 24 (US 24) is a state highway extending locally from the City of Colorado Springs to Peyton in a northeasterly direction and then continuing east. US 24 is planned to be widened to four lanes through the Falcon area and is classified as an E-X - Expressway by the Colorado Department of Transportation (CDOT) and a 4-lane Principal Arterial on the EI Paso County Major Transportation Corridors Plan (MTCP). The posted speed limit on US 24 adjacent to the site is 65 miles per hour (mph). Auxiliary left-turn lanes currently exist on the northbound and southbound approaches at the signalized intersection of US 24/Judge Orr.

Judge Orr Road is a two-lane roadway that extends east from Eastonville Road across most of El Paso County. It is shown on the El Paso County 2040 Major Transportation Corridors Plan and the Preserved Corridor Network Plan as a four-lane Minor Arterial adjacent to the site (and west of Curtis Road). Posted speed limits adjacent to the site range from 45 to 55 mph . West of Curtis Road, the speed limit is 45 mph , while it generally increases to 55 mph east of Curtis Road. The intersection of US $24 / J u d g e$ Orr is currently signalized. Due to the oblique angle of this intersection, the eastbound and westbound approaches are split-phased. The US 24 Access Control Plan/PEL Study shows future plans for realignment of Judge Orr at US 24 to improve the intersection and provide an intersection angle closer to 90 degrees.

Eastonville Road is shown as a two-lane Minor Arterial on the El Paso County 2040 Major Transportation Corridors Plan and the Preserved Corridor Network Plan. A two-lane roadway extending northeast from Meridian Road past Hodgen Road, Eastonville Road has a posted speed limit of 35 mph . All approaches at the four-way stop-sign-controlled intersection of Judge Orr Road/Eastonville Road have an exclusive left-turn lane, while the northwest-bound approach also has an auxiliary right-turn lane. South of Stapleton Drive, Eastonville Road's cross-section is consistent with a two-lane Urban Collector cross-section with a painted two-way left-turn lane (TWLTL).

Meridian Ranch Road extends from Eastonville Road to Sunset Crater Drive and is shown as a two-lane Collector on the MTCP. Judge Orr Road transitions to Meridian Road northwest of Eastonville Road and has a posted speed limit of 35 mph . The southeast-bound approach has a painted TWLTL with a shared through/right-turn lane.

## Existing Traffic Volumes

Vehicular turning-movement counts were conducted for the following dates and times at the following intersections:

- Judge Orr Road/Eastonville Road
- Tuesday, May 10, 2022 from 6:30-8:30 a.m.
- Tuesday, May 10, 2022 from 4:00-6:00 p.m
- US 24/Judge Orr Road
- Thursday, July 7, 2022 from 6:30-8:30 a.m.

Identify the adjustment factor used and explain how you determined the adjustment factor.

- Wednesday, lunt 22, 2022 from 4:00-6:00 p.m.

Count data has been adjusted to account for any differences due to area school traffic. The adjusted volumes are shown in Figure 3 shows these turning-movement volumes, as well as the average weekday traffic volumes (estimated based on factored peak-hour count data) on the study-area roadways. Raw count data is attached.

## PEDESTRIAN AND BICYCLE FACILITIES

Judge Orr Road and Eastonville Road do not currently have sidewalks or bicycle lanes to accommodate pedestrians or bicycles, but sidewalks would be required along both roadways following site buildout. The proposed subdivision roads are likely to be Urban roadways and, per ECM criteria, would require sidewalks.

## TRIP GENERATION

Estimates of the vehicle trips projected to be generated by the proposed Judge Orr Eastonville Commercial Center development have been made using the nationally published trip-generation rates from Trip Generation, $11^{\text {th }}$ Edition, 2021 by the Institute of Transportation Engineers (ITE). Corresponding trip-generation rates from ITE Land Use Category " 215 - Single-Family (Attached) Housing" have been used to develop the trip-generation estimates for the proposed 214-dwelling unit residential site.

Table 1 below presents a summary of the estimated external site trip generation. A detailed trip-generation estimate for the site, including ITE rates for the proposed land uses, is presented in Table 5 (attached). Figure 2 shows the layout within the site.

The proposed residential site is projected to generate about 1,541 total vehicle trips on the average weekday during a 24 -hour period, with approximately half entering and half exiting the site. During the morning peak hour, approximately 32 entering vehicles and 71 exiting vehicles are estimated to be generated. Approximately 70 entering and 52 exiting vehicles are estimated to be generated by the site during the afternoon peak hour.

Table 1: Estimated Site Vehicle-Trip Generation

| Analysis Period | Weekday |  |  |
| :---: | :---: | :---: | :---: |
|  | In | Out | Total |
| Morning Peak Hour | 32 | 71 | 103 |
| Afternoon Peak Hour | 70 | 52 | 122 |
| Daily/24-hour | 721 | 721 | 1,541 |

## TRIP DISTRIBUTION AND ASSIGNMENT

## Trip Directional Distribution

The directional-distribution estimate of site-generated vehicle trips to the study-area roads and intersections is a necessary component in determining the site's traffic impacts. Figure 4 shows the percentages of the site-generated vehicle trips projected to be oriented to and from the site's major approaches. Estimates have been based on the following factors: the proposed new land use, the area roadway system serving the site, and the site's geographic location relative to the overall greater El Paso County/Colorado Springs area. Figure 4 shows estimated distribution splits for the short and long term. The long-term splits consider the addition of the Stapleton Road connection to the west and new development to the northeast, east, and southeast.

## Site-Generated Traffic

Site-generated traffic volumes have been estimated at the following intersections:

- Judge Orr Road/Eastonville Road
- Judge Orr Road/proposed south full-movement site access
- Eastonville Road/Copenhagen Road/proposed north full-movement site access
- US 24/Judge Orr Road


## Short Term

Short-term site-generated volumes have been calculated by applying the short-term directional-distribution percentages estimated by LSC (from Figure 4) to the trip-generation estimates (from Table 5). Figure 5a shows the projected short-term site-generated traffic volumes for the weekday morning and afternoon peak hours.

## Long Term

Long-term site-generated volumes have been calculated by applying the long-term directional-distribution percentages estimated by LSC (from Figure 4) to the trip-generation estimates (from Table 5). Figure 5b shows the projected long-term site-generated traffic volumes for the weekday morning and afternoon peak hours.

## Existing + Site-Generated Traffic Volumes

Figure 6 shows the sum of the 2023 background traffic volumes (from Figure 3) and short-term site-generated peak-hour traffic volumes (shown in Figure 5a). These volumes represent the projected short-term total traffic following site buildout. Laneage and traffic control at the study-area intersections following site buildout are shown in Figure 6.

## 2042 Background Traffic Volumes $\_$State the growth rate factor used.

Long-term background traffic volumes are estimates by LSC, based on projected 2042 volumes adjacent to the site shown in Map 9 of the MTCP. Additionally, traffic generated by planned adjacent and nearby developments, such as Meadowlake Ranch, Liberty Tree Academy, Meadowlake Industrial Park, and Falcon Crossing, has been included in 2042 background traffic volumes. Please refer to Figure 7 for estimated long-term background volumes and assumed laneage at the study-area intersections.

Projected long-term background traffic volume projections along Eastonville Road and Judge Orr Road in this vicinity have been based, in part, on the recent Eastonville Road Project Traffic Impact Study by Wilson \& Company. Site-generated traffic from nearby planned developments has also been considered.

Future access to the currently-undeveloped parcel to the south would likely be required to align with this site's access on Judge Orr Road. LSC has assumed single-family residential development on approximately 49 acres, with the potential for additional future single-family residential dwelling units northeast of this area (east of the drainage channel). Approximately 60 percent of future residential traffic from this south parcel was assumed to orient to/from US 24, while the remainder would access the site via the Eastonville/Judge Orr/Meridian Ranch intersection to the west.

## 2042 Total Traffic Volumes

Figure 8 shows the sum of 2040 background traffic volumes (from Figure 7) plus long-term sitegenerated traffic volumes (from Figure 5b).

## LEVEL OF SERVICE ANALYSIS

Level of service (LOS) is a quantitative measure of the level of congestion or delay at an intersection and is indicated on a scale from "A" to " $F$." LOS A is indicative of little congestion or delay. LOS F indicates a high level of congestion or delay. Table 2 shows the level of service delay ranges for signalized and unsignalized intersections.

Table 2: Intersection Levels of Service Delay Ranges

| Level of Service | Signalized Intersections | Unsignalized Intersections |
| :---: | :---: | :---: |
|  | Average Control Delay <br> (seconds per vehicle) | Average Control Delay <br> (seconds per vehicle) ${ }^{(\mathbf{1})}$ |
| A | 10.0 sec or less | 10.0 sec or less |
| B | $10.1-20.0 \mathrm{sec}$ | $10.1-15.0 \mathrm{sec}$ |
| C | $20.1-35.0 \mathrm{sec}$ | $15.1-25.0 \mathrm{sec}$ |
| D | $35.1-55.0 \mathrm{sec}$ | $25.1-35.0 \mathrm{sec}$ |
| E | $55.1-80.0 \mathrm{sec}$ | $35.1-50.0 \mathrm{sec}$ |
| F | 80.1 sec or more | 50.1 sec or more |

(1) For unsignalized intersections, if $\mathrm{V} / \mathrm{C}$ ratio is greater than 1.0 the level of service is LOS F, regardless of the projected average control delay per vehicle.

LOS values have been included in each figure for each turning movement/approach during the weekday morning and afternoon peak hours for the proposed site-access intersections and off-site intersections in the study area:

- Figure 3: 2022 Existing Traffic, Lane Geometry, Traffic Control, and LOS
- Figure 6: 2022 Existing + Site Traffic, Lane Geometry, Traffic Control, and LOS
- Figure 7: 2042 Background Traffic, Lane Geometry, Traffic Control, and LOS
- Figure 8: 2042 Background + Site Traffic, Lane Geometry, Traffic Control, and LOS

LOS calculations for long-term scenarios were based upon the recommended lane geometries and traffic controls outlined in the figures above.

## Judge Orr Road/Eastonville Road/Meridian Ranch

## Short Term

The intersection of Judge Orr/Meridian Ranch/Eastonville is currently all-way, stop-sign-controlled (AWSC). All movements at this intersection currently operate at and are projected to remain at LOS C or better during both peak hours with the addition of site-generated traffic. No modifications would be required to this intersection during the short term.

## Long Term

If the intersection of Judge Orr/Eastonville/Meridian Ranch remains AWSC, several turning movements and single-lane approaches would operate at LOS F during the peak hours, based on the projected long-term background and total volumes. However, if this intersection were either reconstructed as a modern roundabout, the intersection is projected to operate at LOS A overall during both long-term peak hours.

Note: Section 5.2 of the Eastonville Road Project Traffic Impact Study indicates that the intersection of Judge Orr/Eastonville/Meridian Ranch would likely be improved to a roundabout once it operates at LOS C or worse as an all-way stop-sign-controlled intersection. It is likely that this intersection will be reconstructed as a modern roundabout with the next phase of the PPRTA project (south of Snaffle Bit). Most other intersections to the north along Eastonville (through the Phase 1 sections of the Eastonville PPRTA project) are currently planned to be roundabouts.

## Eastonville Road/Copenhagen Road (Proposed North Site Access)

All individual turning movements and approaches are projected to operate at LOS D or better during both short-term and long-term peak hours as a two-way stop-sign-controlled intersection during both peak hours. Please refer to Figure 6 and Figure 8 for recommended lane configurations and LOS summaries at this intersection during the short-term and long-term scenarios, respectively.

## Judge Orr Road/Proposed South Site Access

All individual turning movements and approaches are projected to operate at LOS C or better through the long term as a stop-sign-controlled intersection without the addition of any auxiliary turn lanes. Please refer to Figure 6 and Figure 8 for recommended lane configurations and LOS summaries at this intersection during the short-term and long-term scenarios, respectively.

## US Highway 24/Judge Orr Road

## Short Term

The intersection of US $24 /$ Judge Orr is currently signalized. The US 24 Access Control Plan shows this intersection realigned to one of two alternate alignments that would provide an intersection angle closer to 90 degrees. All movements at this intersection except for the westbound-through movement are currently operating at LOS D or better during both peak hours.

Short-term analysis assumes the proposed realignment has not yet been constructed, but assumes future southbound right-turn deceleration, a southbound right-turn acceleration, and an eastbound right-turn lane. These turn lanes are shown at the intersection of US 24/Judge Orr in CDOT's US 24 Planning \& Environmental Linkages (PEL) Study.

## Long-Term

By 2040, it was assumed that this intersection would be realigned and both Judge Orr Road and US 24 would be widened to provide two through lanes in each direction. Based on the projected 2040 background and total traffic volumes and the lane geometry shown in Figure 7 and Figure 8 , this intersection is projected to operate at an overall LOS D during the peak hours. Some minor movements are projected to operate at LOS E during the peak hours simply because of the
likelihood of arrival at the traffic signal at the beginning of the red phase at an intersection with many phases and a long cycle length. These movements would not be considered "failing" since the volume-to-capacity ratios would be less than 1.0. The justification is that to progress through traffic along an arterial corridor, the traffic signal offsets and left-turn and side street phase times have been adjusted to favor the through traffic band, which can often result in higher delay for the left-turn movements even though there is sufficient capacity for them.

## VEHICLE QUEUING

This section contains the projected $95^{\text {th }}$-percentile queues for the following turning movements:

- Judge Orr Road between Eastonville Road and the proposed south access
- Eastonville Road/Copenhagen Road/proposed north site access


## Eastonville Road/Copenhagen Road/Proposed North Site Access

Table 3 presents the projected short-term and long-term $95^{\text {th }}$-percentile queues for the southbound-left turning movement at the intersection of Eastonville Road/Copenhagen Road/proposed north site access. Synchro scenario queue reports indicated that the $95^{\text {th }}$-percentile eastbound-left turning-movement queues would not exceed the available stacking length during either short-term or long-term peak hour. Synchro queueing reports indicated a $95^{\text {th }}$-percentile queue length of 1-3 vehicles ( $25-75$ feet) during all short-term and long-term peak hours.

Table 3: 95 ${ }^{\text {th }}$-Percentile Queues ( 2042 Background + Site) Eastonville Road/Proposed North Access - Southbound Left-Turn Lane

| Major Street | Easto | Road |
| :---: | :---: | :---: |
| Minor Street | Proposed | Site Access |
| Turning Movement | South | Left |
| Analysis Period | A.M. Peak | P.M. Peak |
| Existing + Site (Two-Way Stop Sign Control) |  |  |
| Storage Length (ft) | 160' | 160' |
| Taper Length (ft) | 155' | 155' |
| $95^{\text {th }}$-Percentile Queue (ft) | 75' | 50' |
| 2040 Background + Site (Roundabout) |  |  |
| Storage Length (ft) | - | - |
| Taper Length (ft) | - | - |
| 95 ${ }^{\text {th }}$ Percentile Queue (ft) | 50' | 25' |
| Note: Synchro assumes queue length per average vehicle is 25 ft |  |  |

## Judge Orr Road/Proposed South Site Access

The $95^{\text {th }}$ percentile queue for the eastbound left-turn movement at the south site access is projected to be about one vehicle.

## US Highway 24/Judge Orr Road

Table 4 presents the projected short-term and long-term $95^{\text {th }}$-percentile queues for several turning movements at the intersection of US 24/Judge Orr Road. Synchro scenario queue reports indicated that the $95^{\text {th }}$-percentile queues would not exceed the available stacking length during either shortterm or long-term peak hour for the following turning movements: eastbound through/left (shortterm), westbound approach (short-term), eastbound left (long-term), westbound left (long-term), and northbound left (short-term and long-term).

Table 4: $95^{\text {th }}$-Percentile Queues (US Highway 24/Judge Orr Road)

| Major Street | US Highway 24 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Minor Street | Judge Orr Road |  |  |  |  |  |
| Turning Movement | Eastbound* |  | Westbound* |  | Northbound Left |  |
| Analysis Period | A.M. Peak | P.M. Peak | A.M. Peak | P.M. Peak | A.M. Peak | P.M. Peak |
| Existing + Site |  |  |  |  |  |  |
| Storage Length ( ft ) | - | - | - | - | 860' | $860{ }^{\prime}$ |
| Taper Length ( ft ) | - | - | - | - | $300^{\prime}$ | $300{ }^{\prime}$ |
| Max Queue (ft) | $90^{\prime}$ | 89' | 197' | $286{ }^{\prime}$ | $67^{\prime}$ | $103 '$ |
| 2040 Background + Site |  |  |  |  |  |  |
| Storage Length ( ft ) | 290' | 290' | 290' | $290{ }^{\prime}$ | 860' | 860' |
| Taper Length ( ft ) | $240{ }^{\prime}$ | $240{ }^{\prime}$ | $240{ }^{\prime}$ | $240{ }^{\prime}$ | $300{ }^{\prime}$ | $300{ }^{\prime}$ |
| Max Queue (ft) | $68^{\prime}$ | $166{ }^{\prime}$ | 146' | 271' | 125' | 229 ' |

Note: Synchro assumes queue length per average vehicle is 25 ft

* Analysis is for EB through/left lane during short-term, but EB left-turn lane for 2042


## ROADWAY IMPROVEMENTS

## Auxiliary Turn Lanes

The following design speeds were used to determine required turn lane lengths for each of the study-area roadways:

- US Highway 24-70 mph
- Judge Orr Road - 50 mph
- Eastonville Road - 40 mph
- Meridian Ranch Boulevard - 40 mph


## Judge Orr Road/Proposed South Site Access

## Eastbound Approach

According to the El Paso County Engineering Criteria Manual (ECM), exclusive left-turn lanes shall be provided for any access on a Minor Arterial or Collector with a projected peak-hour ingress turning volume of 25 vehicles per hour (vph) or greater. The projected left-turn volume at the south site-access point is not expected to exceed the 25 -vph minimum left-turn volume thresholds prescribing a turn lane outlined in the ECM upon site buildout. As such, an eastbound left-turn deceleration lane would not be required on Judge Orr Road approaching the south access. Note: In the future, with this and other development along Judge Orr Road along with increases in through background traffic, the roadway is likely to be upgraded to an Urban Minor Arterial cross section. That cross section includes a striped center median for left-turning movements.

## Westbound Approach

State the turning volume determined for both EB and WB Judge Orr Rd approaches

According to ECM, exclusive right-turn lanes shall be provided for any access on a Minor Arterial or Collector with a projected peak-hour ingress turning volume of 50 vehicles per hour (vph) or greater. The projected right-turn volume at the south site access point is not expected to exceed the 50-vph minimum right-turn volume thresholds prescribing a turn lane outlined in the ECM upon site buildout. As such, a westbound right-turn deceleration lane would not be required on Judge Orr Road approaching the south access.

## Eastonville Road/Proposed North Site Access

## Southwest Approach

Eastonville Road is currently striped with a painted center two-way left-turn lane (TWLTL). Although, the projected southbound left-turn volume at the north site access point is not expected to exceed the minimum left-turn volume threshold prescribing a left-turn lane outlined in the ECM, the existing TWLTL currently provides a separate lane for this project's southbound left-turning movements.

Restriping will be required for the center southbound turn lane. Add to list of required applicant improvements

## Northeast Approach

According to the ECM, exclusive right-turn lanes shall be provided for any access on a Minor Arterial or Collector with a projected peak-hour ingress turning volume of 50 vehicles per hour (vph) or greater. The projected northbound right-turn volume at the north site access point is not expected to exceed the $50-\mathrm{vph}$ minimum right-turn volume thresholds prescribing an exclusive turn lane outlined in the ECM upon site buildout. As such, a northeast-bound right-turn deceleration lane would not be required on Eastonville Road approaching the north access.

## State the NB

right-turn volume determined at full build out.

```
Provide justification for full
movement turn instead of
3/4 movement at both north
and south access points
```


## US Highway 24/Judge Orr Road

Auxiliary turn lanes are planned to be added at this intersection as part of El Paso County intersection improvement project C14. This roadway improvement project has been identified as being needed by the year 2040 per Map 13 and Table 4 of El Paso County's 2016 MTCP:

- C14 - Judge Orr Road from Eastonville Road to Peyton Highway $(\$ 38,248,000)$
- Existing conditions - 2-lane Rural Minor Arterial
- Future conditions - 4-lane Rural Minor Arterial

As such, no modifications would be required by the applicant at the intersection of US 24/Judge Orr as a result of additional site-generated traffic from this development.

## Judge Orr Road/Meridian Ranch Boulevard/Eastonville Road

No modifications to existing auxiliary turn lanes would be required at the intersection of Eastonville/Judge Orr/Meridian Ranch following site buildout. However, Section 5.2 of the Eastonville Road Project Traffic Impact Study indicates that the intersection of Judge Orr/Eastonville/Meridian Ranch would likely be improved to a roundabout once it operates at LOS C or worse as an all-way stop-sign-controlled intersection.

It is likely that this intersection will be reconstructed as a modern roundabout with the next phase of the PPRTA project (south of Snaffle Bit). Most other intersections to the north along Eastonville (through the Phase 1 sections of the Eastonville PPRTA project) are currently planned to be roundabouts and are under design.

## Intersection Configuration and Traffic Control

Please refer to the Roadway Improvements Table (attached as Table 6).

## ROADWAY CLASSIFICATIONS

All internal roadways within the 214-dwelling-unit residential development are proposed to be private streets.

## COUNTY ROAD IMPROVEMENT FEE PROGRAM

## Transportation Impact Fees

Per ECM Appendix B: State what the current applicable Transportation Impact Fees are and what option the developer will be selecting for payment.

The applicant will be required to participate in this program. The PID option will be identified with a future Preliminary Plan/Plat submittal.

## Reimbursable Improvements

The following roadway improvement projects have been identified as being needed by the year 2040 per Map 13 and Table 4 of El Paso County's 2016 MTCP:

- C14 - Judge Orr Road from Eastonville Road to Peyton Highway $(\$ 38,248,000)$
- Existing conditions - 2-lane Rural Minor Arterial
- Future conditions - 4-lane Rural Minor Arterial
- Note: It would seem most logical and consistent with the existing section of Eastonville adjacent to the site, plans for other sections of Eastonville Road, and existing Meridian Ranch Drive, for the section of Judge Orr Road between Eastonville and US Highway 24 to be an Urban Minor Arterial rather than "Rural."
- U19 - Eastonville Road from McLaughlin Road to Latigo Boulevard $(\$ 18,420,000)$
- Existing conditions (note: some sections following PPRTA improvements) - 2-lane Rural Unimproved County Road
- Future conditions - 2-lane Rural Minor Arterial
- Note: This PPRTA project has been divided into several phases. The first phase will be from Snaffle Bit north to Rex and the second phase will be between McLaughlin and Snaffle Bit. The Phase 1 segment of Eastonville will be a modified Urban Minor Arterial cross section. Phase 1 is currently under design.

See the attached MTCP maps for reference.

## MULTI-MODAL TRANSPORTATION AND TDM OPPORTUNITIES

The following roadway improvement projects have been identified as being needed by the year 2040 per Map 15 and Table 5 of El Paso County's 2016 MTCP:

- M8 - Judge Orr Road from Eastonville Road to South Peyton Highway
- Bicycle improvements ( 2.98 miles)


## Pedestrian and Bicycle Accommodations

There are two existing public schools located within two miles of the site, Falcon High School and Woodmen Hills Elementary School. Additionally, the Transcend Trail connects several local parks west of the site within a two-mile radius.

Figure 10 and Figure 11 show the school pedestrian/bike routes between the proposed residential site and Woodmen Hills Elementary School and Falcon High School, respectively. There are currently no sidewalks on Judge Orr Road or Eastonville Road.

The following is a list of known and planned multi-modal and pedestrian accommodations in the vicinity of the site:

- A park-and-ride facility is planned for a site near Meridian Road and US Highway 24.
- The Rock Island Regional Trail passes near the site to the east.
- Many of the area County roads have been or will be upgraded to provide paved shoulders for cyclists. Stapleton is shown as a future "bike route."
- The MTCP shows a future primary regional trail along Eastonville Road. Another future primary regional trail is shown extending west from Eastonville Road though Meridian Ranch.
- The Highway 24 PEL study also includes multi-modal elements.


## DEVIATIONS

The following deviations to ECM design criteria are proposed at the proposed site access intersections on Judge Orr Road and Eastonville Road:

- Section 2.2.5.C - Roadway Access Criteria (Urban Minor Arterial Access Standards)
- Section 2.3.2 - Design Standards by Function Classification

Please refer to the deviation request forms included with the application submittal.

## FINDINGS AND CONCLUSIONS

- The site is projected to generate about 1,541 new driveway vehicle-trips on the average weekday.
- During the weekday morning peak hour of adjacent street traffic, 32 vehicles would enter the site while 71 vehicles would exit.
- During the weekday afternoon peak hour of adjacent street traffic, 70 vehicles would enter the site while 52 vehicles would exit.
- All individual approaches and turn lanes at both site-access intersections would operate at LOS D or better during both short-term and long-term peak hours as stop-sign-controlled intersections with single-lane exiting approaches. Please refer to the "Level of Service" section above for detailed LOS results and discussion regarding all study-area intersections.
- Auxiliary left-turn and right-turn deceleration lanes would not be required at either of the site-access points, based on projected buildout traffic volumes. Please refer to the "Auxiliary Turn-Lane Analysis" section for evaluation of potential turn-lane needs.
- All internal site access roadways are proposed to be private streets.
- Please refer to the "Queuing Analysis" section above for additional details. Synchro queue reports indicated that the $95^{\text {th }}$ percentile left-turn queues at both site-access points are not projected to exceed the back-to-back left-turn stacking distances to adjacent upstream intersections during either peak hour.
- Please refer to the "List of Improvements" (attached) for a summary of roadway improvements, including timing and financial responsibility for each improvement.
- Deviations are included with this submittal.

Please contact me if you have any questions regarding this report.
Respectfully Submitted,

LSC TRANSPORTATION CONSULTANTS, INC.
By: Jeffrey C. Hodsdon, P.E.
Principal
JCH/JAB:jas
Enclosures: Table 5 and 6
Figure 1 - Figure 11
Traffic Count Reports
Synchro LOS Reports

Tables

Table 5: Detailed Trip Generation Estimate

| ITE |  | Value | Units ${ }^{1}$ | Trip Generation Rates ${ }^{2}$ |  |  |  |  | \% <br> Internal <br> Capture | Driveway Trips Generated |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Average <br> Weekday |  | A.M. |  | P.M. |  | Average <br> Weekday |  | A.M. |  | P.M. |  |
| Code | Description |  |  | In | Out | In | Out |  |  | In | Out | In | Out |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Currently-Proposed Site Plan |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 215 | Single-Family (Attached) Housing | 214 | DU | 7.20 | 0.15 | 0.33 | 0.32 | 0.25 | 0\% | 1541 | 32 | 71 | 70 | 52 |
|  |  | $\underbrace{\prime}$ |  |  |  |  |  |  |  |  |  |  |  |  |
| Previously-Approved Site Plan |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 151 | Mini-Warehouse | 5.00 | \& (100s) | 18.04 | 0.62 | 0.60 | 0.98 | 0.98 | 0\% | 90 | 3 | 3 | 5 | 5 |
| 565 | Day Care Center | 90 | students | 4.09 | 0.41 | 0.37 | 0.37 | 0.42 | 0\% | 368 | 37 | 33 | 33 | 38 |
| 820 | Shopping Center | 117.612 | KSFF | 57.08 | 1.11 | 0.68 | 2.50 | 2.71 | 16\% | 5639 | 110 | 67 | 247 | 268 |
| 912 | Drive-in Bank | 7.000 | \{KSF | 99.60 | 5.51 | 3.99 | 10.23 | 10.23 | 0\% | 697 | 39 | 28 | 72 | 72 |
|  |  | $\cdots$ |  |  |  |  |  |  | Total | 6798 | 191 | 132 | 359 | 383 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  | ently-P | ropose | d Site Plan | 1541 | 32 | 71 | 70 | 52 |
|  |  |  |  |  |  | Prev | ously-A | pprove | d Site Plan | 6798 | 191 | 132 | 359 | 383 |
|  |  |  |  |  |  |  |  |  | Total | -5257 | -159 | -61 | -289 | -331 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ${ }^{2}$ Source: Trip Generation, 11th Edition (2021) by the Institute of Transportation Engineers (ITE) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Remove. This appears to be from Judge Orr Eastonville Sketch Plan Amendment TIS (PCD Flle No. SKP203). The project was withdrawn by the applicant and the associated file was not accepted for file by the County.

Table 6: Roadway Improvements

| Existing County Roadway Segment Improvements |  |  |  |
| :---: | :---: | :---: | :---: |
| Item \# | Improvement | Timing | Responsibility |
| 1.1 | Eastonville Road Widen to 2-Lane Rural Minor Arterial Shown in 2040 MTCP (Project U19) | The timing of this improvement may be identified with the Preliminary Plan/Plat, if not determined before that time by others. | Details TBD <br> Any responsibility of this development for completing this improvement or a portion thereof will be identified with the Preliminary Plan/Plat. |
| 1.2 | Judge Orr Road Widen to 4-Lane Rural Minor Arterial Shown in 2040 MTCP (Project C14) | The timing of this improvement may be identified with the Preliminary Plan/Plat, if not determined before that time by others. | Details TBD <br> Any responsibility of this development for completing this improvement or a portion thereof will be identified with the Preliminary Plan/Plat. |
| 1.3 | Judge Orr Road Add bicycle lanes from Eastonville Road to S. Peyton Highway Shown in 2040 MTCP (Project M8) | The timing of this improvement may be identified with the Preliminary Plan/Plat, if not determined before that time by others. | Details TBD <br> Any responsibility of this development for completing this improvement or a portion thereof will be identified with the Preliminary Plan/Plat. |
|  |  | Proposed Internal Site Roadways |  |
| Item \# | Improvement | Timing | Responsibility |
| 2.1 | Construct internal streets to County Urban Local Standards; may also be developed with private streets. | With site development (may be phased). The timing of this improvement will be identified with the Preliminary Plan/Plat. | Applicant |
| Off-Site, CDOT Intersection |  |  |  |
| US Highway 24/Judge Orr Road Intersection |  |  |  |
| Item \# | Improvement | Timing | Responsibility |
| 3.1 | Long Term (or Prior to 2040) <br> Realign eastbound and westbound approaches to reduce the intersection skew angle. | TBD; Please refer to the US Highway 24 PEL Study and the CDOT US Highway 24 Corridor information. | This realignment is likley to be a CDOT project. |
| 3.2 | Long Term (or Prior to 2040) Southwest-bound right-turn deceleration lane | Timing be determined through the CDOT access permit process. That process will come at a later stage of development. The timing will likely be associated with prevailing turning movement volumes at that time and relative to Access Code thresholds for turn lanes. As indicated in the CDOT comment letter, site-generated southwest-to-westbound right turn movement at Hwy 24 and Judge Orr is projected to add 25 vehicles (short term) in the AM peak hour. The State Highway Access Code §3.7(4)(b) requires installation of right turn deceleration lane for any access with a projected right turn volume greater than 10 vehicles per hour. The timing/phasing of improvements or participation in future improvements will likley depend on the pace and intensity of development of this site and the rate of other area developments and associated background traffic growth. | The responsibility will be determined through the CDOT access permit process. That process will come at a later stage of development. This is a Master study. CDOT indicated "Land Use(s) will need to be determined prior to making application for the State Highway Access Permit. No determination of land use(s) we described in the Letter of Intent and was general in nature." The responsibility will be determined by CDOT and may involve this development contributing a fair share escrow amount toward identified future improvements and/or actually installing a turn lane(s) or other improvement. |
| 3.3 | Long Term (or Prior to 2040) Southwest-bound right-turn acceleration lane | Timing be determined through the CDOT access permit process. That process will come at a later stage of development. The timing will likely be associated with prevailing turning movement volumes at that time and relative to Access Code thresholds for turn lanes. As indicated in the CDOT comment letter, Site-generated east-to-southwest-bound right turn movement at Hwy 24 and Judge Orr is projected to add 73 vehicles (short term) in the PM peak hour. The State Highway Access Code $\S 3.7$ (4)(c) requires installation of right turn acceleration lane for any access with a projected right turn volume greater than 10 vehicles per hour. The timing/phasing of improvements or participation in future improvements will likley depend on the pace and intensity of development of this site and the rate of other area developments and associated background traffic growth. |  |
| 3.4 | Long Term (or Prior to 2040) Northeast-bound right-turn deceleration lane | Dependent on Background Traffic and/or timing of a CDOT or other project at this intersection. | Although this project may have some responsibility for improvement of this intersection. This project will not add to the right turn movement at this intersection. |
| Adjacent Intersections |  |  |  |
| Eastonville Road/Woodmen Hills Drive/Judge Orr Road Intersection |  |  |  |
| Item \# | Improvement | Timing | Responsibility |
| 4.1 | Long Term (or Prior to 2040) <br> Reconstruct intersection as a modern roundabout (or signalize the intersection) | Once LOS of AWSC drops below acceptable levels (roundabout); or once signal warrants are met (for conversion to a signal or roundabout). Depends on the pace and intensity of development of this site and the rate of other area development and associated background traffic growth. | Details TBD <br> Any responsibility of this development for completing intersection improvements or a portion thereof will be identified with the Preliminary Plan/Plat. |
| Eastonville Road/Copenhagen/North Site Street Connection (Proposed) |  |  |  |
| Item \# | Improvement | Timing | Responsibility |
| 6.1 | Short Term <br> Southwest-bound left-turn deceleration lane | With subdivision/plat filings, per ECM turning volume thresholds | Applicant |
| 6.2 | Short Term <br> Northeast-bound right-turn deceleration lane | With subdivision/plat filings, per ECM turning volume thresholds | Applicant |
| Proposed New Public Street Intersection |  |  |  |
| Judge Orr Road/South Site Street Connection/Future Street South of Judge Orr |  |  |  |
| Item \# | Improvement | Timing | Responsibility |
| 5.1 | Short Term <br> Eastbound left-turn deceleration lane | With subdivision/plat filings, per ECM turning volume thresholds | Applicant |
| 5.2 | Short Term <br> Westbound right-turn deceleration lane | With subdivision/plat filings, per ECM turning volume thresholds | Applicant |
| 5.3 | Long Term <br> Reconstruct intersection as a modern roundabout | With subdivision/plat filings (if implemented) | Applicant and potentially the future development south of Judge Orr Road |
| Source: LSC Transportation Consultants, Inc. (Revised 2/26/2021) |  |  |  |
| Note: T | Timing and responsibility is subject to change as future ap | lications are submitted |  |

Figures














## Traffic Counts

# LSC Transportation Consultants, Inc. <br> 2504 E. Pikes Peak Ave, Suite 304 <br> Colorado Springs, CO 80909 <br> 719-633-2868 

File Name : hwy 24 - judge orr rd am
Site Code : S214950
Start Date : 5/10/2022
Page No : 1

Groups Printed- Unshifted

|  | $\begin{gathered} \text { Hwy } 24 \\ \text { Southbound } \end{gathered}$ |  |  |  |  | Judge Orr Rd Westbound |  |  |  |  | Hwy 24 Northbound |  |  |  |  | Judge Orr Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| 06:30 | 1 | 130 | 0 | 0 | 131 | 1 | 7 | 36 | 0 | 44 | 4 | 66 | 8 | 0 | 78 | 43 | 14 | 2 | 0 | 59 | 312 |
| 06:45 | 4 | 173 | 3 | 0 | 180 | 0 | 10 | 20 | 0 | 30 | 18 | 92 | 8 | 0 | 118 | 34 | 10 | 4 | 0 | 48 | 376 |
| Total | 5 | 303 | 3 | 0 | 311 | 1 | 17 | 56 | 0 | 74 | 22 | 158 | 16 | 0 | 196 | 77 | 24 | 6 | 0 | 107 | 688 |
| 07:00 | 2 | 132 | 0 | 0 | 134 | 3 | 7 | 39 | 0 | 49 | 18 | 98 | 23 | 0 | 139 | 50 | 16 | 9 | 0 | 75 | 397 |
| 07:15 | 3 | 137 | 2 | 0 | 142 | 1 | 23 | 26 | 0 | 50 | 19 | 82 | 18 | 0 | 119 | 43 | 16 | 2 | 0 | 61 | 372 |
| 07:30 | 9 | 137 | 2 | 0 | 148 | 0 | 17 | 30 | 0 | 47 | 9 | 71 | 24 | 0 | 104 | 51 | 20 | 0 | 0 | 71 | 370 |
| 07:45 | 1 | 102 | 1 | 0 | 104 | 1 | 15 | 15 | 0 | 31 | 21 | 67 | 17 | 0 | 105 | 21 | 15 | 3 | 0 | 39 | 279 |
| Total | 15 | 508 | 5 | 0 | 528 | 5 | 62 | 110 | 0 | 177 | 67 | 318 | 82 | 0 | 467 | 165 | 67 | 14 | 0 | 246 | 1418 |
| 08:00 | 2 | 108 | 1 | 0 | 111 | 1 | 8 | 22 | 0 | 31 | 23 | 68 | 12 | 1 | 104 | 28 | 20 | 5 | 0 | 53 | 299 |
| 08:15 | 5 | 96 | 1 | 0 | 102 | 2 | 3 | 29 | 0 | 34 | 15 | 70 | 14 | 0 | 99 | 15 | 13 | 4 | 0 | 32 | 267 |
| Grand Total | 27 | 1015 | 10 | 0 | 1052 | 9 | 90 | 217 | 0 | 316 | 127 | 614 | 124 | 1 | 866 | 285 | 124 | 29 | 0 | 438 | 2672 |
| Apprch \% | 2.6 | 96.5 | 1 | 0 |  | 2.8 | 28.5 | 68.7 | 0 |  | 14.7 | 70.9 | 14.3 | 0.1 |  | 65.1 | 28.3 | 6.6 | 0 |  |  |
| Total \% | 1 | 38 | 0.4 | 0 | 39.4 | 0.3 | 3.4 | 8.1 | 0 | 11.8 | 4.8 | 23 | 4.6 | 0 | 32.4 | 10.7 | 4.6 | 1.1 | 0 | 16.4 |  |

# LSC Transportation Consultants, Inc. 

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : hwy 24 - judge orr rd am
Site Code : S214950
Start Date : 5/10/2022
Page No : 2

|  | Hwy 24 Southbound |  |  |  |  | Judge Orr Rd Westbound |  |  |  |  | Hwy 24 Northbound |  |  |  |  | Judge Orr Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 6:30:00 AM to 8:15:00 AM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 6:45:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:45:00 AM | 4 | 173 | 3 | 0 | 180 | 0 | 10 | 20 | 0 | 30 | 18 | 92 | 8 | 0 | 118 | 34 | 10 | 4 | 0 | 48 | 376 |
| 7:00:00 AM | 2 | 132 | 0 | 0 | 134 | 3 | 7 | 39 | 0 | 49 | 18 | 98 | 23 | 0 | 139 | 50 | 16 | 9 | 0 | 75 | 397 |
| 7:15:00 AM | 3 | 137 | 2 | 0 | 142 | 1 | 23 | 26 | 0 | 50 | 19 | 82 | 18 | 0 | 119 | 43 | 16 | 2 | 0 | 61 | 372 |
| 7:30:00 AM | 9 | 137 | 2 | 0 | 148 | 0 | 17 | 30 | 0 | 47 | 9 | 71 | 24 | 0 | 104 | 51 | 20 | 0 | 0 | 71 | 370 |
| Total Volume | 18 | 579 | 7 | 0 | 604 | 4 | 57 | 115 | 0 | 176 | 64 | 343 | 73 | 0 | 480 | 178 | 62 | 15 | 0 | 255 | 1515 |
| \% App. Total | 3 | 95.9 | 1.2 | 0 |  | 2.3 | 32.4 | 65.3 | 0 |  | 13.3 | 71.5 | 15.2 | 0 |  | 69.8 | 24.3 | 5.9 | 0 |  |  |
| PHF | . 500 | . 837 | . 583 | . 000 | . 839 | . 333 | . 620 | . 737 | . 000 | . 880 | . 842 | . 875 | . 760 | . 000 | . 863 | . 873 | . 775 | . 417 | . 000 | . 850 | . 954 |



# LSC Transportation Consultants, Inc. 

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : hwy 24 - judge orr rd am
Site Code : S214950
Start Date : 5/10/2022
Page No : 3

|  | Hwy 24Southbound |  |  |  |  | Judge Orr Rd Westbound |  |  |  |  | Hwy 24 Northbound |  |  |  |  | Judge Orr Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 6:30:00 AM to 8:15:00 AM - Peak 1 of 1 Peak Hour for Each Approach Begins at: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 6:45:00 AN |  |  |  |  | 7:00:00 AM |  |  |  |  | 6:45:00 AM |  |  |  |  | 6:45:00 AM |  |  |  |  |  |
| +0 mins. | 4 | 173 | 3 | 0 | 180 | 3 | 7 | 39 | 0 | 49 | 18 | 92 | 8 | 0 | 118 | 34 | 10 | 4 | 0 | 48 |  |
| +5 mins. | 2 | 132 | 0 | 0 | 134 | 1 | 23 | 26 | 0 | 50 | 18 | 98 | 23 | 0 | 139 | 50 | 16 | 9 | 0 | 75 |  |
| +10 mins. | 3 | 137 | 2 | 0 | 142 | 0 | 17 | 30 | 0 | 47 | 19 | 82 | 18 | 0 | 119 | 43 | 16 | 2 | 0 | 61 |  |
| +15 mins. | 9 | 137 | 2 | 0 | 148 | 1 | 15 | 15 | 0 | 31 | 9 | 71 | 24 | 0 | 104 | 51 | 20 | 0 | 0 | 71 |  |
| Total Volume | 18 | 579 | 7 | 0 | 604 | 5 | 62 | 110 | 0 | 177 | 64 | 343 | 73 | 0 | 480 | 178 | 62 | 15 | 0 | 255 |  |
| \% App. Total | 3 | 95.9 | 1.2 | 0 |  | 2.8 | 35 | 62.1 | 0 |  | 13.3 | 71.5 | 15.2 | 0 |  | 69.8 | 24.3 | 5.9 | 0 |  |  |
| PHF | . 500 | . 837 | . 583 | . 000 | . 839 | . 417 | . 674 | . 705 | . 000 | . 885 | . 842 | . 875 | . 760 | . 000 | . 863 | . 873 | . 775 | . 417 | . 000 | . 850 |  |



# LSC Transportation Consultants, Inc. <br> 2504 E. Pikes Peak Ave, Suite 304 <br> Colorado Springs, CO 80909 <br> 719-633-2868 

File Name : Hwy 24 - Judge Orr Rd PM
Site Code : S214950
Start Date : 5/10/2022
Page No : 1

Groups Printed- Unshifted

|  | Hwy 24 Southbound |  |  |  |  | Judge Orr Rd Westbound |  |  |  |  | Hwy 24 Northbound |  |  |  |  | Judge Orr Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | ${ }^{\text {App }}$ Total | Right | Thru | Left | Peds | ${ }_{\text {App }}$ Toaal | Right | Thru | Left | Peds | App. T | Int. Total |
| 16:00 | 5 | 77 | 2 | 0 | 84 | 1 | 7 | 22 | 0 | 30 | 33 | 143 | 24 | 0 | 200 | 10 | 7 | 5 | 0 | 22 | 336 |
| 16:15 | 3 | 105 | 1 | 0 | 109 | 5 | 17 | 25 | 0 | 47 | 27 | 152 | 30 | 0 | 209 | 21 | 11 | 11 | 0 | 43 | 408 |
| 16:30 | 7 | 105 | 1 | 0 | 113 | 1 | 14 | 29 | 0 | 44 | 34 | 144 | 34 | 1 | 213 | 18 | 11 | 11 | 0 | 40 | 410 |
| 16:45 | 1 | 101 | 0 | 0 | 102 | 2 | 9 | 24 | 0 | 35 | 31 | 135 | 41 | 0 | 207 | 15 | 13 | 12 | 0 | 40 | 384 |
| Total | 16 | 388 | 4 | 0 | 408 | 9 | 47 | 100 | 0 | 156 | 125 | 574 | 129 | 1 | 829 | 64 | 42 | 39 | 0 | 145 | 1538 |
| 17:00 | 2 | 99 | 0 | 0 | 101 | 4 | 13 | 38 | 0 | 55 | 29 | 147 | 40 | 0 | 216 | 16 | 16 | 10 | 0 | 42 | 414 |
| 17:15 | 7 | 127 | 0 | 0 | 134 | 2 | 16 | 26 | 0 | 44 | 34 | 133 | 24 | 1 | 192 | 13 | 11 | 7 | 0 | 31 | 401 |
| 17:30 | 6 | 91 | 1 | 0 | 98 | 2 | 6 | 16 | 0 | 24 | 39 | 149 | 32 | 0 | 220 | 10 | 15 | 10 | 0 | 35 | 377 |
| 17:45 | 6 | 98 | 0 | 0 | 104 | 0 | 5 | 22 | 0 | 27 | 29 | 158 | 30 | 0 | 217 | 11 | 17 | 8 | 0 | 36 | 384 |
| Total | 21 | 415 | 1 | 0 | 437 | 8 | 40 | 102 | 0 | 150 | 131 | 587 | 126 | 1 | 845 | 50 | 59 | 35 | 0 | 144 | 1576 |
| Grand Total | 37 | 803 | 5 | 0 | 845 | 17 | 87 | 202 | 0 | 306 | 256 | 1161 | 255 | 2 | 1674 | 114 | 101 | 74 | 0 | 289 | 3114 |
| Apprch \% | 4.4 | 95 | 0.6 | 0 |  | 5.6 | 28.4 | 66 | 0 |  | 15.3 | 69.4 | 15.2 | 0.1 |  | 39.4 | 34.9 | 25.6 | 0 |  |  |
| Total \% | 1.2 | 25.8 | 0.2 | 0 | 27.1 | 0.5 | 2.8 | 6.5 | 0 | 9.8 | 8.2 | 37.3 | 8.2 | 0.1 | 53.8 | 3.7 | 3.2 | 2.4 | 0 | 9.3 |  |

# LSC Transportation Consultants, Inc. <br> 2504 E. Pikes Peak Ave, Suite 304 <br> Colorado Springs, CO 80909 <br> 719-633-2868 

File Name : Hwy 24 - Judge Orr Rd PM
Site Code : S214950
Start Date : 5/10/2022
Page No : 2

|  | Hwy 24 Southbound |  |  |  |  | Judge Orr Rd Westbound |  |  |  |  | Hwy 24 Northbound |  |  |  |  | Judge Orr Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 4:00:00 PM to 5:45:00 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 4:15:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4:15:00 PM | 3 | 105 | 1 | 0 | 109 | 5 | 17 | 25 | 0 | 47 | 27 | 152 | 30 | 0 | 209 | 21 | 11 | 11 | 0 | 43 | 408 |
| 4:30:00 PM | 7 | 105 | 1 | 0 | 113 | 1 | 14 | 29 | 0 | 44 | 34 | 144 | 34 | 1 | 213 | 18 | 11 | 11 | 0 | 40 | 410 |
| 4:45:00 PM | 1 | 101 | 0 | 0 | 102 | 2 | 9 | 24 | 0 | 35 | 31 | 135 | 41 | 0 | 207 | 15 | 13 | 12 | 0 | 40 | 384 |
| 5:00:00 PM | 2 | 99 | 0 | 0 | 101 | 4 | 13 | 38 | 0 | 55 | 29 | 147 | 40 | 0 | 216 | 16 | 16 | 10 | 0 | 42 | 414 |
| Total Volume | 13 | 410 | 2 | 0 | 425 | 12 | 53 | 116 | 0 | 181 | 121 | 578 | 145 | 1 | 845 | 70 | 51 | 44 | 0 | 165 | 1616 |
| \% App. Total | 3.1 | 96.5 | 0.5 | 0 |  | 6.6 | 29.3 | 64.1 | 0 |  | 14.3 | 68.4 | 17.2 | 0.1 |  | 42.4 | 30.9 | 26.7 | 0 |  |  |
| PHF | . 464 | . 976 | . 500 | . 000 | . 940 | . 600 | . 779 | . 763 | . 000 | . 823 | . 890 | . 951 | . 884 | . 250 | . 978 | . 833 | . 797 | . 917 | . 000 | . 959 | . 976 |



# LSC Transportation Consultants, Inc. <br> 2504 E. Pikes Peak Ave, Suite 304 <br> Colorado Springs, CO 80909 <br> 719-633-2868 

File Name : Hwy 24 - Judge Orr Rd PM
Site Code : S214950
Start Date : 5/10/2022
Page No : 3

|  | Hwy 24Southbound |  |  |  |  | Judge Orr Rd Westbound |  |  |  |  | Hwy 24 Northbound |  |  |  |  | Judge Orr Rd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 4:00:00 PM to 5:45:00 PM - Peak 1 of 1 Peak Hour for Each Approach Begins at: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 4:30:00 PM |  |  |  |  | 4:15:00 PM |  |  |  |  | 4:15:00 PM |  |  |  |  | 4:15:00 PM |  |  |  |  |  |
| +0 mins. | 7 | 105 | 1 | 0 | 113 | 5 | 17 | 25 | 0 | 47 | 27 | 152 | 30 | 0 | 209 | 21 | 11 | 11 | 0 | 43 |  |
| +5 mins. | 1 | 101 | 0 | 0 | 102 | 1 | 14 | 29 | 0 | 44 | 34 | 144 | 34 | 1 | 213 | 18 | 11 | 11 | 0 | 40 |  |
| +10 mins. | 2 | 99 | 0 | 0 | 101 | 2 | 9 | 24 | 0 | 35 | 31 | 135 | 41 | 0 | 207 | 15 | 13 | 12 | 0 | 40 |  |
| +15 mins. | 7 | 127 | 0 | 0 | 134 | 4 | 13 | 38 | 0 | 55 | 29 | 147 | 40 | 0 | 216 | 16 | 16 | 10 | 0 | 42 |  |
| Total Volume | 17 | 432 | 1 | 0 | 450 | 12 | 53 | 116 | 0 | 181 | 121 | 578 | 145 | 1 | 845 | 70 | 51 | 44 | 0 | 165 |  |
| \% App. Total | 3.8 | 96 | 0.2 | 0 |  | 6.6 | 29.3 | 64.1 | 0 |  | 14.3 | 68.4 | 17.2 | 0.1 |  | 42.4 | 30.9 | 26.7 | 0 |  |  |
| PHF | . 607 | . 850 | . 250 | . 000 | . 840 | . 600 | . 779 | . 763 | . 000 | . 823 | . 890 | . 951 | . 884 | . 250 | . 978 | . 833 | . 797 | . 917 | . 000 | . 959 |  |

# LSC Transportation Consultants, Inc. <br> 2504 E. Pikes Peak Ave, Suite 304 <br> Colorado Springs, CO 80909 <br> 719-633-2868 

File Name : Eastonville Rd - Judge Orr Rd AM
Site Code : S220400
Start Date: 7/7/2022
Page No : 1

Groups Printed- Unshifted

|  | Eastonville Rd Southbound |  |  |  |  | Judge Orr Rd Westbound |  |  |  |  | Eastonville Rd Northbound |  |  |  |  | Meridian Ranch Blvd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | App. Toatal | int. Total |
| 06:30 | 1 | 9 | 11 | 0 | 21 | 6 | 7 | 4 | 0 | 17 | 6 | 3 | 2 | 0 | 11 | 12 | 33 | 0 | 0 | 45 | 94 |
| 06:45 | 1 | 12 | 7 | 0 | 20 | 9 | 4 | 2 | 0 | 15 | 7 | 3 | 2 | 0 | 12 | 12 | 29 | 0 | 0 | 41 | 88 |
| Total | 2 | 21 | 18 | 0 | 41 | 15 | 11 | 6 | 0 | 32 | 13 | 6 | 4 | 0 | 23 | 24 | 62 | 0 | 0 | 86 | 182 |
| 07:00 | 1 | 10 | 14 | 0 | 25 | 4 | 5 | 4 | 0 | 13 | 9 | 2 |  | 0 | 15 | 17 | 41 | 0 | 0 | 58 | 111 |
| 07:15 | 0 | 11 | 6 | 0 | 17 | 3 | 3 | 2 | 0 | 8 | 10 | 7 | 4 | 0 | 21 | 22 | 34 | 0 | 0 | 56 | 102 |
| 07:30 | 0 | 10 | 9 | 0 | 19 | 4 | 5 | 4 | 0 | 13 | 1 | 4 | 8 | 0 | 13 | 18 | 28 | 2 | 0 | 48 | 93 |
| 07:45 | 1 | 11 | 11 | 0 | 23 | 1 | 8 | 3 | 0 | 12 | 7 | 7 | 7 | 0 | 21 | 23 | 23 | 0 | 0 | 46 | 102 |
| Total | 2 | 42 | 40 | 0 | 84 | 12 | 21 | 13 | 0 | 46 | 27 | 20 | 23 | 0 | 70 | 80 | 126 | 2 | 0 | 208 | 408 |
| 08:00 | 0 | 11 | 7 | 0 | 18 | 4 | 8 | 5 | 0 | 17 | 5 | 9 | 8 | 0 | 22 | 14 | 24 | 2 | 0 | 40 | 97 |
| 08:15 | 0 | 10 | 11 | 0 | 21 | 0 | 8 | 3 | 0 | 11 | 4 | 6 | 10 | 0 | 20 | 9 | 27 | 0 | 0 | 36 | 88 |
| Grand Total | 4 | 84 | 76 | 0 | 164 | 31 | 48 | 27 | 0 | 106 | 49 | 41 | 45 | 0 | 135 | 127 | 239 | 4 | 0 | 370 | 775 |
| Apprch \% | 2.4 | 51.2 | 46.3 | 0 |  | 29.2 | 45.3 | 25.5 | 0 |  | 36.3 | 30.4 | 33.3 | 0 |  | 34.3 | 64.6 | 1.1 | 0 |  |  |
| Total \% | 0.5 | 10.8 | 9.8 | 0 | 21.2 |  | 6.2 | 3.5 | 0 | 13.7 | 6.3 | 5.3 | 5.8 | , | 17.4 | 16.4 | 30.8 | 0.5 | 0 | 47.7 |  |

# LSC Transportation Consultants, Inc. 

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : Eastonville Rd - Judge Orr Rd AM
Site Code : S220400
Start Date : 7/7/2022
Page No : 2

|  | Eastonville Rd Southbound |  |  |  |  | Judge Orr Rd Westbound |  |  |  |  | Eastonville Rd Northbound |  |  |  |  | Meridian Ranch Blvd Eastbound |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | App. Toal |  |
| Peak Hour Analysis From 6:30:00 AM to 8:15:00 AM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 7:00:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:00:00 AM | 1 | 10 | 14 | 0 | 25 | 4 | 5 | 4 | 0 | 13 | 9 | 2 | 4 | 0 | 15 | 17 | 41 | 0 | 0 | 58 | 111 |
| 7:15:00 AM | 0 | 11 | 6 | 0 | 17 | 3 | 3 | 2 | 0 | 8 | 10 | 7 | 4 | 0 | 21 | 22 | 34 | 0 | 0 | 56 | 102 |
| 7:30:00 AM | 0 | 10 | 9 | 0 | 19 | 4 | 5 | 4 | 0 | 13 | 1 | 4 | 8 | 0 | 13 | 18 | 28 | 2 | 0 | 48 | 93 |
| 7:45:00 AM | 1 | 11 | 11 | 0 | 23 | 1 | 8 | 3 | 0 | 12 | 7 | 7 | 7 | 0 | 21 | 23 | 23 | 0 | 0 | 46 | 102 |
| Total Volume | 2 | 42 | 40 | 0 | 84 | 12 | 21 | 13 | 0 | 46 | 27 | 20 | 23 | 0 | 70 | 80 | 126 | 2 | 0 | 208 | 408 |
| \% App. Total | 2.4 | 50 | 47.6 | 0 |  | 26.1 | 45.7 | 28.3 | 0 |  | 38.6 | 28.6 | 32.9 | 0 |  | 38.5 | 60.6 | 1 | 0 |  |  |
| PHF | . 500 | . 955 | . 714 | . 000 | . 840 | . 750 | . 656 | . 813 | . 000 | . 885 | . 675 | . 714 | . 719 | 000 | . 833 | . 870 | . 768 | . 250 | . 000 | 897 | . 919 |



## LSC Transportation Consultants, Inc.

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : Eastonville Rd - Judge Orr Rd AM
Site Code : S220400
Start Date : 7/7/2022
Page No : 3

|  | Eastonville Rd Southbound |  |  |  |  | Judge Orr Rd Westbound |  |  |  |  | Eastonville Rd Northbound |  |  |  |  | Meridian Ranch BIvd Eastbound |  |  |  |  | int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | Apo. Toal | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | App. Toal |  |
| Peak Hour Analysis From 6:30:00 AM to 8:15:00 AM - Peak 1 of 1 Peak Hour for Each Approach Begins at: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| +0 mins. | $\begin{array}{\|c\|c\|} \hline \text { 7.00.0.0 AM } \\ \hline \end{array}$ | 10 | 14 | 0 | 25 | ${ }^{\text {6:30:00 am }} 6$ | 7 | 4 | 0 | 17 | ${ }^{\text {7:15:00 AM }}$ | 7 | 4 | 0 | 21 | 7:00:00 AM 17 | 41 | 0 | 0 | 58 |  |
| +5 mins. | 0 | 11 | 6 | 0 | 17 | 9 | 4 | 2 | 0 | 15 | 1 | 4 | 8 | 0 | 13 | 22 | 34 | 0 | 0 | 56 |  |
| +10 mins. | 0 | 10 | 9 | 0 | 19 | 4 | 5 | 4 | 0 | 13 | 7 | 7 | 7 | 0 | 21 | 18 | 28 | 2 | 0 | 48 |  |
| +15 mins. | 1 | 11 | 11 | 0 | 23 | 3 | 3 | 2 | 0 | 8 | 5 | 9 | 8 | 0 | 22 | 23 | 23 | 0 | 0 | 46 |  |
| Total Volume | 2 | 42 | 40 | 0 | 84 | 22 | 19 | 12 | 0 | 53 | 23 | 27 | 27 | 0 | 77 | 80 | 126 | 2 | 0 | 208 |  |
| \% App. Total | 2.4 | 50 | 47.6 | 0 |  | 41.5 | 35.8 | 22.6 | 0 |  | 29.9 | 35.1 | 35.1 | 0 |  | 38.5 | 60.6 | 1 | 0 |  |  |
| PHF | . 500 | . 955 | . 714 | . 000 | . 840 | . 611 | . 679 | . 750 | . 000 | . 779 | . 575 | . 750 | . 844 | . 000 | . 875 | . 870 | . 768 | . 250 | . 000 | . 897 |  |


|  |  |  |
| :---: | :---: | :---: |
|  | Peak Hour Data <br> Unshifted |  |
|  |  |  |

# LSC Transportation Consultants, Inc. <br> 2504 E. Pikes Peak Ave, Suite 304 <br> Colorado Springs, CO 80909 <br> 719-633-2868 

File Name : Eastonville Rd - Judge Orr Rd PM
Site Code : S224400
Start Date : 6/22/2022
Page No : 1

Groups Printed- Unshifted

|  | Eastonville Rd Southbound |  |  |  |  | Judge Orr Rd Westbound |  |  |  |  | Eastonville Rd Northbound |  |  |  |  | Meridian Ranch BIvd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Toala | Right | Thru | Left | Peds | Apo. Toal | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | App. Toala | Int. Total |
| 16:00 | 0 | 16 | 4 | 0 | 20 | 10 | 31 | 8 | 0 | 49 | 11 | 28 | 31 | 0 | 70 | 21 | 12 | 1 | 0 | 34 | 173 |
| 16:15 | 1 | 13 | 6 | 0 | 20 | 8 | 32 | 8 | 0 | 48 | 13 | 33 | 21 | 0 | 67 | 16 | 14 | 0 | 0 | 30 | 165 |
| 16:30 | 1 | 15 | 2 | 0 | 18 | 15 | 24 | 7 | 0 | 46 | 10 | 46 | 49 | 0 | 105 | 17 | 16 | 0 | 0 | 33 | 202 |
| 16:45 | 0 | 15 | 7 | 0 | 22 | 11 | 31 | 10 | 0 | 52 | 15 | 32 | 43 | 0 | 90 | 30 | 13 | 0 | 0 | 43 | 207 |
| Total | 2 | 59 | 19 | 0 | 80 | 44 | 118 | 33 | 0 | 195 | 49 | 139 | 144 | 0 | 332 | 84 | 55 |  | 0 | 140 | 747 |
| 17:00 | 0 | 11 | 1 | 0 | 12 | 9 | 32 | 8 | 0 | 49 | 14 | 37 | 35 | 0 | 86 | 14 | 18 | 1 | 0 | 33 | 180 |
| 17:15 | 0 | 9 | 5 | 0 | 14 | 10 | 41 | 10 | 0 | 61 | 13 | 41 | 49 | 0 | 103 | 25 | 15 | 2 | 0 | 42 | 220 |
| 17:30 | 0 | 11 | 5 | 0 | 16 | 17 | 26 | 9 | 0 | 52 | 11 | 50 | 44 | 0 | 105 | 20 | 11 | 0 | 1 | 32 | 205 |
| 17:45 | 2 | 13 | 4 | 0 | 19 | 9 | 18 | 7 | 0 | 34 | 11 | 48 | 49 | 0 | 108 | 25 | 15 | 0 | 0 | 40 | 201 |
| Total | 2 | 44 | 15 | 0 | 61 | 45 | 117 | 34 | 0 | 196 | 49 | 176 | 177 | 0 | 402 | 84 | 59 | 3 | 1 | 147 | 806 |
| Grand Total | 4 | 103 | 34 | 0 | 141 | 89 | 235 | 67 | 0 | 391 | 98 | 315 | 321 | 0 | 734 | 168 | 114 | 4 | 1 | 287 | 1553 |
| Apprch \% | 2.8 | 73 | 24.1 | 0 |  | 22.8 | 60.1 | 17.1 | 0 |  | 13.4 | 42.9 | 43.7 | 0 |  | 58.5 | 39.7 | 1.4 | 0.3 |  |  |
| Total \% | 0.3 | 6.6 | 2.2 | 0 | 9.1 | 5.7 | 15.1 | 4.3 | 0 | 25.2 | 6.3 | 20.3 | 20.7 | 0 | 47.3 | 10.8 | 7.3 | 0.3 | 0.1 | 18.5 |  |

# LSC Transportation Consultants, Inc. 

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : Eastonville Rd - Judge Orr Rd PM
Site Code : S224400
Start Date : 6/22/2022
Page No : 2

|  | Eastonville Rd Southbound |  |  |  |  | Judge Orr Rd Westbound |  |  |  |  | Eastonville Rd Northbound |  |  |  |  | Meridian Ranch Blvd Eastbound |  |  |  |  | int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | po. Total | Right | Thru | Left | Peds | App. Toal | Right | Thru | Left | Peds | Pot | Right | Thru | Left | Peds | App. Toal |  |
| Peak Hour Analysis From 4:00:00 PM to 5:45:00 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 4:45:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4:45:00 PM | 0 | 15 | 7 | 0 | 22 | 11 | 31 | 10 | 0 | 52 | 15 | 32 | 43 | 0 | 90 | 30 | 13 | 0 | 0 | 43 | 207 |
| 5:00:00 PM | 0 | 11 | 1 | 0 | 12 | 9 | 32 | 8 | 0 | 49 | 14 | 37 | 35 | 0 | 86 | 14 | 18 | 1 | 0 | 33 | 180 |
| 5:15:00 PM | 0 | 9 | 5 | 0 | 14 | 10 | 41 | 10 | 0 | 61 | 13 | 41 | 49 | 0 | 103 | 25 | 15 | 2 | 0 | 42 | 220 |
| 5:30:00 PM | 0 | 11 | 5 | 0 | 16 | 17 | 26 | 9 | 0 | 52 | 11 | 50 | 44 | 0 | 105 | 20 | 11 | 0 | 1 | 32 | 205 |
| Total Volume | 0 | 46 | 18 | 0 | 64 | 47 | 130 | 37 | 0 | 214 | 53 | 160 | 171 | 0 | 384 | 89 | 57 | 3 | 1 | 150 | 812 |
| \% App. Total | 0 | 71.9 | 28.1 | 0 |  | 22 | 60.7 | 17.3 | 0 |  | 13.8 | 41.7 | 44.5 | 0 |  | 59.3 | 38 | 2 | 0.7 |  |  |
| PHF | . 000 | . 767 | . 643 | . 000 | . 727 | . 691 | . 793 | . 925 | . 000 | . 877 | . 883 | . 800 | . 872 | . 000 | . 914 | . 742 | . 792 | . 375 | . 250 | . 872 | . 923 |



## LSC Transportation Consultants, Inc.

2504 E. Pikes Peak Ave, Suite 304
Colorado Springs, CO 80909
719-633-2868
File Name : Eastonville Rd - Judge Orr Rd PM
Site Code : S224400
Start Date : 6/22/2022
Page No : 3

|  | Eastonville Rd Southbound |  |  |  |  | Judge Orr Rd Westbound |  |  |  |  | Eastonville Rd Northbound |  |  |  |  | Meridian Ranch BIvd Eastbound |  |  |  |  | lnt. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Peak Hour Analysis From 4:00:00 PM to 5:45:00 PM - Peak 1 of 1 Peak Hour for Each Approach Begins at: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| +0 mins. | ${ }^{4.00: 00 ~ P M ~}$ | 16 | 4 | 0 | 20 | 4.4500 PM 11 | 31 | 10 | 0 | 52 | ${ }^{\text {5.00.00 PM }} 14$ | 37 | 35 | 0 | 86 | 4.30.00 PM 17 | 16 | 0 | 0 | 33 |  |
| +5 mins. | 1 | 13 | 6 | 0 | 20 | 9 | 32 | 8 | 0 | 49 | 13 | 41 | 49 | 0 | 103 | 30 | 13 | 0 | 0 | 43 |  |
| +10 mins. | 1 | 15 | 2 | 0 | 18 | 10 | 41 | 10 | 0 | 61 | 11 | 50 | 44 | 0 | 105 | 14 | 18 | 1 | 0 | 33 |  |
| +15 mins. | 0 | 15 | 7 | 0 | 22 | 17 | 26 | 9 | 0 | 52 | 11 | 48 | 49 | 0 | 108 | 25 | 15 | 2 | 0 | 42 |  |
| Total Volume | 2 | 59 | 19 | 0 | 80 | 47 | 130 | 37 | 0 | 214 | 49 | 176 | 177 | 0 | 402 | 86 | 62 | 3 | 0 | 151 |  |
| \% App. Total | 2.5 | 73.8 | 23.8 | 0 |  | 22 | 60.7 | 17.3 | 0 |  | 12.2 | 43.8 | 44 | 0 |  | 57 | 41.1 | 2 | 0 |  |  |
| PHF | . 500 | . 922 | . 679 | . 000 | . 909 | . 691 | . 793 | . 925 | . 000 | . 877 | . 875 | . 880 | . 903 | . 000 | . 931 | . 717 | . 861 | . 375 | . 000 | . 878 |  |


|  |  |  |
| :---: | :---: | :---: |
|  | Peak Hour Data <br> Unshifted |  |
|  |  |  |


|  | $\rightarrow$ | $\rightarrow$ | 2 | $\cdots$ |  |  |  | $\nearrow$ | $\rho$ | 4 |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  | $\dagger$ |  |  | $\uparrow$ |  | \% | $\uparrow$ |  | \% | 1 |  |
| Traffic Volume (vph) | 15 | 62 | 178 | 115 | 57 | 4 | 73 | 343 | 64 | 7 | 579 | 18 |
| Future Volume (vph) | 15 | 62 | 178 | 115 | 57 | 4 | 73 | 343 | 64 | 7 | 579 | 18 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 860 |  | 0 | 695 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 300 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.906 |  |  | 0.997 |  |  | 0.976 |  |  | 0.996 |  |
| Flt Protected |  | 0.997 |  |  | 0.969 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1683 | 0 | 0 | 1800 | 0 | 1770 | 1818 | 0 | 1770 | 1855 | 0 |
| Flt Permitted |  | 0.997 |  |  | 0.969 |  | 0.120 |  |  | 0.506 |  |  |
| Satd. Flow (perm) | 0 | 1683 | 0 | 0 | 1800 | 0 | 224 | 1818 | 0 | 943 | 1855 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 112 |  |  | , |  |  | 14 |  |  | 2 |  |
| Link Speed (mph) |  | 45 |  |  | 45 |  |  | 55 |  |  | 55 |  |
| Link Distance (ft) |  | 2032 |  |  | 1524 |  |  | 1735 |  |  | 2505 |  |
| Travel Time (s) |  | 30.8 |  |  | 23.1 |  |  | 21.5 |  |  | 31.1 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.87 | 0.87 | 0.87 | 0.92 | 0.92 | 0.92 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 16 | 67 | 193 | 132 | 66 | 5 | 79 | 373 | 70 | 8 | 623 | 19 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 276 | 0 | 0 | 203 | 0 | 79 | 443 | 0 | 8 | 642 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(ft) |  | 0 |  |  | 0 |  |  | 12 |  |  | 12 |  |
| Link Offset(ft) |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width(ft) |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Number of Detectors | 1 | 2 |  | 1 | 2 |  | 1 | 2 |  | 1 | 2 |  |
| Detector Template | Left | Thru |  | Left | Thru |  | Left | Thru |  | Left | Thru |  |
| Leading Detector (ft) | 20 | 100 |  | 20 | 100 |  | 20 | 100 |  | 20 | 100 |  |
| Trailing Detector ( t ) | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Detector 1 Position(ft) | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Detector 1 Size(ft) | 20 | 6 |  | 20 | 6 |  | 20 | 6 |  | 20 | 6 |  |
| Detector 1 Type | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ |  | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ |  | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ |  | $\mathrm{Cl}+\mathrm{Ex}$ | Cl+Ex |  |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Detector 1 Queue (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Detector 1 Delay (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Detector 2 Position(ft) |  | 94 |  |  | 94 |  |  | 94 |  |  | 94 |  |
| Detector 2 Size(ft) |  | 6 |  |  | 6 |  |  | 6 |  |  | 6 |  |
| Detector 2 Type |  | Cl+Ex |  |  | Cl+Ex |  |  | Cl+Ex |  |  | Cl+Ex |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | Split | NA |  | Split | NA |  | pm+pt | NA |  | Perm | NA |  |
| Protected Phases | 4 | 4 |  | 8 | 8 |  | 5 | 2 |  |  | 6 |  |
| Permitted Phases |  |  |  |  |  |  | 2 |  |  | 6 |  |  |


|  | $\rightarrow$ |  | 7 | $\ldots$ |  |  | * | $\nearrow$ |  | 4 | $\lambda$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 5 | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 9.5 | 24.0 |  | 24.0 | 24.0 |  |
| Total Split (s) | 21.0 | 21.0 |  | 21.0 | 21.0 |  | 10.0 | 48.0 |  | 38.0 | 38.0 |  |
| Total Split (\%) | 23.3\% | 23.3\% |  | 23.3\% | 23.3\% |  | 11.1\% | 53.3\% |  | 42.2\% | 42.2\% |  |
| Maximum Green (s) | 15.0 | 15.0 |  | 15.0 | 15.0 |  | 5.5 | 42.0 |  | 32.0 | 32.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 3.5 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 1.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 6.0 |  |  | 6.0 |  | 4.5 | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  | Lead |  |  | Lag | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes |  |  | Yes | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | None | Max |  | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  |  | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  |  | 11.0 |  | 11.0 | 11.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | , | 0 |  |  | 0 |  | 0 | 0 |  |
| Act Effct Green (s) |  | 12.7 |  |  | 13.3 |  | 43.7 | 42.2 |  | 34.4 | 34.4 |  |
| Actuated g/C Ratio |  | 0.15 |  |  | 0.15 |  | 0.51 | 0.49 |  | 0.40 | 0.40 |  |
| V/c Ratio |  | 0.81 |  |  | 0.73 |  | 0.37 | 0.49 |  | 0.02 | 0.87 |  |
| Control Delay |  | 40.0 |  |  | 51.4 |  | 17.5 | 17.6 |  | 19.3 | 40.8 |  |
| Queue Delay |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay |  | 40.0 |  |  | 51.4 |  | 17.5 | 17.6 |  | 19.3 | 40.8 |  |
| LOS |  | D |  |  | D |  | B | B |  | B | D |  |
| Approach Delay |  | 40.0 |  |  | 51.4 |  |  | 17.6 |  |  | 40.5 |  |
| Approach LOS |  | D |  |  | D |  |  | B |  |  | D |  |
| Queue Length 50th (ft) |  | 88 |  |  | 109 |  | 23 | 165 |  | 3 | 353 |  |
| Queue Length 95th (t) |  | \#202 |  |  | \#179 |  | 47 | 252 |  | 12 | \#583 |  |
| Internal Link Dist (ft) |  | 1952 |  |  | 1444 |  |  | 1655 |  |  | 2425 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  | 860 |  |  | 695 |  |  |
| Base Capacity (vph) |  | 386 |  |  | 315 |  | 212 | 896 |  | 376 | 740 |  |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio |  | 0.72 |  |  | 0.64 |  | 0.37 | 0.49 |  | 0.02 | 0.87 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

## Area Type: Other

Cycle Length: 90
Actuated Cycle Length: 86.2
Natural Cycle: 95
Control Type: Actuated-Uncoordinated

## Maximum v/c Ratio: 0.87

Intersection Signal Delay: 34.5
Intersection LOS: C
Intersection Capacity Utilization 79.1\% ICU Level of Service D
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Splits and Phases: 2: US 24 \& Judge Orr Rd


| Intersection |  |
| :--- | :---: | :--- |
| Intersection Delay, s/veh | 16 |
| Intersection LOS | C |


| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\uparrow$ |  | 7 | $\uparrow$ | 「 | ${ }^{7}$ | $\hat{F}$ |  | 7 | F |  |
| Traffic Vol, veh/h | 100 | 150 | 100 | 25 | 50 | 100 | 25 | 200 | 50 | 75 | 175 | 10 |
| Future Vol, veh/h | 100 | 150 | 100 | 25 | 50 | 100 | 25 | 200 | 50 | 75 | 175 | 10 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.87 | 0.87 | 0.87 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 109 | 163 | 109 | 29 | 57 | 115 | 27 | 217 | 54 | 82 | 190 | 11 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 1 | 1 | 1 | 0 | 1 | 1 | 0 |
| Approach | SE |  |  | NW |  |  | NE |  |  | SW |  |  |
| Opposing Approach | NW |  |  | SE |  |  | SW |  |  | NE |  |  |
| Opposing Lanes | 3 |  |  | 2 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Left | SW |  |  | NE |  |  | SE |  |  | NW |  |  |
| Conflicting Lanes Left | 2 |  |  | 2 |  |  | 2 |  |  | 3 |  |  |
| Conflicting Approach Right | NE |  |  | SW |  |  | NW |  |  | SE |  |  |
| Conflicting Lanes Right | 2 |  |  | 2 |  |  | 3 |  |  | 2 |  |  |
| HCM Control Delay | 16.7 |  |  | 12.1 |  |  | 18.6 |  |  | 14.9 |  |  |
| HCMLOS | C |  |  | B |  |  | C |  |  | B |  |  |


| Lane | NELn1 | NELn2 | NWLn1 | NWLn2 | NWLn3 | SELn1 | SELn2 | SWLn1 | SWLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $100 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Thru, \% | $0 \%$ | $80 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $60 \%$ | $0 \%$ | $95 \%$ |
| Vol Right, \% | $0 \%$ | $20 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $40 \%$ | $0 \%$ | $5 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 25 | 250 | 25 | 50 | 100 | 100 | 250 | 75 | 185 |
| LT Vol | 25 | 0 | 25 | 0 | 0 | 100 | 0 | 75 | 0 |
| Through Vol | 0 | 200 | 0 | 50 | 0 | 0 | 150 | 0 | 175 |
| RT Vol | 0 | 50 | 0 | 0 | 100 | 0 | 100 | 0 | 10 |
| Lane Flow Rate | 27 | 272 | 29 | 57 | 115 | 109 | 272 | 82 | 201 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.061 | 0.56 | 0.068 | 0.127 | 0.232 | 0.24 | 0.541 | 0.184 | 0.423 |
| Departure Headway (Hd) | 8.066 | 7.415 | 8.49 | 7.977 | 7.258 | 7.964 | 7.165 | 8.128 | 7.58 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 443 | 486 | 421 | 448 | 493 | 450 | 503 | 440 | 475 |
| Service Time | 5.829 | 5.178 | 6.262 | 5.749 | 5.029 | 5.727 | 4.928 | 5.895 | 5.347 |
| HCM Lane V/C Ratio | 0.061 | 0.56 | 0.069 | 0.127 | 0.233 | 0.242 | 0.541 | 0.186 | 0.423 |
| HCM Control Delay | 11.4 | 19.3 | 11.9 | 11.9 | 12.2 | 13.2 | 18.1 | 12.7 | 15.8 |
| HCM Lane LOS | B | C | B | B | B | B | C | B | C |
| HCM 95th-tile Q | 0.2 | 3.4 | 0.2 | 0.4 | 0.9 | 0.9 | 3.2 | 0.7 | 2.1 |




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | ¢ |  |  | $\dagger$ |  | \% | $\hat{1}$ |  | 7 | $\hat{1}$ |  |
| Traffic Volume (vph) | 33 | 32 | 55 | 120 | 90 | 15 | 135 | 565 | 130 | 5 | 420 | 20 |
| Future Volume (vph) | 33 | 32 | 55 | 120 | 90 | 15 | 135 | 565 | 130 | 5 | 420 | 20 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 860 |  | 0 | 695 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 300 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.939 |  |  | 0.991 |  |  | 0.972 |  |  | 0.993 |  |
| Flt Protected |  | 0.986 |  |  | 0.974 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1725 | 0 | 0 | 1798 | 0 | 1770 | 1811 | 0 | 1770 | 1850 | 0 |
| Flt Permitted |  | 0.986 |  |  | 0.756 |  | 0.235 |  |  | 0.194 |  |  |
| Satd. Flow (perm) | 0 | 1725 | 0 | 0 | 1396 | 0 | 438 | 1811 | 0 | 361 | 1850 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 37 |  |  | 4 |  |  | 17 |  |  | 3 |  |
| Link Speed (mph) |  | 45 |  |  | 45 |  |  | 55 |  |  | 55 |  |
| Link Distance (ft) |  | 2032 |  |  | 1524 |  |  | 1735 |  |  | 2505 |  |
| Travel Time (s) |  | 30.8 |  |  | 23.1 |  |  | 21.5 |  |  | 31.1 |  |
| Peak Hour Factor | 0.83 | 0.83 | 0.83 | 0.87 | 0.87 | 0.87 | 0.93 | 0.93 | 0.93 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 40 | 39 | 66 | 138 | 103 | 17 | 145 | 608 | 140 | 5 | 457 | 22 |

Shared Lane Traffic (\%)
Lane Group Flow (vph)

| Number of Detectors | 1 | 2 | 1 | 2 | 1 | 2 | 1 | 2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Detector Template | Left | Thru | Left | Thru | Left | Thru | Left | Thru |
| Leading Detector (ft) | 20 | 100 | 20 | 100 | 20 | 100 | 20 | 100 |
| Trailing Detector (ft) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Detector 1 Position(ft) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Detector 1 Size(ft) | 20 | 6 | 20 | 6 | 20 | 6 | 20 | 6 |
| Detector 1 Type | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex |
| Detector 1 Channel |  |  |  |  |  |  |  |  |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(ft) |  | 94 |  | 94 |  | 94 |  | 94 |
| Detector 2 Size(ft) |  | 6 |  | 6 |  | 6 |  | 6 |
| Detector 2 Type |  | Cl+Ex |  | Cl+Ex |  | Cl+Ex |  | Cl+Ex |

Detector 2 Channel

| Detector 2 Extend (s) |  | 0.0 |  | 0.0 |  | 0.0 |  | 0.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Turn Type | Split | NA | Perm | NA | pm+pt | NA | Perm | NA |
| Protected Phases | 4 | 4 | 8 | 8 | 5 | 2 | 6 |  |
| Permitted Phases |  |  | 8 | 2 |  | 6 |  |  |


|  | $\rightarrow$ | $\rightarrow$ | 2 | $\cdots$ |  |  | * | $\not$ | $\bigcirc$ | 4 | $\chi$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 5 | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 9.5 | 24.0 |  | 24.0 | 24.0 |  |
| Total Split (s) | 14.0 | 14.0 |  | 28.0 | 28.0 |  | 10.6 | 48.0 |  | 37.4 | 37.4 |  |
| Total Split (\%) | 15.6\% | 15.6\% |  | 31.1\% | 31.1\% |  | 11.8\% | 53.3\% |  | 41.6\% | 41.6\% |  |
| Maximum Green (s) | 8.0 | 8.0 |  | 22.0 | 22.0 |  | 6.1 | 42.0 |  | 31.4 | 31.4 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 3.5 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 1.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 6.0 |  |  | 6.0 |  | 4.5 | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  | Lead |  |  | Lag | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes |  |  | Yes | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | None | Max |  | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  |  | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  |  | 11.0 |  | 11.0 | 11.0 |  |
| Pedestrian Calls (\#/hr) | 0 | , |  | 0 | 0 |  |  | 0 |  | 0 | 0 |  |
| Act Effct Green (s) |  | 7.8 |  |  | 19.3 |  | 43.6 | 42.1 |  | 31.5 | 31.5 |  |
| Actuated g/C Ratio |  | 0.09 |  |  | 0.22 |  | 0.50 | 0.48 |  | 0.36 | 0.36 |  |
| $\mathrm{v} / \mathrm{c}$ Ratio |  | 0.78 |  |  | 0.83 |  | 0.46 | 0.85 |  | 0.04 | 0.72 |  |
| Control Delay |  | 57.5 |  |  | 54.5 |  | 18.0 | 31.3 |  | 20.6 | 31.8 |  |
| Queue Delay |  | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay |  | 57.5 |  |  | 54.5 |  | 18.0 | 31.3 |  | 20.6 | 31.8 |  |
| LOS |  | E |  |  | D |  | B | C |  | C | C |  |
| Approach Delay |  | 57.5 |  |  | 54.5 |  |  | 29.1 |  |  | 31.7 |  |
| Approach LOS |  | E |  |  | D |  |  | C |  |  | C |  |
| Queue Length 50th (t) |  | 61 |  |  | 134 |  | 44 | 362 |  | 2 | 234 |  |
| Queue Length 95th (t) |  | \#136 |  |  | \#235 |  | 79 | \#597 |  | 10 | 352 |  |
| Internal Link Dist (ft) |  | 1952 |  |  | 1444 |  |  | 1655 |  |  | 2425 |  |
| Turn Bay Length ( ft ) |  |  |  |  |  |  | 860 |  |  | 695 |  |  |
| Base Capacity (vph) |  | 192 |  |  | 356 |  | 312 | 883 |  | 129 | 669 |  |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio |  | 0.76 |  |  | 0.72 |  | 0.46 | 0.85 |  | 0.04 | 0.72 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

## Area Type: Other

Cycle Length: 90
Actuated Cycle Length: 87.2
Natural Cycle: 85
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.85
Intersection Signal Delay: 35.8
Intersection LOS: D
Intersection Capacity Utilization $75.8 \% \quad$ ICU Level of Service $D$
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Splits and Phases: 2: US 24 \& Judge Orr Rd


|  |  |
| :--- | ---: | :--- |
| Intersection | 13.4 |
| Intersection Delay, s/veh | B |


| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\uparrow$ |  | \% | 4 | 「 | \% | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  |
| Traffic Vol, veh/h | 10 | 60 | 90 | 50 | 150 | 47 | 170 | 170 | 55 | 25 | 100 | 10 |
| Future Vol, veh/h | 10 | 60 | 90 | 50 | 150 | 47 | 170 | 170 | 55 | 25 | 100 | 10 |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.92 | 0.92 | 0.92 | 0.83 | 0.83 | 0.83 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 11 | 69 | 103 | 57 | 172 | 54 | 185 | 185 | 60 | 30 | 120 | 12 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 1 | 1 | 1 | 0 | 1 | 1 | 0 |
| Approach | SE |  |  | NW |  |  | NE |  |  | SW |  |  |
| Opposing Approach | NW |  |  | SE |  |  | SW |  |  | NE |  |  |
| Opposing Lanes | 3 |  |  | 2 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Left | SW |  |  | NE |  |  | SE |  |  | NW |  |  |
| Conflicting Lanes Left | 2 |  |  | 2 |  |  | 2 |  |  | 3 |  |  |
| Conflicting Approach Right | NE |  |  | SW |  |  | NW |  |  | SE |  |  |
| Conflicting Lanes Right | 2 |  |  | 2 |  |  | 3 |  |  | 2 |  |  |
| HCM Control Delay | 13.2 |  |  | 12.5 |  |  | 14.4 |  |  | 12.5 |  |  |
| HCM LOS | B |  |  | B |  |  | B |  |  | B |  |  |


| Lane | NELn1 | NELn2 | NWLn1 | NWLn2 | NWLn3 | SELn1 | SELn2 | SWLn1 | SWLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $100 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Thru, \% | $0 \%$ | $76 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $40 \%$ | $0 \%$ | $91 \%$ |
| Vol Right, \% | $0 \%$ | $24 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $60 \%$ | $0 \%$ | $9 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 170 | 225 | 50 | 150 | 47 | 10 | 150 | 25 | 110 |
| LT Vol | 170 | 0 | 50 | 0 | 0 | 10 | 0 | 25 | 0 |
| Through Vol | 0 | 170 | 0 | 150 | 0 | 0 | 60 | 0 | 100 |
| RT Vol | 0 | 55 | 0 | 0 | 47 | 0 | 90 | 0 | 10 |
| Lane Flow Rate | 185 | 245 | 57 | 172 | 54 | 11 | 172 | 30 | 133 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.374 | 0.448 | 0.123 | 0.344 | 0.097 | 0.025 | 0.336 | 0.066 | 0.27 |
| Departure Headway (Hd) | 7.28 | 6.601 | 7.688 | 7.179 | 6.465 | 7.961 | 7.019 | 7.906 | 7.333 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 497 | 548 | 467 | 502 | 554 | 450 | 512 | 453 | 490 |
| Service Time | 4.98 | 4.301 | 5.428 | 4.918 | 4.205 | 5.705 | 4.763 | 5.65 | 5.077 |
| HCM Lane V/C Ratio | 0.372 | 0.447 | 0.122 | 0.343 | 0.097 | 0.024 | 0.336 | 0.066 | 0.271 |
| HCM Control Delay | 14.3 | 14.5 | 11.5 | 13.7 | 9.9 | 10.9 | 13.3 | 11.2 | 12.8 |
| HCM Lane LOS | B | B | $B$ | $B$ | A | B | B | B | B |
| HCM 95th-tile Q | 1.7 | 2.3 | 0.4 | 1.5 | 0.3 | 0.1 | 1.5 | 0.2 | 1.1 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1 |  |  |  |  |  |
| Movement | SEL | SER | NEL | NET | SWT | SWR |
| Lane Configurations | M |  | 10 | 4 | 个 |  |
| Traffic Vol, veh/h | 10 | 10 | 25 | 202 | 125 | 20 |
| Future Vol, veh/h | 10 | 10 | 25 | 202 | 125 | 20 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 25 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 78 | 78 | 87 | 87 | 87 | 87 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 13 | 13 | 29 | 232 | 144 | 23 |


| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 446 | 156 | 167 | 0 | - | 0 |
| Stage 1 | 156 | - | - | - | - | - |
| Stage 2 | 290 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 570 | 890 | 1411 | - | - | - |
| Stage 1 | 872 | - | - | - | - | - |
| Stage 2 | 759 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 558 | 890 | 1411 | - | - | - |
| Mov Cap-2 Maneuver | 619 | - | - | - | - | - |
| Stage 1 | 854 | - | - | - | - | - |
| Stage 2 | 759 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | SE |  | NE |  | SW |  |
| HCM Control Delay, s | 10.1 |  | 0.8 |  | 0 |  |
| HCM LOS | B |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NEL | NET SELn1 |  | SWT | SWR |
| Capacity (veh/h) |  | 1411 | - | 730 | - | - |
| HCM Lane V/C Ratio |  | 0.02 | - | 0.035 | - | - |
| HCM Control Delay (s) |  | 7.6 | - | 10.1 | - | - |
| HCM Lane LOS |  | A | - | B | - | - |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | 0.1 | - | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 168 | 0 | 453 | 168 |
| Stage 1 | - | - | - |  | 168 | - |
| Stage 2 | - | - | - | - | 285 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1410 | - | 565 | 876 |
| Stage 1 | - | - | - |  | 862 | - |
| Stage 2 | - | - | - |  | 763 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1410 | - | 564 | 876 |
| Mov Cap-2 Maneuver | - | - | - | - | 564 | - |
| Stage 1 | - | - | - | - | 862 | - |
| Stage 2 | - | - | - | - | 762 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0 |  | 10.3 |  |
| HCM LOS |  |  |  |  | B |  |
| HCMLOS |  |  |  |  |  |  |
| Minor Lane/Major Mumt |  | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) |  | 686 | - | - | 1410 | - |
| HCM Lane V/C Ratio |  | 0.004 | - | - | 0.001 | - |
| HCM Control Delay (s) |  | 10.3 | - | - | 7.6 | 0 |
| HCM Lane LOS |  | B | - | - | A | A |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | 0 | - |


|  | $\rightarrow$ | $\rightarrow$ | 7 | $\cdots$ |  | $C$ | * | $\nearrow$ | $\rho$ | 4 | $\backslash$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  | $\uparrow$ | ${ }^{7}$ |  | \$ |  | \% | $\uparrow$ |  | 7 | F | 「 |
| Traffic Volume (vph) | 17 | 66 | 204 | 115 | 68 | 4 | 84 | 343 | 64 | 7 | 579 | 19 |
| Future Volume (vph) | 17 | 66 | 204 | 115 | 68 | 4 | 84 | 343 | 64 | 7 | 579 | 19 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 860 |  | 0 | 695 |  | 0 |
| Storage Lanes | 0 |  | 1 | 0 |  | 0 | 1 |  | 0 | 1 |  | 1 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 300 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 |
| Frt |  |  | 0.850 |  | 0.997 |  |  | 0.976 |  |  |  | 0.850 |
| Flt Protected |  | 0.990 |  |  | 0.970 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1844 | 1583 | 0 | 1801 | 0 | 1770 | 1818 | 0 | 1770 | 1770 | 1504 |
| Flt Permitted |  | 0.990 |  |  | 0.760 |  | 0.110 |  |  | 0.490 |  |  |
| Satd. Flow (perm) | 0 | 1844 | 1583 | 0 | 1411 | 0 | 205 | 1818 | 0 | 913 | 1770 | 1504 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 222 |  | 1 |  |  | 13 |  |  |  | 164 |
| Link Speed (mph) |  | 45 |  |  | 45 |  |  | 55 |  |  | 55 |  |
| Link Distance ( ft ) |  | 2032 |  |  | 1524 |  |  | 1735 |  |  | 2505 |  |
| Travel Time (s) |  | 30.8 |  |  | 23.1 |  |  | 21.5 |  |  | 31.1 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.87 | 0.87 | 0.87 | 0.92 | 0.92 | 0.92 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 18 | 72 | 222 | 132 | 78 | 5 | 91 | 373 | 70 | 8 | 623 | 20 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  | 10\% |
| Lane Group Flow (vph) | 0 | 90 | 222 | 0 | 215 | 0 | 91 | 443 | 0 | 8 | 625 | 18 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(ft) |  | 0 |  |  | 0 |  |  | 12 |  |  | 12 |  |
| Link Offset(ft) |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width(ft) |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 |  | 1 | 2 |  | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru |  | Left | Thru |  | Left | Thru | Right |
| Leading Detector (ft) | 20 | 100 | 20 | 20 | 100 |  | 20 | 100 |  | 20 | 100 | 20 |
| Trailing Detector (tt) | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Detector 1 Position(ft) | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Detector 1 Size(tt) | 20 | 6 | 20 | 20 | 6 |  | 20 | 6 |  | 20 | 6 | 20 |
| Detector 1 Type | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ |  | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ |  | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(ft) |  | 94 |  |  | 94 |  |  | 94 |  |  | 94 |  |
| Detector 2 Size(ft) |  | 6 |  |  | 6 |  |  | 6 |  |  | 6 |  |
| Detector 2 Type |  | $\mathrm{Cl}+\mathrm{Ex}$ |  |  | Cl+Ex |  |  | $\mathrm{Cl}+\mathrm{Ex}$ |  |  | Cl+Ex |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | Split | NA | Perm | Perm | NA |  | pm+pt | NA |  | Perm | NA | Perm |
| Protected Phases | 4 | 4 |  |  | 8 |  | 5 | 2 |  |  | 6 |  |
| Permitted Phases |  |  | 4 | 8 |  |  | 2 |  |  | 6 |  | 6 |
| Existing + Site AM <br> Lanes, Volumes, Timings |  |  |  |  |  |  |  |  |  |  | nchro 1 | Report JAB |


|  | $\rightarrow$ |  | 2 |  |  | $\longleftarrow$ | * | $\nearrow$ |  | 4 | $\chi$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| Detector Phase | 4 | 4 | 4 | 8 | 8 |  | 5 | 2 |  | 6 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 24.0 | 24.0 | 24.0 | 24.0 | 24.0 |  | 9.5 | 24.0 |  | 24.0 | 24.0 | 24.0 |
| Total Split (s) | 21.0 | 21.0 | 21.0 | 25.0 | 25.0 |  | 8.0 | 44.0 |  | 36.0 | 36.0 | 36.0 |
| Total Split (\%) | 23.3\% | 23.3\% | 23.3\% | 27.8\% | 27.8\% |  | 8.9\% | 48.9\% |  | 40.0\% | 40.0\% | 40.0\% |
| Maximum Green (s) | 15.0 | 15.0 | 15.0 | 19.0 | 19.0 |  | 3.5 | 38.0 |  | 30.0 | 30.0 | 30.0 |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 3.5 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 1.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | 0.0 | 0.0 |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) |  | 6.0 | 6.0 |  | 6.0 |  | 4.5 | 6.0 |  | 6.0 | 6.0 | 6.0 |
| Lead/Lag |  |  |  |  |  |  | Lead |  |  | Lag | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes |  |  | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | None |  | None | Max |  | Max | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |  | 7.0 |  | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 |  |  | 11.0 |  | 11.0 | 11.0 | 11.0 |
| Pedestrian Calls (\#/hr) | 0 | 0 | 0 | 0 | 0 |  |  | 0 |  | 0 | 0 | 0 |
| Act Effct Green (s) |  | 9.3 | 9.3 |  | 16.2 |  | 39.7 | 38.2 |  | 31.9 | 31.9 | 31.9 |
| Actuated g/C Ratio |  | 0.11 | 0.11 |  | 0.20 |  | 0.49 | 0.47 |  | 0.39 | 0.39 | 0.39 |
| V/c Ratio |  | 0.43 | 0.59 |  | 0.77 |  | 0.55 | 0.52 |  | 0.02 | 0.90 | 0.03 |
| Control Delay |  | 41.0 | 12.1 |  | 50.4 |  | 27.9 | 18.7 |  | 19.3 | 45.5 | 0.1 |
| Queue Delay |  | 0.0 | 0.0 |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 41.0 | 12.1 |  | 50.4 |  | 27.9 | 18.7 |  | 19.3 | 45.5 | 0.1 |
| LOS |  | D | B |  | D |  | C | B |  | B | D | A |
| Approach Delay |  | 20.4 |  |  | 50.4 |  |  | 20.3 |  |  | 43.9 |  |
| Approach LOS |  | C |  |  | D |  |  | C |  |  | D |  |
| Queue Length 50th (t) |  | 45 | 0 |  | 104 |  | 25 | 156 |  | 3 | 337 | 0 |
| Queue Length 95th (t) |  | 90 | 62 |  | \#197 |  | \#67 | 267 |  | 13 | \#613 | 0 |
| Internal Link Dist (ft) |  | 1952 |  |  | 1444 |  |  | 1655 |  |  | 2425 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  | 860 |  |  | 695 |  |  |
| Base Capacity (vph) |  | 339 | 472 |  | 329 |  | 166 | 855 |  | 356 | 691 | 687 |
| Starvation Cap Reductn |  | 0 | 0 |  | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Spillback Cap Reductn |  | 0 | 0 |  | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 | 0 |  | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Reduced v/c Ratio |  | 0.27 | 0.47 |  | 0.65 |  | 0.55 | 0.52 |  | 0.02 | 0.90 | 0.03 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other
Cycle Length: 90
Actuated Cycle Length: 81.8
Natural Cycle: 95
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.90
Intersection Signal Delay: 33.
Intersection LOS: C
Intersection Capacity Utilization 68.7\% ICU Level of Service C
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Splits and Phases: 2: US 24 \& Judge Orr Rd



| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\uparrow$ |  | ${ }^{1 /}$ | 4 | 「 | ${ }^{7}$ | $\uparrow$ |  | ${ }^{1}$ | $\hat{\beta}$ |  |
| Traffic Vol, veh/h | 102 | 152 | 100 | 40 | 54 | 101 | 25 | 205 | 57 | 77 | 186 | 13 |
| Future Vol, veh/h | 102 | 152 | 100 | 40 | 54 | 101 | 25 | 205 | 57 | 77 | 186 | 13 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.87 | 0.87 | 0.87 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 111 | 165 | 109 | 46 | 62 | 116 | 27 | 223 | 62 | 84 | 202 | 14 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 1 | 1 | 1 | 0 | 1 | 1 | 0 |
| Approach | SE |  |  | NW |  |  | NE |  |  | SW |  |  |
| Opposing Approach | NW |  |  | SE |  |  | SW |  |  | NE |  |  |
| Opposing Lanes | 3 |  |  | 2 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Left | SW |  |  | NE |  |  | SE |  |  | NW |  |  |
| Conflicting Lanes Left | 2 |  |  | 2 |  |  | 2 |  |  | 3 |  |  |
| Conflicting Approach Right | NE |  |  | SW |  |  | NW |  |  | SE |  |  |
| Conflicting Lanes Right | 2 |  |  | 2 |  |  | 3 |  |  | 2 |  |  |
| HCM Control Delay | 17.9 |  |  | 12.5 |  |  | 20.6 |  |  | 16.2 |  |  |
| HCM LOS | C |  |  | B |  |  | C |  |  | C |  |  |


| Lane | NELn1 | NELn2 | NWLn1 | NWLn2 | NWLn3 | SELn1 | SELn2 | SWLn1 | SWLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $100 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Thru, \% | $0 \%$ | $78 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $60 \%$ | $0 \%$ | $93 \%$ |
| Vol Right, \% | $0 \%$ | $22 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $40 \%$ | $0 \%$ | $7 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 25 | 262 | 40 | 54 | 101 | 102 | 252 | 77 | 199 |
| LT Vol | 25 | 0 | 40 | 0 | 0 | 102 | 0 | 77 | 0 |
| Through Vol | 0 | 205 | 0 | 54 | 0 | 0 | 152 | 0 | 186 |
| RT Vol | 0 | 57 | 0 | 0 | 101 | 0 | 100 | 0 | 13 |
| Lane Flow Rate | 27 | 285 | 46 | 62 | 116 | 111 | 274 | 84 | 216 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.063 | 0.604 | 0.111 | 0.141 | 0.241 | 0.253 | 0.565 | 0.194 | 0.468 |
| Departure Headway (Hd) | 8.296 | 7.631 | 8.708 | 8.194 | 7.474 | 8.221 | 7.422 | 8.351 | 7.794 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 430 | 470 | 410 | 436 | 477 | 436 | 485 | 428 | 461 |
| Service Time | 6.075 | 5.409 | 6.5 | 5.985 | 5.264 | 5.999 | 5.2 | 6.135 | 5.578 |
| HCM Lane V/C Ratio | 0.063 | 0.606 | 0.112 | 0.142 | 0.243 | 0.255 | 0.565 | 0.196 | 0.469 |
| HCM Control Delay | 11.6 | 21.5 | 12.6 | 12.3 | 12.6 | 13.8 | 19.5 | 13.2 | 17.3 |
| HCM Lane LOS | B | C | B | B | B | B | C | B | C |
| HCM 95th-tile Q | 0.2 | 3.9 | 0.4 | 0.5 | 0.9 | 1 | 3.4 | 0.7 | 2.4 |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1.6 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  | $\leftrightarrow$ |  |  | \& |  | ${ }^{1}$ | $\uparrow$ |  | ${ }^{1}$ | $\dagger$ |  |
| Traffic Vol, veh/h | 20 | 0 | 20 | 16 | 0 | 7 | 15 | 385 | 8 | 2 | 240 | 10 |
| Future Vol, veh/h | 20 | 0 | 20 | 16 | 0 | 7 | 15 | 385 | 8 | 2 | 240 | 10 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | 50 | - | - | 200 | - | - |
| Veh in Median Storage, \# | \# - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 78 | 92 | 78 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 87 | 87 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 26 | 0 | 26 | 17 | 0 | 8 | 16 | 418 | 9 | 2 | 276 | 11 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1.4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  | \$ |  |  |
| Traffic Vol, veh/h | 9 | 276 | 1 | 1 | 175 | 13 | 1 | 0 | 1 | 29 | 0 | 18 |  |
| Future Vol, veh/h | 9 | 276 | 1 | 1 | 175 | 13 | 1 | 0 | 1 | 29 | 0 | 18 |  |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control F | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |  |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 87 | 87 | 87 | 78 | 78 | 78 | 78 | 78 | 78 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow | 10 | 300 | 1 | 1 | 201 | 15 | 1 | 0 | 1 | 37 | 0 | 23 |  |



|  | $\rightarrow$ | $\rightarrow$ | 7 | $\cdots$ |  |  | b | $\nearrow$ | $>$ | 4 | 4 | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  | $\uparrow$ | 「 |  | $\dagger$ |  | \% | $\uparrow$ |  | \% | $\uparrow$ | F |
| Traffic Volume (vph) | 35 | 35 | 72 | 120 | 114 | 15 | 159 | 565 | 130 | 5 | 420 | 22 |
| Future Volume (vph) | 35 | 35 | 72 | 120 | 114 | 15 | 159 | 565 | 130 | 5 | 420 | 22 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 860 |  | 0 | 695 |  | 0 |
| Storage Lanes | 0 |  | 1 | 0 |  | 0 | 1 |  | 0 | 1 |  | 1 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 300 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  | 0.850 |  | 0.992 |  |  | 0.972 |  |  |  | 0.850 |
| Flt Protected |  | 0.976 |  |  | 0.976 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1818 | 1583 | 0 | 1803 | 0 | 1770 | 1811 | 0 | 1770 | 1863 | 1583 |
| Flt Permitted |  | 0.976 |  |  | 0.804 |  | 0.300 |  |  | 0.189 |  |  |
| Satd. Flow (perm) | 0 | 1818 | 1583 | 0 | 1486 | 0 | 559 | 1811 | 0 | 352 | 1863 | 1583 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 147 |  | 3 |  |  | 15 |  |  |  | 147 |
| Link Speed (mph) |  | 45 |  |  | 45 |  |  | 55 |  |  | 55 |  |
| Link Distance (ft) |  | 2032 |  |  | 1524 |  |  | 1735 |  |  | 2505 |  |
| Travel Time (s) |  | 30.8 |  |  | 23.1 |  |  | 21.5 |  |  | 31.1 |  |
| Peak Hour Factor | 0.83 | 0.83 | 0.83 | 0.87 | 0.87 | 0.87 | 0.93 | 0.93 | 0.93 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 42 | 42 | 87 | 138 | 131 | 17 | 171 | 608 | 140 | 5 | 457 | 24 |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 84 | 87 | 0 | 286 | 0 | 171 | 748 | 0 | 5 | 457 | 24 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(tt) |  | 0 |  |  | 0 |  |  | 12 |  |  | 12 |  |
| Link Offset(ft) |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width(ft) |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 |  | 1 | 2 |  | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru |  | Left | Thru |  | Left | Thru | Right |
| Leading Detector (ft) | 20 | 100 | 20 | 20 | 100 |  | 20 | 100 |  | 20 | 100 | 20 |
| Trailing Detector ( t ) | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Detector 1 Position(ft) | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Detector 1 Size(ft) | 20 | 6 | 20 | 20 | 6 |  | 20 | 6 |  | 20 | 6 | 20 |
| Detector 1 Type | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex |  | Cl+Ex | Cl+Ex |  | Cl+Ex | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(ft) |  | 94 |  |  | 94 |  |  | 94 |  |  | 94 |  |
| Detector 2 Size(ft) |  | 6 |  |  | 6 |  |  | 6 |  |  | 6 |  |
| Detector 2 Type |  | CI+Ex |  |  | CI+Ex |  |  | Cl+Ex |  |  | Cl+Ex |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | Split | NA | Perm | Perm | NA |  | pm+pt | NA |  | Perm | NA | Perm |
| Protected Phases | 4 | 4 |  |  | 8 |  | 5 | 2 |  |  | 6 |  |
| Permitted Phases |  |  | 4 | 8 |  |  | 2 |  |  | 6 |  | 6 |


|  | $\rightarrow$ |  | 2 | $\ldots$ |  |  | * | $\nearrow$ |  | 4 | $\checkmark$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| Detector Phase | 4 | 4 | 4 | 8 | 8 |  | 5 | 2 |  | 6 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 24.0 | 24.0 | 24.0 | 24.0 | 24.0 |  | 9.5 | 24.0 |  | 24.0 | 24.0 | 24.0 |
| Total Split (s) | 18.0 | 18.0 | 18.0 | 30.0 | 30.0 |  | 8.0 | 52.0 |  | 44.0 | 44.0 | 44.0 |
| Total Split (\%) | 18.0\% | 18.0\% | 18.0\% | 30.0\% | 30.0\% |  | 8.0\% | 52.0\% |  | 44.0\% | 44.0\% | 44.0\% |
| Maximum Green (s) | 12.0 | 12.0 | 12.0 | 24.0 | 24.0 |  | 3.5 | 46.0 |  | 38.0 | 38.0 | 38.0 |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 3.5 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 1.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) |  | 0.0 | 0.0 |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) |  | 6.0 | 6.0 |  | 6.0 |  | 4.5 | 6.0 |  | 6.0 | 6.0 | 6.0 |
| Lead/Lag |  |  |  |  |  |  | Lead |  |  | Lag | Lag | Lag |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes |  |  | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | None |  | None | Max |  | Max | Max | Max |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |  | 7.0 |  | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 |  |  | 11.0 |  | 11.0 | 11.0 | 11.0 |
| Pedestrian Calls (\#/hr) | 0 | 0 | 0 | 0 | 0 |  |  | 0 |  | 0 | 0 | 0 |
| Act Effct Green (s) |  | 9.4 | 9.4 |  | 21.3 |  | 48.2 | 46.6 |  | 38.5 | 38.5 | 38.5 |
| Actuated g/C Ratio |  | 0.10 | 0.10 |  | 0.23 |  | 0.52 | 0.50 |  | 0.42 | 0.42 | 0.42 |
| V/c Ratio |  | 0.46 | 0.30 |  | 0.83 |  | 0.51 | 0.81 |  | 0.03 | 0.59 | 0.03 |
| Control Delay |  | 49.4 | 3.7 |  | 56.0 |  | 21.5 | 30.2 |  | 20.4 | 26.9 | 0.1 |
| Queue Delay |  | 0.0 | 0.0 |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Delay |  | 49.4 | 3.7 |  | 56.0 |  | 21.5 | 30.2 |  | 20.4 | 26.9 | 0.1 |
| LOS |  | D | A |  | E |  | C | C |  | C | C | A |
| Approach Delay |  | 26.2 |  |  | 56.0 |  |  | 28.6 |  |  | 25.5 |  |
| Approach LOS |  | C |  |  | E |  |  | C |  |  | C |  |
| Queue Length 50th (ft) |  | 50 | 0 |  | 165 |  | 58 | 396 |  | 2 | 226 | 0 |
| Queue Length 95th (t) |  | 89 | 1 |  | \#286 |  | 103 | \#657 |  | 10 | 345 | 0 |
| Internal Link Dist (ft) |  | 1952 |  |  | 1444 |  |  | 1655 |  |  | 2425 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  | 860 |  |  | 695 |  |  |
| Base Capacity (vph) |  | 239 | 336 |  | 393 |  | 337 | 920 |  | 146 | 776 | 744 |
| Starvation Cap Reductn |  | 0 | 0 |  | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Spillback Cap Reductn |  | 0 | 0 |  | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 | 0 |  | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Reduced v/c Ratio |  | 0.35 | 0.26 |  | 0.73 |  | 0.51 | 0.81 |  | 0.03 | 0.59 | 0.03 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

## Area Type: Other

Cycle Length: 100
Actuated Cycle Length: 92.5
Natural Cycle: 85
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.83
Intersection Signal Delay: $31.7 \quad$ Intersection LOS: C
Intersection Capacity Utilization $77.0 \%$ ICU Level of Service D
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Splits and Phases: 2: US 24 \& Judge Orr Rd


|  |  |
| :--- | ---: | :--- |
| Intersection |  |
| Intersection Delay, s/veh | 14.2 |
| Intersection LOS | B |


| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{*}$ | 4 | 「 | ${ }^{7}$ | $\hat{\beta}$ |  | ${ }^{*}$ | $\hat{\beta}$ |  |
| Traffic Vol, veh/h | 14 | 64 | 90 | 59 | 154 | 48 | 170 | 182 | 71 | 27 | 107 | 13 |
| Future Vol, veh/h | 14 | 64 | 90 | 59 | 154 | 48 | 170 | 182 | 71 | 27 | 107 | 13 |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.83 | 0.83 | 0.83 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 16 | 74 | 103 | 64 | 167 | 52 | 185 | 198 | 77 | 33 | 129 | 16 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 1 | 1 | 1 | 0 | 1 | 1 | 0 |
| Approach | SE |  |  | NW |  |  | NE |  |  | SW |  |  |
| Opposing Approach | NW |  |  | SE |  |  | SW |  |  | NE |  |  |
| Opposing Lanes | 3 |  |  | 2 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Left | SW |  |  | NE |  |  | SE |  |  | NW |  |  |
| Conflicting Lanes Left | 2 |  |  | 2 |  |  | 2 |  |  | 3 |  |  |
| Conflicting Approach Right | NE |  |  | SW |  |  | NW |  |  | SE |  |  |
| Conflicting Lanes Right | 2 |  |  | 2 |  |  | 3 |  |  | 2 |  |  |
| HCM Control Delay | 13.7 |  |  | 12.8 |  |  | 15.6 |  |  | 13.1 |  |  |
| HCM LOS | B |  |  | B |  |  | C |  |  | B |  |  |


| Lane | NELn1 | NELn2 | NWLn1 | NWLn2 | NWLn3 | SELn1 | SELn2 | SWLn1 | SWLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $100 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $0 \%$ | $72 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $42 \%$ | $0 \%$ | $89 \%$ |
| Vol Right, \% | $0 \%$ | $28 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $58 \%$ | $0 \%$ | $11 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 170 | 253 | 59 | 154 | 48 | 14 | 154 | 27 | 120 |
| LT Vol | 170 | 0 | 59 | 0 | 0 | 14 | 0 | 27 | 0 |
| Through Vol | 0 | 182 | 0 | 154 | 0 | 0 | 64 | 0 | 107 |
| RT Vol | 0 | 71 | 0 | 0 | 48 | 0 | 90 | 0 | 13 |
| Lane Flow Rate | 185 | 275 | 64 | 167 | 52 | 16 | 177 | 33 | 145 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.379 | 0.51 | 0.141 | 0.344 | 0.097 | 0.036 | 0.355 | 0.073 | 0.301 |
| Departure Headway (Hd) | 7.377 | 6.672 | 7.898 | 7.388 | 6.674 | 8.152 | 7.22 | 8.07 | 7.484 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 488 | 542 | 454 | 487 | 536 | 439 | 497 | 444 | 480 |
| Service Time | 5.118 | 4.413 | 5.645 | 5.134 | 4.419 | 5.903 | 4.97 | 5.821 | 5.235 |
| HCM Lane V/C Ratio | 0.379 | 0.507 | 0.141 | 0.343 | 0.097 | 0.036 | 0.356 | 0.074 | 0.302 |
| HCM Control Delay | 14.6 | 16.2 | 11.9 | 14 | 10.1 | 11.2 | 13.9 | 11.5 | 13.4 |
| HCM Lane LOS | B | C | $B$ | $B$ | $B$ | $B$ | $B$ | B | B |
| HCM 95th-tile Q | 1.7 | 2.9 | 0.5 | 1.5 | 0.3 | 0.1 | 1.6 | 0.2 | 1.3 |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1.6 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  | \& |  |  | $\leqslant$ |  | \% | $\hat{\dagger}$ |  | ${ }^{1 /}$ | $\uparrow$ |  |
| Traffic Vol, veh/h | 10 | 0 | 10 | 12 | 0 | 7 | 25 | 202 | 17 | 3 | 125 | 20 |
| Future Vol, veh/h | 10 | 0 | 10 | 12 | 0 | 7 | 25 | 202 | 17 | 3 | 125 | 20 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control S | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | 50 | - | - | 200 | - | - |
| Veh in Median Storage, \# | \# - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 78 | 92 | 78 | 78 | 78 | 78 | 87 | 87 | 87 | 83 | 83 | 83 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 13 | 0 | 13 | 15 | 0 | 9 | 29 | 232 | 20 | 4 | 151 | 24 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1.4 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \& |  |  | * |  |  | \$ |  |  | 4 |  |
| Traffic Vol, veh/h | 20 | 141 | 1 | 1 | 247 | 29 | 1 | 0 | 1 | 19 | 0 | 15 |
| Future Vol, veh/h | 20 | 141 | 1 | 1 | 247 | 29 | 1 | 0 | 1 | 19 | 0 | 15 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Fros | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 87 | 87 | 87 | 92 | 92 | 92 | 78 | 78 | 78 | 78 | 78 | 78 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 23 | 162 | 1 | 1 | 268 | 32 | 1 | 0 | 1 | 24 | 0 | 19 |



|  | $\rightarrow$ | $\rightarrow$ | 2 | $\ldots$ |  | $\cdots$ | ＊ | $\varnothing$ | $p$ | 4 | $\backslash$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations | ${ }^{4}$ | 4 | \％ | \％${ }^{1 / 1}$ | 个个 | ${ }^{7}$ | \％${ }^{1 / 1}$ | 个个 | ${ }^{7}$ | \％ | 个4 | F |
| Traffic Volume（vph） | 65 | 150 | 275 | 265 | 125 | 50 | 230 | 675 | 200 | 100 | 1200 | 100 |
| Future Volume（vph） | 65 | 150 | 275 | 265 | 125 | 50 | 230 | 675 | 200 | 100 | 1200 | 100 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（ft） | 235 |  | 0 | 290 |  | 0 | 860 |  | 0 | 695 |  | 0 |
| Storage Lanes | 1 |  | 1 | 2 |  | 1 | 2 |  | 1 | 1 |  | 1 |
| Taper Length（ft） | 200 |  |  | 200 |  |  | 300 |  |  | 25 |  |  |
| Lane Util．Factor | 1.00 | 1.00 | 1.00 | 0.97 | 0.95 | 1.00 | 0.97 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| FIt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1770 | 1863 | 1583 | 3433 | 3539 | 1583 | 3433 | 3539 | 1583 | 1770 | 3539 | 1583 |
| Flt Permitted | 0.666 |  |  | 0.950 |  |  | 0.950 |  |  | 0.355 |  |  |
| Satd．Flow（perm） | 1241 | 1863 | 1583 | 3433 | 3539 | 1583 | 3433 | 3539 | 1583 | 661 | 3539 | 1583 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 248 |  |  | 149 |  |  | 211 |  |  | 149 |
| Link Speed（mph） |  | 45 |  |  | 45 |  |  | 55 |  |  | 55 |  |
| Link Distance（ft） |  | 2032 |  |  | 1524 |  |  | 1735 |  |  | 2505 |  |
| Travel Time（s） |  | 30.8 |  |  | 23.1 |  |  | 21.5 |  |  | 31.1 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj．Flow（vph） | 71 | 163 | 299 | 288 | 136 | 54 | 242 | 711 | 211 | 105 | 1263 | 105 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 71 | 163 | 299 | 288 | 136 | 54 | 242 | 711 | 211 | 105 | 1263 | 105 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width（ft） |  | 24 |  |  | 24 |  |  | 24 |  |  | 24 |  |
| Link Offset（ft） |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width（ft） |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed（mph） | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector（ft） | 20 | 100 | 20 | 20 | 100 | 20 | 20 | 100 | 20 | 20 | 100 | 20 |
| Trailing Detector（ t ） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Detector 1 Position（ft） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Detector 1 Size（ft） | 20 | 6 | 20 | 20 | 6 | 20 | 20 | 6 | 20 | 20 | 6 | 20 |
| Detector 1 Type | Cl＋Ex | Cl＋Ex | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | Cl＋Ex | $\mathrm{Cl}+\mathrm{Ex}$ | Cl＋Ex | Cl＋Ex | $\mathrm{Cl}+\mathrm{Ex}$ | Cl＋Ex | $\mathrm{Cl}+\mathrm{Ex}$ |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position（ft） |  | 94 |  |  | 94 |  |  | 94 |  |  | 94 |  |
| Detector 2 Size（ft） |  | 6 |  |  | 6 |  |  | 6 |  |  | 6 |  |
| Detector 2 Type |  | $\mathrm{Cl}+\mathrm{Ex}$ |  |  | Cl＋Ex |  |  | Cl＋Ex |  |  | Cl＋Ex |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend（s） |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | pm＋pt | NA | Perm | Prot | NA | Perm | Prot | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  | 4 |  |  | 8 |  |  | 2 | 6 |  | 6 |


| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 2 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 9.5 | 22.5 | 22.5 | 9.5 | 22.5 | 22.5 | 9.5 | 22.5 | 22.5 | 9.5 | 22.5 | 22.5 |
| Total Split (s) | 17.0 | 24.0 | 24.0 | 19.0 | 26.0 | 26.0 | 23.0 | 56.0 | 56.0 | 11.0 | 44.0 | 44.0 |
| Total Split (\%) | 15.5\% | 21.8\% | 21.8\% | 17.3\% | 23.6\% | 23.6\% | 20.9\% | 50.9\% | 50.9\% | 10.0\% | 40.0\% | 40.0\% |
| Maximum Green (s) | 12.5 | 19.5 | 19.5 | 14.5 | 21.5 | 21.5 | 18.5 | 51.5 | 51.5 | 6.5 | 39.5 | 39.5 |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | None | None | None | Max | Max | None | Max | Max |
| Walk Time (s) |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk (s) |  | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 11.0 |
| Pedestrian Calls (\#/hr) |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |
| Act Effct Green (s) | 22.8 | 14.3 | 14.3 | 12.9 | 21.1 | 21.1 | 12.6 | 51.7 | 51.7 | 51.9 | 45.5 | 45.5 |
| Actuated g/C Ratio | 0.22 | 0.14 | 0.14 | 0.12 | 0.20 | 0.20 | 0.12 | 0.50 | 0.50 | 0.50 | 0.44 | 0.44 |
| v/c Ratio | 0.22 | 0.63 | 0.69 | 0.67 | 0.19 | 0.12 | 0.58 | 0.40 | 0.24 | 0.26 | 0.81 | 0.13 |
| Control Delay | 27.3 | 53.6 | 18.1 | 52.1 | 36.1 | 0.6 | 49.1 | 17.8 | 3.0 | 12.3 | 32.0 | 1.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 27.3 | 53.6 | 18.1 | 52.1 | 36.1 | 0.6 | 49.1 | 17.8 | 3.0 | 12.3 | 32.0 | 1.7 |
| LOS | C | D | B | D | D | A | D | B | A | B | C | A |
| Approach Delay |  | 30.2 |  |  | 41.7 |  |  | 21.7 |  |  | 28.5 |  |
| Approach LOS |  | C |  |  | D |  |  | C |  |  | C |  |
| Queue Length 50th (ft) | 34 | 104 | 31 | 94 | 40 | 0 | 79 | 152 | 0 | 28 | 380 | 0 |
| Queue Length 95th (ft) | 67 | 173 | 120 | 146 | 70 | 0 | 121 | 220 | 40 | 58 | \#597 | 14 |
| Internal Link Dist (ft) |  | 1952 |  |  | 1444 |  |  | 1655 |  |  | 2425 |  |
| Turn Bay Length (ft) | 235 |  |  | 290 |  |  | 860 |  |  | 695 |  |  |
| Base Capacity (vph) | 386 | 352 | 500 | 482 | 765 | 459 | 616 | 1767 | 896 | 402 | 1557 | 779 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.18 | 0.46 | 0.60 | 0.60 | 0.18 | 0.12 | 0.39 | 0.40 | 0.24 | 0.26 | 0.81 | 0.13 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other
Cycle Length: 110
Actuated Cycle Length: 103.4
Natural Cycle: 90
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.81
Intersection Signal Delay: 28.3
Intersection LOS: C
Intersection Capacity Utilization 70.2\% ICU Level of Service C
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Splits and Phases: 2: US 24 \& Judge Orr Rd


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh | 8.2 |  |  |  |
| Intersection LOS | A |  | NW | NE |
| Approach | SE | 2 | 2 | 2 |
| Entry Lanes | 2 | 1 | 1 | 1 |
| Conflicting Circle Lanes | 1 | 326 | 489 | 592 |
| Adj Approach Flow, veh/h | 522 | 332 | 499 | 603 |
| Demand Flow Rate, veh/h | 532 | 531 | 587 | 221 |
| Vehicles Circulating, veh/h | 636 | 555 | 581 | 042 |
| Vehicles Exiting, veh/h | 188 | 0 | 0 | 0 |
| Ped Vol Crossing Leg, \#h | 0 | 1.000 | 1.000 | 1.000 |
| Ped Cap Adj | 1.000 | 6.1 | 5.8 |  |
| Approach Delay, slveh | 9.5 | A | B | A |


| Lane | Left | Right | Left | Right | Left | Right | Left | Right |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Designated Moves | LT | R | LT | R | L | TR | L | TR |
| Assumed Moves | LT | R | LT | R | L | TR | L | TR |
| RT Channelized |  |  |  |  |  |  |  |  |
| Lane Util | 0.688 | 0.312 | 0.500 | 0.500 | 0.110 | 0.890 | 0.367 | 0.633 |
| Follow-Up Headway, s | 2.535 | 2.535 | 2.535 | 2.535 | 2.535 | 2.535 | 2.535 | 2.535 |
| Critical Headway, s | 4.544 | 4.544 | 4.544 | 4.544 | 4.544 | 4.544 | 4.544 | 4.544 |
| Entry Flow, veh/h | 366 | 166 | 166 | 166 | 55 | 444 | 221 | 382 |
| Cap Entry Lane, veh/h | 796 | 796 | 876 | 876 | 832 | 832 | 1161 | 1161 |
| Entry HV Adj Factor | 0.981 | 0.982 | 0.981 | 0.982 | 0.982 | 0.980 | 0.982 | 0.982 |
| Flow Entry, veh/h | 359 | 163 | 163 | 163 | 54 | 435 | 217 | 375 |
| Cap Entry, veh/h | 781 | 782 | 859 | 860 | 817 | 815 | 1140 | 1140 |
| VIC Ratio | 0.460 | 0.209 | 0.190 | 0.190 | 0.066 | 0.533 | 0.190 | 0.329 |
| Control Delay, s/veh | 10.8 | 6.9 | 6.1 | 6.1 | 5.0 | 12.0 | 4.8 | 6.3 |
| LOS | B | A | A | A | A | B | A | A |
| 95th \%tile Queue, veh | 2 | 1 | 1 | 1 | 0 | 3 | 1 | 1 |



| Major/Minor | Minor2 | Major1 |  | Major2 |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Conflicting Flow All | 1255 | 609 | 614 | 0 | - |
| $\quad$ Stage 1 | 609 | - | - | - | - |

HCMLOS B

| Minor Lane/Major Mvmt | NEL | NET SELn1 | SWT | SWR |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 965 | -422 | - | - |
| HCM Lane V/C Ratio | 0.017 | -0.091 | - | - |
| HCM Control Delay (s) | 8.8 | -14.4 | - | - |
| HCM Lane LOS | A | - | B | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | 0.3 | - |
| (s) | - |  |  |  |



| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 544 | 0 | 701 | 223 |
| Stage 1 | - | - | - | - | 446 | - |
| Stage 2 | - | - | - | - | 255 | - |
| Critical Hdwy | - | - | 4.14 | - | 6.84 | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.84 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.84 | - |
| Follow-up Hdwy | - | - | 2.22 | - | 3.52 | 3.32 |
| Pot Cap-1 Maneuver | - | - | 1021 | - | 453 | 780 |
| Stage 1 | - | - | - | - | 612 | - |
| Stage 2 | - | - | - | - | 913 | - |
| Platoon blocked, \% | - | - |  | - | 1 |  |
| Mov Cap-1 Maneuver | - | - | 1021 | - | 429 | 780 |
| Mov Cap-2 Maneuver | - | - | - | - | 429 | - |
| Stage 1 | - | - | - | - | 612 | - |
| Stage 2 | - | - | - | - | 864 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 1.4 |  | 12.4 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) |  | 684 | - | - | 1021 | - |
| HCM Lane V/C Ratio |  | 0.294 | - | - | 0.053 | - |
| HCM Control Delay (s) |  | 12.4 | - | - | 8.7 | - |
| HCM Lane LOS |  | B | - | - | A | - |
| HCM 95th \%tile Q(veh) |  | 1.2 | - | - | 0.2 | - |


|  | $\rightarrow$ | $\rightarrow$ | 2 | $\cdots$ |  | $\checkmark$ | b | $\nearrow$ | $\rightarrow$ | 4 | $\backslash$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations | \％ | 中4 | \％ | \％${ }^{\text {\％}}$ | 个4 | F | \％${ }^{\text {\％}}$ | 个4 | F | 7\％ | 性 | F |
| Traffic Volume（vph） | 190 | 200 | 340 | 435 | 200 | 165 | 400 | 1234 | 430 | 150 | 790 | 155 |
| Future Volume（vph） | 190 | 200 | 340 | 435 | 200 | 165 | 400 | 1234 | 430 | 150 | 790 | 155 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（ft） | 235 |  | 235 | 235 |  | 235 | 860 |  | 290 | 695 |  | 290 |
| Storage Lanes | 1 |  | 1 | 2 |  | 1 | 2 |  | 1 | 2 |  | 1 |
| Taper Length（ft） | 200 |  |  | 200 |  |  | 300 |  |  | 300 |  |  |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 0.97 | 0.95 | 1.00 | 0.97 | 0.95 | 1.00 | 0.97 | 0.95 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1770 | 3539 | 1583 | 3433 | 3539 | 1583 | 3433 | 3539 | 1583 | 3433 | 3539 | 1583 |
| Flt Permitted | 0.617 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（perm） | 1149 | 3539 | 1583 | 3433 | 3539 | 1583 | 3433 | 3539 | 1583 | 3433 | 3539 | 1583 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 203 |  |  | 177 |  |  | 453 |  |  | 164 |
| Link Speed（mph） |  | 45 |  |  | 45 |  |  | 55 |  |  | 55 |  |
| Link Distance（ft） |  | 2032 |  |  | 1524 |  |  | 1735 |  |  | 2505 |  |
| Travel Time（s） |  | 30.8 |  |  | 23.1 |  |  | 21.5 |  |  | 31.1 |  |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj．Flow（vph） | 204 | 215 | 366 | 468 | 215 | 177 | 421 | 1299 | 453 | 158 | 832 | 163 |
| Shared Lane Trafic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 204 | 215 | 366 | 468 | 215 | 177 | 421 | 1299 | 453 | 158 | 832 | 163 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width（ft） |  | 24 |  |  | 24 |  |  | 24 |  |  | 24 |  |
| Link Offset（ft） |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width（ft） |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed（mph） | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector（tt） | 20 | 100 | 20 | 20 | 100 | 20 | 20 | 100 | 20 | 20 | 100 | 20 |
| Trailing Detector（ft） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Detector 1 Position（ft） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Detector 1 Size（ft） | 20 | 6 | 20 | 20 | 6 | 20 | 20 | 6 | 20 | 20 | 6 | 20 |
| Detector 1 Type | Cl＋Ex | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | Cl＋Ex | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position（ft） |  | 94 |  |  | 94 |  |  | 94 |  |  | 94 |  |
| Detector 2 Size（ft） |  | 6 |  |  | 6 |  |  | 6 |  |  | 6 |  |
| Detector 2 Type |  | Cl＋Ex |  |  | Cl＋Ex |  |  | Cl＋Ex |  |  | Cl＋Ex |  |
| Detector 2 Channel $0^{\text {a }}$ |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend（s） |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | pm＋pt | NA | Perm | Prot | NA | Perm | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |


| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 2 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 9.5 | 24.0 | 24.0 | 9.5 | 24.0 | 24.0 | 9.5 | 24.0 | 24.0 | 9.5 | 24.0 | 24.0 |
| Total Split (s) | 19.0 | 24.0 | 24.0 | 20.0 | 25.0 | 25.0 | 19.0 | 56.0 | 56.0 | 10.0 | 47.0 | 47.0 |
| Total Split (\%) | 17.3\% | 21.8\% | 21.8\% | 18.2\% | 22.7\% | 22.7\% | 17.3\% | 50.9\% | 50.9\% | 9.1\% | 42.7\% | 42.7\% |
| Maximum Green (s) | 14.5 | 18.0 | 18.0 | 15.5 | 19.0 | 19.0 | 14.5 | 50.0 | 50.0 | 5.5 | 41.0 | 41.0 |
| Yellow Time (s) | 3.5 | 4.0 | 4.0 | 3.5 | 4.0 | 4.0 | 3.5 | 4.0 | 4.0 | 3.5 | 4.0 | 4.0 |
| All-Red Time (s) | 1.0 | 2.0 | 2.0 | 1.0 | 2.0 | 2.0 | 1.0 | 2.0 | 2.0 | 1.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 6.0 | 6.0 | 4.5 | 6.0 | 6.0 | 4.5 | 6.0 | 6.0 | 4.5 | 6.0 | 6.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | None | None | None | Max | Max | None | Max | Max |
| Walk Time (s) |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk (s) |  | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 11.0 |
| Pedestrian Calls (\#/hr) |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |
| Act Effct Green (s) | 30.2 | 15.6 | 15.6 | 15.5 | 18.0 | 18.0 | 14.5 | 50.1 | 50.1 | 5.5 | 41.1 | 41.1 |
| Actuated g/C Ratio | 0.28 | 0.14 | 0.14 | 0.14 | 0.17 | 0.17 | 0.13 | 0.47 | 0.47 | 0.05 | 0.38 | 0.38 |
| v/c Ratio | 0.51 | 0.42 | 0.91 | 0.95 | 0.36 | 0.43 | 0.91 | 0.79 | 0.46 | 0.90 | 0.62 | 0.23 |
| Control Delay | 31.3 | 44.3 | 47.8 | 76.1 | 41.9 | 9.5 | 71.7 | 29.2 | 3.4 | 99.0 | 29.8 | 4.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 31.3 | 44.3 | 47.8 | 76.1 | 41.9 | 9.5 | 71.7 | 29.2 | 3.4 | 99.0 | 29.8 | 4.4 |
| LOS | C | D | D | E | D | A | E | C | A | F | C | A |
| Approach Delay |  | 42.5 |  |  | 53.8 |  |  | 32.0 |  |  | 35.7 |  |
| Approach LOS |  | D |  |  | D |  |  | C |  |  | D |  |
| Queue Length 50th (ft) | 103 | 72 | 116 | 171 | 71 | 0 | 153 | 405 | 0 | 58 | 250 | 0 |
| Queue Length 95th (ft) | 165 | 110 | \#279 | \#275 | 108 | 60 | \#247 | 498 | 55 | \#123 | 317 | 42 |
| Internal Link Dist (ft) |  | 1952 |  |  | 1444 |  |  | 1655 |  |  | 2425 |  |
| Turn Bay Length (ft) | 235 |  | 235 | 235 |  | 235 | 860 |  | 290 | 695 |  | 290 |
| Base Capacity (vph) | 421 | 592 | 433 | 494 | 625 | 425 | 462 | 1644 | 978 | 175 | 1349 | 704 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.48 | 0.36 | 0.85 | 0.95 | 0.34 | 0.42 | 0.91 | 0.79 | 0.46 | 0.90 | 0.62 | 0.23 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other
Cycle Length: 110
Actuated Cycle Length: 107.7
Natural Cycle: 90
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.95
Intersection Signal Delay: $38.3 \quad$ Intersection LOS: D
Intersection Capacity Utilization 73.8\% ICU Level of Service D
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Splits and Phases: 2: US 24 \& Judge Orr Rd


| Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 7.1 |  |  |  |
| Intersection LOS | A |  |  |  |
| Approach | SE | NW | NE | SW |
| Entry Lanes | 2 | 2 | 2 | 2 |
| Conflicting Circle Lanes | 1 | 1 | 1 | 1 |
| Adj Approach Flow, veh/h | 288 | 543 | 672 | 365 |
| Demand Flow Rate, veh/h | 294 | 553 | 685 | 372 |
| Vehicles Circulating, veh/h | 472 | 564 | 266 | 551 |
| Vehicles Exiting, veh/h | 451 | 387 | 500 | 566 |
| Ped Vol Crossing Leg, \#/h | 0 | 0 | 0 | 0 |
| Ped Cap Adj | 1.000 | 1.000 | 1.000 | 1.000 |
| Approach Delay, s/veh | 5.5 | 8.3 | 6.9 | 7.0 |
| Approach LOS | A | A | A | A |


| Lane | Left | Right | Left | Right | Left | Right | Left | Right |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Designated Moves | LT | R | LT | R | L | TR | L | TR |
| Assumed Moves | LT | R | LT | R | L | TR | L | TR |
| RT Channelized |  |  |  |  |  |  |  |  |
| Lane Util | 0.527 | 0.473 | 0.600 | 0.400 | 0.320 | 0.680 | 0.298 | 0.702 |
| Follow-Up Headway, s | 2.535 | 2.535 | 2.535 | 2.535 | 2.535 | 2.535 | 2.535 | 2.535 |
| Critical Headway, s | 4.544 | 4.544 | 4.544 | 4.544 | 4.544 | 4.544 | 4.544 | 4.544 |
| Entry Flow, veh/h | 155 | 139 | 332 | 221 | 219 | 466 | 111 | 261 |
| Cap Entry Lane, veh/h | 924 | 924 | 850 | 850 | 1115 | 1115 | 860 | 860 |
| Entry HV Adj Factor | 0.982 | 0.978 | 0.981 | 0.982 | 0.982 | 0.980 | 0.982 | 0.981 |
| Flow Entry, veh/h | 152 | 136 | 326 | 217 | 215 | 457 | 109 | 256 |
| Cap Entry, veh/h | 908 | 904 | 834 | 835 | 1094 | 1092 | 845 | 844 |
| V/C Ratio | 0.168 | 0.150 | 0.391 | 0.260 | 0.196 | 0.418 | 0.129 | 0.303 |
| Control Delay, s/veh | 5.6 | 5.4 | 9.0 | 7.1 | 5.1 | 7.7 | 5.5 | 7.6 |
| LOS | A | A | A | A | A | A | A | A |
| 95th \%tile Queue, veh | 1 | 1 | 2 | 1 | 1 | 2 | 0 | 1 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.6 |  |  |  |  |  |
| Movement | SEL | SER | NEL | NET | SWT | SWR |
| Lane Configurations | Y |  | 10 | 4 | b |  |
| Traffic Vol, veh/h | 10 | 10 | 25 | 490 | 325 | 20 |
| Future Vol, veh/h | 10 | 10 | 25 | 490 | 325 | 20 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 25 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 78 | 78 | 93 | 93 | 93 | 93 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 13 | 13 | 27 | 527 | 349 | 22 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.7 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 个4 | $\mathbf{7}$ |  | 4. | Mr |  |
| Traffic Vol, veh/h | 230 | 120 | 150 | 440 | 60 | 95 |
| Future Vol, veh/h | 230 | 120 | 150 | 440 | 60 | 95 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 235 | 385 | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 93 | 93 | 87 | 87 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 250 | 130 | 161 | 473 | 69 | 109 |


| Major/Minor M | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 380 | 0 | 809 | 125 |
| Stage 1 | - | - | - | - | 250 | - |
| Stage 2 | - | - | - | - | 559 | - |
| Critical Hdwy | - | - | 4.14 | - | 6.84 | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.84 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.84 | - |
| Follow-up Hdwy | - | - | 2.22 | - | 3.52 | 3.32 |
| Pot Cap-1 Maneuver | - | - | 1175 | - | 318 | 902 |
| Stage 1 | - | - | - | - | 768 | - |
| Stage 2 | - | - | - | - | 536 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1175 | - | 274 | 902 |
| Mov Cap-2 Maneuver | - | - | - | - | 274 | - |
| Stage 1 | - | - | - | - | 768 | - |
| Stage 2 | - | - | - | - | 463 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 2.2 |  | 16.9 |  |
| HCM LOS |  |  |  |  | C |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) |  | 478 | - | - | 1175 | - |
| HCM Lane V/C Ratio |  | 0.373 | - | - | 0.137 | - |
| HCM Control Delay (s) |  | 16.9 | - | - | 8.6 | - |
| HCM Lane LOS |  | C | - | - | A | - |
| HCM 95th \%tile Q(veh) |  | 1.7 | - | - | 0.5 | - |


|  | $\rightarrow$ | $\rightarrow$ | 2 | $\cdots$ |  | $\checkmark$ | * | $\nearrow$ | $\rightarrow$ | 4 | $\lambda$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ | \% | \% ${ }^{\text {\% }}$ | 个4 | ${ }^{7}$ | 7\% | ¢ $\uparrow$ | ${ }^{*}$ | \% | ¢ 4 | F |
| Trafic Volume (vph) | 67 | 154 | 298 | 265 | 134 | 50 | 239 | 675 | 200 | 100 | 1200 | 102 |
| Future Volume (vph) | 67 | 154 | 298 | 265 | 134 | 50 | 239 | 675 | 200 | 100 | 1200 | 102 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 290 |  | 0 | 290 |  | 290 | 860 |  | 290 | 695 |  | 290 |
| Storage Lanes | 1 |  | 1 | 2 |  | 1 | 2 |  | 1 | 1 |  | 1 |
| Taper Length (ft) | 240 |  |  | 240 |  |  | 300 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.97 | 0.95 | 1.00 | 0.97 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 3433 | 3539 | 1583 | 3433 | 3539 | 1583 | 1770 | 3539 | 1583 |
| Flt Permitted | 0.659 |  |  | 0.950 |  |  | 0.950 |  |  | 0.354 |  |  |
| Satd. Flow (perm) | 1228 | 1863 | 1583 | 3433 | 3539 | 1583 | 3433 | 3539 | 1583 | 659 | 3539 | 1583 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 246 |  |  | 149 |  |  | 211 |  |  | 149 |
| Link Speed (mph) |  | 45 |  |  | 45 |  |  | 55 |  |  | 55 |  |
| Link Distance (ft) |  | 2032 |  |  | 1524 |  |  | 1735 |  |  | 2505 |  |
| Travel Time (s) |  | 30.8 |  |  | 23.1 |  |  | 21.5 |  |  | 31.1 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 73 | 167 | 324 | 288 | 146 | 54 | 252 | 711 | 211 | 105 | 1263 | 107 |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 73 | 167 | 324 | 288 | 146 | 54 | 252 | 711 | 211 | 105 | 1263 | 107 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(ft) |  | 24 |  |  | 24 |  |  | 24 |  |  | 24 |  |
| Link Offset(ft) |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width(ft) |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector (ft) | 20 | 100 | 20 | 20 | 100 | 20 | 20 | 100 | 20 | 20 | 100 | 20 |
| Trailing Detector ( t ) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Detector 1 Position(f) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Detector 1 Size(ft) | 20 | 6 | 20 | 20 | 6 | 20 | 20 | 6 | 20 | 20 | 6 | 20 |
| Detector 1 Type | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(ft) |  | 94 |  |  | 94 |  |  | 94 |  |  | 94 |  |
| Detector 2 Size(ft) |  | 6 |  |  | 6 |  |  | 6 |  |  | 6 |  |
| Detector 2 Type |  | Cl+Ex |  |  | Cl+Ex |  |  | Cl+Ex |  |  | Cl+Ex |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | pm+pt | NA | Perm | Prot | NA | Perm | Prot | NA | Perm | $\mathrm{pm}+\mathrm{pt}$ | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  | 4 |  |  | 8 |  |  | 2 | 6 |  | 6 |


|  | $\rightarrow$ | $\rightarrow$ | 7 |  |  | $\checkmark$ | * |  | $\rho$ | 4 |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 2 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 9.5 | 22.5 | 22.5 | 9.5 | 22.5 | 22.5 | 9.5 | 22.5 | 22.5 | 9.5 | 22.5 | 22.5 |
| Total Split (s) | 17.0 | 23.6 | 23.6 | 19.0 | 25.6 | 25.6 | 23.0 | 56.0 | 56.0 | 11.4 | 44.4 | 44.4 |
| Total Split (\%) | 15.5\% | 21.5\% | 21.5\% | 17.3\% | 23.3\% | 23.3\% | 20.9\% | 50.9\% | 50.9\% | 10.4\% | 40.4\% | 40.4\% |
| Maximum Green (s) | 12.5 | 19.1 | 19.1 | 14.5 | 21.1 | 21.1 | 18.5 | 51.5 | 51.5 | 6.9 | 39.9 | 39.9 |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | None | None | None | Max | Max | None | Max | Max |
| Walk Time (s) |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk (s) |  | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 11.0 |
| Pedestrian Calls (\#hr) |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |
| Act Effct Green (s) | 23.0 | 14.4 | 14.4 | 12.9 | 21.1 | 21.1 | 12.9 | 51.7 | 51.7 | 52.2 | 45.5 | 45.5 |
| Actuated g/C Ratio | 0.22 | 0.14 | 0.14 | 0.12 | 0.20 | 0.20 | 0.12 | 0.50 | 0.50 | 0.50 | 0.44 | 0.44 |
| $\mathrm{v} / \mathrm{c}$ Ratio | 0.23 | 0.64 | 0.75 | 0.67 | 0.20 | 0.12 | 0.59 | 0.40 | 0.24 | 0.26 | 0.81 | 0.14 |
| Control Delay | 27.6 | 54.4 | 23.2 | 52.5 | 36.4 | 0.6 | 49.3 | 18.0 | 3.0 | 12.2 | 32.4 | 1.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 27.6 | 54.4 | 23.2 | 52.5 | 36.4 | 0.6 | 49.3 | 18.0 | 3.0 | 12.2 | 32.4 | 1.8 |
| LOS | C | D | C | D | D | A | D | B | A | B | C | A |
| Approach Delay |  | 33.0 |  |  | 41.9 |  |  | 22.0 |  |  | 28.8 |  |
| Approach LOS |  | C |  |  | D |  |  | C |  |  | C |  |
| Queue Length 50th (ft) | 35 | 108 | 48 | 95 | 44 | 0 | 83 | 154 | 0 | 28 | 384 | 0 |
| Queue Length 95th (ft) | 68 | 178 | 148 | 146 | 74 | 0 | 125 | 220 | 40 | 58 | \#597 | 16 |
| Internal Link Dist (ft) |  | 1952 |  |  | 1444 |  |  | 1655 |  |  | 2425 |  |
| Turn Bay Length ( t ) | 290 |  |  | 290 |  | 290 | 860 |  | 290 | 695 |  | 290 |
| Base Capacity (vph) | 384 | 343 | 492 | 480 | 756 | 455 | 613 | 1761 | 893 | 406 | 1550 | 777 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.19 | 0.49 | 0.66 | 0.60 | 0.19 | 0.12 | 0.41 | 0.40 | 0.24 | 0.26 | 0.81 | 0.14 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other
Cycle Length: 110
Actuated Cycle Length: 103.8
Natural Cycle: 90
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.81
Intersection Signal Delay: 29.0
Intersection LOS: C
Intersection Capacity Utilization 70.7\% ICU Level of Service C
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Splits and Phases: 2: US 24 \& Judge Orr Rd


| Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 8.1 |  |  |  |
| Intersection LOS | A |  |  |  |
| Approach | SE | NW | NE | SW |
| Entry Lanes | 2 | 2 | 2 | 2 |
| Conflicting Circle Lanes | 2 | 2 | 2 | 2 |
| Adj Approach Flow, veh/h | 528 | 347 | 500 | 602 |
| Demand Flow Rate, veh/h | 538 | 353 | 510 | 614 |
| Vehicles Circulating, veh/h | 656 | 539 | 593 | 241 |
| Vehicles Exiting, veh/h | 199 | 564 | 601 | 651 |
| Ped Vol Crossing Leg, \#/h | 0 | 0 | 0 | 0 |
| Ped Cap Adj | 1.000 | 1.000 | 1.000 | 1.000 |
| Approach Delay, s/veh | 8.9 | 6.4 | 11.0 | 6.1 |
| Approach LOS | A | A | B | A |


| Lane | Left | Right | Left | Right | Left | Right | Left | Right |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Designated Moves | LT | TR | LT | TR | L | TR | L | TR |
| Assumed Moves | LT | TR | LT | TR | L | TR | L | TR |
| RT Channelized | 0.470 | 0.530 | 0.470 | 0.530 | 0.108 | 0.892 | 0.360 | 0.640 |
| Lane Util | .667 | 2.535 | 2.667 | 2.535 | 2.667 | 2.535 | 2.667 | 2.535 |
| Follow-Up Headway, s | 2.645 | 4.328 | 4.645 | 4.328 | 4.645 | 4.328 | 4.645 | 4.328 |
| Critical Headway, s | 4.253 | 166 | 187 | 55 | 455 | 221 | 393 |  |
| Entry Flow, veh/h | 253 | 285 | 822 | 898 | 782 | 858 | 1081 | 1157 |
| Cap Entry Lane, veh/h | 738 | 813 | 0.982 | 0.983 | 0.982 | 0.980 | 0.982 | 0.979 |
| Entry HV Adj Factor | 0.981 | 0.982 | 0.982 |  |  |  |  |  |
| Flow Entry, veh/h | 248 | 280 | 163 | 184 | 54 | 446 | 217 | 385 |
| Cap Entry, veh/h | 724 | 798 | 807 | 883 | 768 | 841 | 1062 | 1133 |
| V/C Ratio | 0.343 | 0.351 | 0.202 | 0.208 | 0.070 | 0.530 | 0.204 | 0.340 |
| Control Delay, s/veh | 9.3 | 8.7 | 6.6 | 6.2 | 5.4 | 11.7 | 5.3 | 6.5 |
| LOS | A | A | A | A | A | B | A | A |
| 95th \%otile Queue, veh | 2 | 2 | 1 | 1 | 0 | 3 | 1 | 2 |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1.4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |  |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  | 7 | $\uparrow$ | F | \% | F |  |  |
| Traffic Vol, veh/h | 10 | - | 20 | 16 | 0 | 9 | 15 | 565 | 8 | 3 | 525 | 10 |  |
| Future Vol, veh/h | 10 | 0 | 20 | 16 | 0 | 9 | 15 | 565 | 8 | 3 | 525 | 10 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control Stor | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |  |
| Storage Length | - | - | - | - | - | - | 50 | - | 155 | 200 | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 78 | 78 | 78 | 78 | 78 | 78 | 93 | 93 | 93 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow | 13 | 0 | 26 | 21 | 0 | 12 | 16 | 608 | 9 | 3 | 571 | 11 |  |


| Major/Minor | Minor2 | Minor1 |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 1234 | 1232 | 577 | 1236 | 1228 | 608 | 582 | 0 | 0 | 617 | 0 |
|  |  |  |  |  |  |  |  |  |  |  |  |
| Stage 1 | 583 | 583 | - | 640 | 640 | - | - | - | - | - | - |




| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | $\uparrow$ | 「 | \％${ }^{1 / 1}$ | 个4 | 「 | \％${ }^{*}$ | ¢4 | F | ${ }^{7}$ | 个个 | F |
| Traffic Volume（vph） | 192 | 203 | 357 | 435 | 220 | 165 | 420 | 1234 | 430 | 150 | 790 | 159 |
| Future Volume（vph） | 192 | 203 | 357 | 435 | 220 | 165 | 420 | 1234 | 430 | 150 | 790 | 159 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（ft） | 235 |  | 0 | 235 |  | 235 | 860 |  | 290 | 695 |  | 290 |
| Storage Lanes | 1 |  | 1 | 2 |  | 1 | 2 |  | 1 | 1 |  | 1 |
| Taper Length（ft） | 200 |  |  | 200 |  |  | 300 |  |  | 300 |  |  |
| Lane Util．Factor | 1.00 | 1.00 | 1.00 | 0.97 | 0.95 | 1.00 | 0.97 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1770 | 1863 | 1583 | 3433 | 3539 | 1583 | 3433 | 3539 | 1583 | 1770 | 3539 | 1583 |
| Flt Permitted | 0.604 |  |  | 0.950 |  |  | 0.950 |  |  | 0.104 |  |  |
| Satd．Flow（perm） | 1125 | 1863 | 1583 | 3433 | 3539 | 1583 | 3433 | 3539 | 1583 | 194 | 3539 | 1583 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 250 |  |  | 177 |  |  | 453 |  |  | 167 |
| Link Speed（mph） |  | 45 |  |  | 45 |  |  | 55 |  |  | 55 |  |
| Link Distance（ft） |  | 2032 |  |  | 1524 |  |  | 1735 |  |  | 2505 |  |
| Travel Time（s） |  | 30.8 |  |  | 23.1 |  |  | 21.5 |  |  | 31.1 |  |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj．Flow（vph） | 206 | 218 | 384 | 468 | 237 | 177 | 442 | 1299 | 453 | 158 | 832 | 167 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 206 | 218 | 384 | 468 | 237 | 177 | 442 | 1299 | 453 | 158 | 832 | 167 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width（ft） |  | 24 |  |  | 24 |  |  | 24 |  |  | 24 |  |
| Link Offset（ft） |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width（ft） |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed（mph） | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector（tt） | 20 | 100 | 20 | 20 | 100 | 20 | 20 | 100 | 20 | 20 | 100 | 20 |
| Trailing Detector（ft） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Detector 1 Position（ft） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Detector 1 Size（ft） | 20 | 6 | 20 | 20 | 6 | 20 | 20 | 6 | 20 | 20 | 6 | 20 |
| Detector 1 Type | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | $\mathrm{Cl}+\mathrm{Ex}$ | Cl＋Ex | Cl＋Ex | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | Cl＋Ex | Cl＋Ex |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position（ft） |  | 94 |  |  | 94 |  |  | 94 |  |  | 94 |  |
| Detector 2 Size（ft） |  | 6 |  |  | 6 |  |  | 6 |  |  | 6 |  |
| Detector 2 Type |  | Cl＋Ex |  |  | Cl＋Ex |  |  | Cl＋Ex |  |  | Cl＋Ex |  |

Detector 2 Channel

| Detector 2 Extend（s） |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Turn Type | $\mathrm{pm}+\mathrm{pt}$ | NA | Perm | Prot | NA | Perm | Prot | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 | 6 |
| Permitted Phases | 4 |  | 4 |  |  | 8 |  |  | 2 | 6 |  | 6 |


| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 2 | 2 | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 9.5 | 24.0 | 24.0 | 9.5 | 24.0 | 24.0 | 9.5 | 24.0 | 24.0 | 9.5 | 24.0 | 24.0 |
| Total Split (s) | 17.6 | 24.0 | 24.0 | 20.4 | 26.8 | 26.8 | 22.0 | 55.0 | 55.0 | 10.6 | 43.6 | 43.6 |
| Total Split (\%) | 16.0\% | 21.8\% | 21.8\% | 18.5\% | 24.4\% | 24.4\% | 20.0\% | 50.0\% | 50.0\% | 9.6\% | 39.6\% | 39.6\% |
| Maximum Green (s) | 13.1 | 18.0 | 18.0 | 15.9 | 20.8 | 20.8 | 17.5 | 49.0 | 49.0 | 6.1 | 37.6 | 37.6 |
| Yellow Time (s) | 3.5 | 4.0 | 4.0 | 3.5 | 4.0 | 4.0 | 3.5 | 4.0 | 4.0 | 3.5 | 4.0 | 4.0 |
| All-Red Time (s) | 1.0 | 2.0 | 2.0 | 1.0 | 2.0 | 2.0 | 1.0 | 2.0 | 2.0 | 1.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 6.0 | 6.0 | 4.5 | 6.0 | 6.0 | 4.5 | 6.0 | 6.0 | 4.5 | 6.0 | 6.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | None | None | None | Max | Max | None | Max | Max |
| Walk Time (s) |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk (s) |  | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 11.0 |
| Pedestrian Calls (\#/hr) |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |
| Act Effct Green (s) | 30.0 | 16.2 | 16.2 | 15.9 | 19.8 | 19.8 | 16.8 | 49.0 | 49.0 | 45.9 | 38.3 | 38.3 |
| Actuated g/C Ratio | 0.28 | 0.15 | 0.15 | 0.15 | 0.18 | 0.18 | 0.16 | 0.45 | 0.45 | 0.42 | 0.35 | 0.35 |
| v/c Ratio | 0.54 | 0.78 | 0.86 | 0.93 | 0.37 | 0.41 | 0.83 | 0.81 | 0.47 | 0.92 | 0.66 | 0.25 |
| Control Delay | 31.8 | 64.4 | 34.7 | 72.3 | 40.7 | 8.8 | 58.7 | 30.9 | 3.5 | 76.3 | 33.2 | 5.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 31.8 | 64.4 | 34.7 | 72.3 | 40.7 | 8.8 | 58.7 | 30.9 | 3.5 | 76.3 | 33.2 | 5.0 |
| LOS | C | E | C | E | D | A | E | C | A | E | C | A |
| Approach Delay |  | 41.9 |  |  | 51.0 |  |  | 30.9 |  |  | 35.0 |  |
| Approach LOS |  | D |  |  | D |  |  | C |  |  | D |  |
| Queue Length 50th (ft) | 104 | 147 | 92 | 171 | 77 | 0 | 157 | 412 | 0 | 59 | 264 | 0 |
| Queue Length 95th (ft) | 166 | \#248 | \#249 | \#271 | 115 | 58 | \#229 | 508 | 56 | \#192 | 335 | 46 |
| Internal Link Dist (ft) |  | 1952 |  |  | 1444 |  |  | 1655 |  |  | 2425 |  |
| Turn Bay Length (ft) | 235 |  |  | 235 |  | 235 | 860 |  | 290 | 695 |  | 290 |
| Base Capacity (vph) | 398 | 309 | 472 | 504 | 680 | 447 | 555 | 1603 | 964 | 171 | 1252 | 668 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.52 | 0.71 | 0.81 | 0.93 | 0.35 | 0.40 | 0.80 | 0.81 | 0.47 | 0.92 | 0.66 | 0.25 |

Area Type: Other
Cycle Length: 110
Actuated Cycle Length: 108.2
Natural Cycle: 90
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.93
Intersection Signal Delay: $37.1 \quad$ Intersection LOS: D
Intersection Capacity Utilization 83.0\% ICU Level of Service E
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Splits and Phases: 2: US 24 \& Judge Orr Rd


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh | 7.3 |  |  |  |
| Intersection LOS | A |  | NW | NE |
| Approach | SE | 2 | SW |  |
| Entry Lanes | 2 | 2 | 2 | 2 |
| Conflicting Circle Lanes | 2 | 558 | 2 |  |
| Adj Approach Flow, veh/h | 301 | 568 | 711 | 377 |
| Demand Flow Rate, veh/h | 307 | 582 | 281 | 584 |
| Vehicles Circulating, veh/h | 490 | 410 | 516 | 585 |
| Vehicles Exiting, veh/h | 459 | 0 | 0 | 0 |
| Ped Vol Crossing Leg, \#/h | 0 | 1.000 | 1.000 |  |
| Ped Cap Adj | 1.00 | 8.4 | 7.3 | A |
| Approach Delay, s/veh | 5.9 | A | A |  |
| Approach LOS | A |  |  |  |


| Lane | Left | Right | Left | Right | Left | Right | Left | Right |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Designated Moves | LT | R | LT | TR | L | TR | L | TR |
| Assumed Moves | LT | R | LT | TR | L | TR | L | TR |
| RT Channelized |  |  |  |  |  |  |  |  |
| Lane Util | 0.547 | 0.453 | 0.470 | 0.530 | 0.308 | 0.692 | 0.294 | 0.706 |
| Follow-Up Headway, s | 2.667 | 2.535 | 2.667 | 2.535 | 2.667 | 2.535 | 2.667 | 2.535 |
| Critical Headway, s | 4.645 | 4.328 | 4.645 | 4.328 | 4.645 | 4.328 | 4.645 | 4.328 |
| Entry Flow, veh/h | 168 | 139 | 267 | 301 | 219 | 492 | 113 | 271 |
| Cap Entry Lane, veh/h | 860 | 936 | 790 | 866 | 1042 | 1118 | 803 | 878 |
| Entry HV Adj Factor | 0.983 | 0.978 | 0.981 | 0.982 | 0.982 | 0.980 | 0.982 | 0.981 |
| Flow Entry, veh/h | 165 | 136 | 262 | 296 | 215 | 482 | 111 | 266 |
| Cap Entry, veh/h | 846 | 916 | 776 | 850 | 1023 | 1096 | 789 | 862 |
| V/C Ratio | 0.195 | 0.148 | 0.338 | 0.348 | 0.210 | 0.440 | 0.141 | 0.308 |
| Control Delay, s/veh | 6.3 | 5.4 | 8.7 | 8.2 | 5.5 | 8.0 | 6.0 | 7.6 |
| LOS | A | A | A | A | A | A | A | A |
| 95th \%tile Queue, veh | 1 | 1 | 1 | 2 | 1 | 2 | 0 | 1 |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1.1 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  | * |  |  | * |  | ${ }^{1}$ | t |  | ${ }^{*}$ | F |  |
| Traffic Vol, veh/h | 10 | 0 | 10 | 12 | 0 | 7 | 25 | 490 | 17 | 6 | 325 | 50 |
| Future Vol, veh/h | 10 | 0 | 10 | 12 | 0 | 7 | 25 | 490 | 17 | 6 | 325 | 50 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Stap | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | 50 | - | - | 155 | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 78 | 78 | 78 | 78 | 78 | 78 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 13 | 0 | 13 | 15 | 0 | 9 | 27 | 533 | 18 | 7 | 353 | 54 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 4.9 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ${ }_{\text {¢ }}$ ¢ | 「 | \% | 中 ${ }^{\text {a }}$ |  |  | $\uparrow$ |  |  | $\leftrightarrow$ |  |
| Traffic Vol, veh/h | 19 | 232 | 120 | 150 | 441 | 27 | 60 | 0 | 95 | 19 | 0 | 15 |
| Future Vol, veh/h | 19 | 232 | 120 | 150 | 441 | 27 | 60 | 0 | 95 | 19 | 0 | 15 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Fr | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | 235 | 385 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 93 | 93 | 87 | 87 | 87 | 78 | 78 | 78 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 21 | 252 | 130 | 163 | 474 | 29 | 69 | 0 | 109 | 24 | 0 | 19 |



