

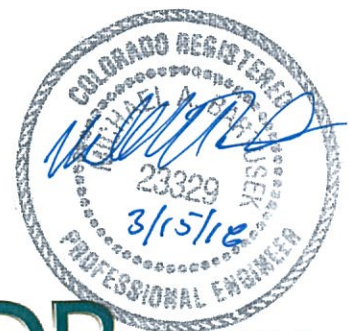
PRELIMINARY/FINAL DRAINAGE REPORT

FOR

SOUTH ACADEMY BUSINESS CENTER

**Prepared For:
10230 Hall Boulevard, LLC
PO Box 38014
Colorado Springs, CO 80937**

**Prepared By:
Associated Design Professionals, Inc.
3520 Austin Bluffs Parkway, Suite 102
Colorado Springs, CO 80918
(719) 266-5212
Project No. 161103
2/27/18
PCD Project No 17-004**

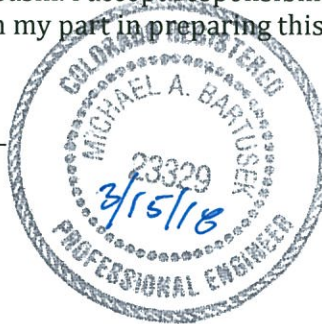


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**ENGINEER'S STATEMENT:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the city/county for drainage reports, and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.


Michael A. Bartusek, P.E. #23329

**DEVELOPER'S STATEMENT:**

I, the Developer, have read and will comply with all of the requirements specified in this drainage report and plan.

By: 
Mr Michael Turley

Title: Manager

Address: 10230 Hall Boulevard, LLC
PO Box 38014
Colorado Springs, CO 80937

EL PASO COUNTY:

Filed in accordance with the El Paso County Land Development Code; the Drainage Criteria Manual, Volumes 1 and 2; and the Engineering Criteria Manual, as amended.

Jennifer Irvine, P.E., County Engineer
ECM Administrator
Conditions:

Approved

by Elizabeth Nijkamp
El Paso County Planning and Community Development
on behalf of Jennifer Irvine, County Engineer, ECM Administrator

Date
04/02/2018 9:33:41 AM





PROJECT DESCRIPTION

This proposed project is contained within a new subdivision named the South Academy Business Center. This currently vacant lot consists of 7.60 acres. It is located in the Southeast Quarter of Section 3, Township 15 South, Range 66 West of the Sixth Principal Meridian, County of El Paso, State of Colorado. The site is located on a narrow strip of land which is bordered on the west by State Highway 85/87 and on the east by the Denver and Rio Grande Western Railroad. Its northern boundary is situated on the south boundary line of the South Academy Boulevard right-of-way.

FLOODPLAIN STATEMENT

This site does not lie within a designated 100-year floodplain as delineated on LOMR No. 03-08-0318P, dated April 9, 2004. It is located within the West Little Johnson drainage basin. The drainage basin map shows a split in the property between the Little Johnson and West Little Johnson Basins. However, field verification revealed that all of the property was located within the West Little Johnson Basin.

SOILS

The soils on the northern site are classified as Blakeland loamy sand by the USDA Soil Conservation Service. This soil is further classified as Hydrologic Soil Group "A". The soils on the proposed site are classified as Nunn clay loam by the USDA Soil Conservation Service. This soil is further classified as Hydrologic Soil Group "C".

METHOD OF COMPUTATION

The methodology utilized for this report is in accordance with *City/County Drainage Criteria Manual*. The Rational Method for computation of runoff was used for determining on-site flows.

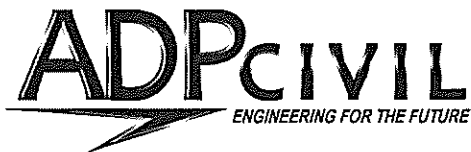
$Q = cia$

Where Q = maximum rate of runoff in cubic feet per second
 c = runoff coefficient representing drainage area characteristics
 i = average rainfall intensity, in inches per hour, for the duration
 required for the runoff to become established
 a = drainage basin size in acres

Off-site flows were determined using the TR20 hydrologic program for project hydrology by the Soil Conservation Service.

EXISTING DRAINAGE CHARACTERISTICS

This previously unplatted site was included in the *Little Johnson/West Little Johnson Drainage Basin Planning Study* prepared by Simons, Li & Associates in 1987. Much of the land north of the proposed project lies within either the Rocky Mountain Materials property or the Stephen Schnurr Living Trust. The Rocky Mountain property encompasses approximately 42 acres of the 54.5-acre basin. The Stephen Schnurr Living Trust owns the 4.6 acres just north of the site. Flows from these properties are released at historic levels onto the site to its south. This vacant land is just north of the proposed project and is covered with rangeland grasses. The tributary area slopes generally southwest at an average slope of one percent. The existing runoff is contained within a broad drainage swale located near the existing railroad tracks.



According to the analysis performed by Simons, Li & Associates, the runoff produced by the entire drainage basin along SH 85/87 would result in no flow for the ten-year storm event and one cfs for the 100-year storm event. The low runoff amounts were due to the Type "A" soils and the long overland flow times. These off-site flows travel to the southeast and are currently directed toward the railroad ditch east of the parcel and do not enter the parcel.

An analysis of the South Academy Business Center site using the Rational Method produced the following flow rates: Sub-Basin A, which drains toward the interior of the parcel and produces 1.6 cfs for the five-year storm and 9.2 cfs for the 100-year storm; Sub-Basin B, which drains to a ditch along SH 85/87 produces a flow of 0.4 cfs for the five-year storm and 2.1 cfs for the 100-year storm. The total flow tributary to the site is 1.9 cfs for the five-year storm and 11.1 cfs for the 100-year storm.

DEVELOPED DRAINAGE CHARACTERISTICS

The proposed development of 7.6 acres will be storage facility comprised of 8' x 40' trailers placed on the site with loose gravel placed over the site.

Runoff from Sub-Basin A will be directed in a southeasterly direction toward the south property line. Based on the proposed developed conditions, Sub-Basin A will produce flows of 4.7 cfs for the five-year storm and 14.3 cfs for the 100-year storm. The detained flows from the Water Quality/Detention Basin will be 1.0 cfs for the five-year storm and 5.0 cfs for the 100-year storm. These detained flows will be directed into an existing grass swale just east of the basin. The existing broad, grassed swale continues flowing to the east at a 0.7% slope with 10:1 side slopes. The 100 year outflow will produce a flow depth of 0.6 ft and a velocity of 1.5 fps.

Runoff from Sub-Basin B will increase slightly to 0.4 cfs for the five-year storm and 2.3 cfs for the 100-year storm. The total flow tributary to the site is 1.4 cfs for the five-year storm and 7.2 cfs for the 100-year storm.

WATER QUALITY/DETENTION REQUIREMENTS

In accordance with current NPDES, stormwater quality BMPs will be provided for this site when it is developed. Based on actual calculations, the commercial development of the site will produce an imperviousness of 48 percent. The water quality component is accomplished by a 2.42' deep 0.703 acre foot private extended detention facility located at the south end of the project. The facility will be maintained by the owner

DRAINAGE BASIN FEE

The proposed development is located within the West Little Johnson drainage basin. The 2017 drainage basin fee calculation is as follows:

| | | |
|-------------------------------|---|-------------------------------|
| Impervious Coverage | = | 48% |
| Area Subject to Fee | = | 0.48 x 7.6 acres = 3.648 acre |
| West Little Johnson Basin Fee | = | \$1,072/acre |
| Drainage Basin Fee | = | \$1,072 x 3.648 = \$3,911 |

There are no associated Bridge Fees for the West Little Johnson drainage basin.



PRIVATE DRAINAGE FACILITIES

| Item | Unit | Quantity | Unit Cost | Total Cost |
|-------------------------------|------|----------|-----------|----------------|
| 18" RCP FES | EA | 1 | \$500 | \$ 600 |
| 18" HDPE | LF | 15 | \$84 | \$ 1,260 |
| Detention Outlet Structure | EA | 1 | \$3,000 | \$ 5,000 |
| Emergency Spillway | EA | 1 | \$1,000 | \$ 1,500 |
| Sub-Total | | | | \$8,360 |
| 15% Contingency & Engineering | | | | \$ 1,254 |
| TOTAL | | | | \$9,614 |

CONCLUSION

Storm runoff from this property will not adversely affect downstream properties or facilities. Grading will take place on the property; therefore, appropriate erosion control measures will be implemented to will include a water quality basin. An on-site detention basin will be incorporated into the parcel to reduce developed flows to historic levels.

Step 1: Runoff has been reduced by disconnecting impervious areas where possible, eliminating "unnecessary" impervious areas and encouraging infiltration into suitable soils.

Step 2: All drainageways, ditches and channels have been stabilized by the following methods:

- New swales within the site are broad and covered with gravel and with a slope of about 0.7% no erosion will take place
- An existing roadside ditch will be enhanced as part of the proposed development.

Step 3: The proposed development will disturb approximately 7.6 acres.

Step 4: The development of this project will not affect sensitive waters.

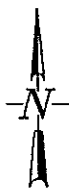
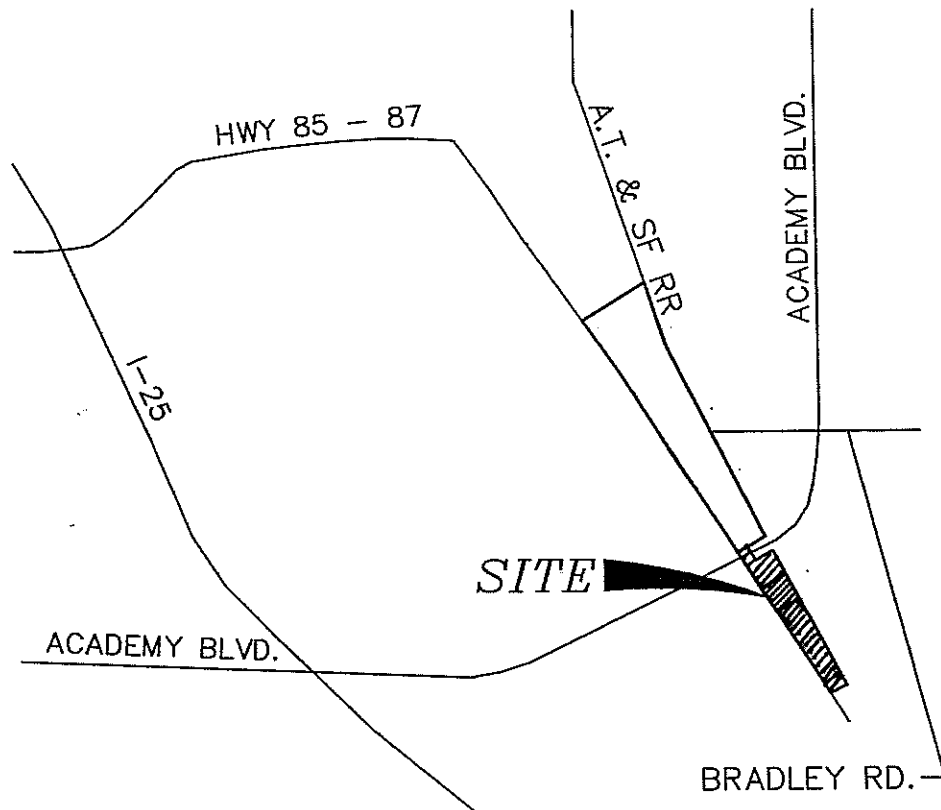
The development of this site will have little impact on downstream properties once the water quality/detention basin is constructed.

REFERENCES

1. City of Colorado Springs and El Paso County (1994). *Drainage Criteria Manual Volume 1* (DCM).
2. City of Colorado Springs and El Paso County (1994). *Drainage Criteria Manual Volume II* (DCM).
3. Soil Survey of El Paso County Area, Colorado by USDA, NRCS.
4. *El Paso County (January 2006) Engineering Criteria Manual*.
5. Urban Drainage and Flood Control District (June 2011). *Urban Storm Drainage Criteria Manual, Volume 1-3*.

**PRELIMINARY/FINAL DRAINAGE REPORT
SOUTH ACADEMY BUSINESS CENTER**

**APPENDIX A
MAPS & EXHIBITS**



VICINITY MAP

N.T.S.

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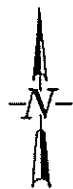
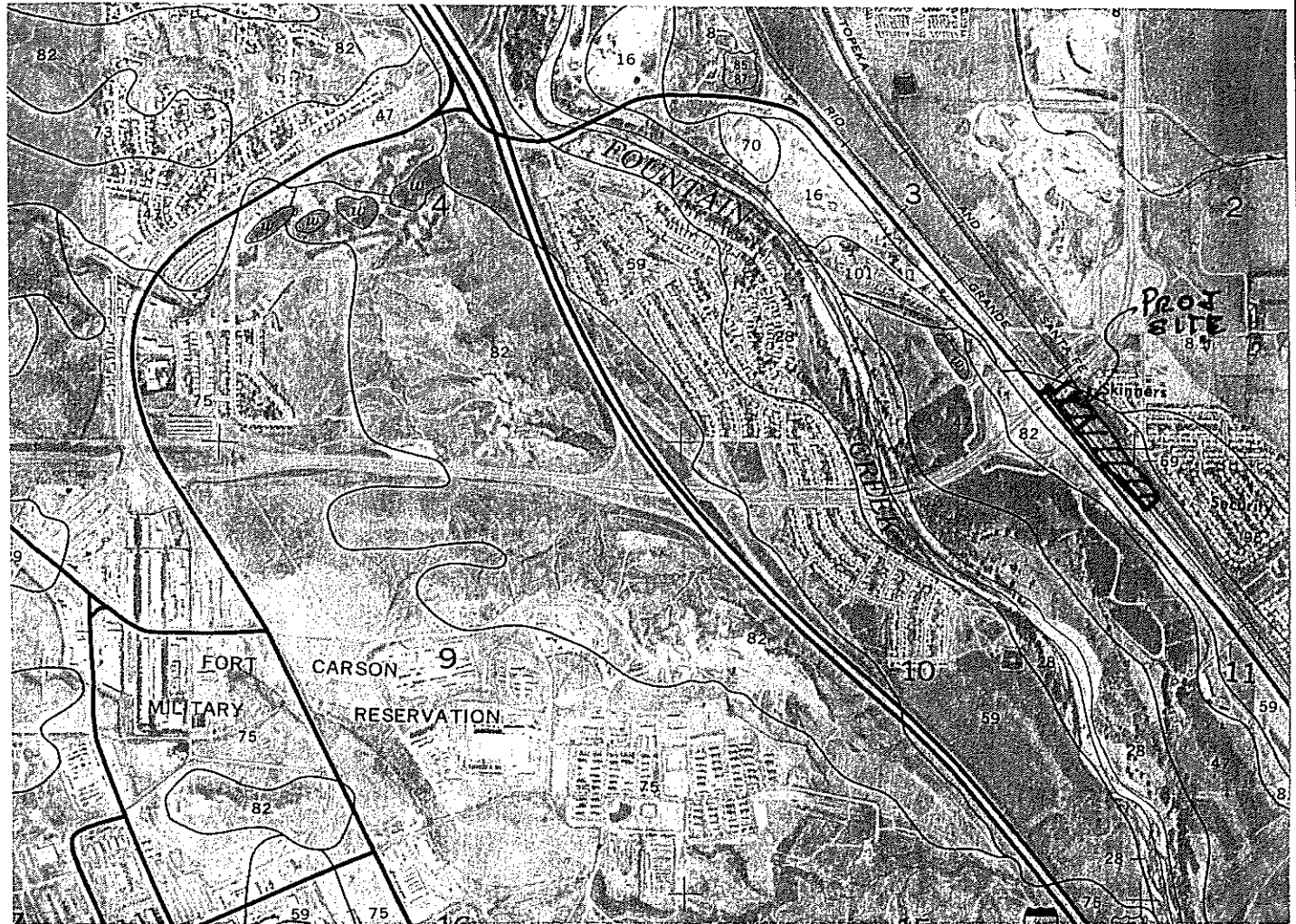
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fax: (719) 266-5341



SOILS MAP

N.T.S.

ADPcIVIL

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**PRELIMINARY/FINAL DRAINAGE REPORT
SOUTH ACADEMY BUSINESS CENTER**

**APPENDIX B
DRAINAGE CALCULATIONS**

| | | | | | | | |
|--------------------------------------|----------------|--------------------------------|-----------------|---------------|---------------------|------------|--|
| SOUTH ACADEMY BUSINESS CENTER | | | | | | | |
| C FACTOR CALCULATION SHEET | | | | | | | |
| | | | | | | | |
| RUNOFF COEFFICIENT | | | | | | | |
| TYPE C SOILS | | | | | | | |
| LAND USE | | | 5 YR | 100 YR | | | |
| | | | | | | | |
| UNDEV & LOOSE GRAVEL | | | 0.15 | 0.5 | | | |
| STREETS/PARKING GRAVEL | | | 0.63 | 0.74 | | | |
| ROOFS/ PAVED AREAS | | | 0.75 | 0.83 | | | |
| | | | | | | | |
| Historic Conditions | | | | | | | |
| | TOTAL | SURFACE CONDITION AREAS | | | CALCULATED C | | |
| AREA | AREA | UNDEV | STREETS/ | ROOFS/ | 5 | 100 | |
| | | | PARKING | PAVED | | | |
| DESIG. | (acre) | | GRAVEL | AREAS | YR | YR | |
| | | | | | | | |
| Aex | 6.40 | 6.40 | | | 0.15 | 0.50 | |
| Bex | 1.30 | 1.30 | | | 0.15 | 0.50 | |
| | | | | | | | |
| RUNOFF COEFFICIENT | | | | | | | |
| TYPE C SOILS | | | | | | | |
| LAND USE | | | 5 YR | 100 YR | | | |
| | | | | | | | |
| UNDEV & LOOSE GRAVEL | | | 0.15 | 0.5 | | | |
| STREETS/PARKING GRAVEL | | | 0.63 | 0.74 | | | |
| ROOFS/ PAVED AREAS | | | 0.75 | 0.83 | | | |
| | | | | | | | |
| Developed Conditions | | | | | | | |
| | TOTAL | SURFACE CONDITION AREAS | | | CALCULATED C | | |
| AREA | AREA | UNDEV | LOOSE | ROOFS/ | 5 | 100 | |
| | | | GRAVEL | PAVED | | | |
| DESIG. | (acre) | | | AREAS | YR | YR | |
| | | | | | | | |
| A | 7.30 | 1.80 | 2.90 | 2.60 | 0.36 | 0.62 | |
| B | 0.30 | 0.30 | | | 0.15 | 0.50 | |
| | | | | | | | |
| IMPERVIOUS | | | | | | | |
| COVERAGE | ACREAGE | % IMP | | | | | |
| Undev | 1.80 | 0 | 0 | | | | |
| Loose Grav | 2.90 | 0.4 | 1.16 | | | | |
| Trailers | 2.60 | 0.9 | 2.34 | | | | |
| | 7.30 | | 3.50 | | | | |
| | | TOTAL IMP | 47.95% | | | | |

| SOUTH ACADEMY BUSINESS CENTER | | | | | | | | | | | | | | | | | | |
|----------------------------------|---------------|----------------------------------|----------|---------------|----------|------------------|-------|-------------------------|--------|-----------|-------|-------|-------|---|---------|-------|-------|--------|
| DRAINAGE CALCULATION SHEET | | | | | | | | | | | | | | | | | | |
| file:lock - load dr | | | | | | | | | | | | | | | | | | |
| 06/09/17 Rev 2/27/18 | | | | | | | | | | | | | | | | | | |
| AREA | AREA | C5 | C100 | C5 X A | C100 X A | Initial Tci | | ti | L (ft) | Slope (%) | V | Tt | TC | I5 | H100 | Q5 | Q100 | AREA |
| DESIG. | (acre) | (5 yr) | (100 yr) | | | L (ft) | (%) | (min) | | | (fps) | (min) | (min) | (in/hr) | (in/hr) | (cfs) | (cfs) | DESIG. |
| CURRENT CONDITIONS | | | | | | | | | | | | | | | | | | |
| OS1 | 54.50 | | | | | | | | | | | | | Flows from this off-site are drain into the railroad ditch and by-pass the proposed development | | | | |
| Aex | 6.30 | 0.15 | 0.50 | 0.95 | 3.15 | 100 | 1.50 | 15.54 | 1900 | 0.70 | 0.90 | 35.19 | 50.73 | 1.67 | 2.91 | 1.58 | 9.18 | Aex |
| Bex | 1.30 | 0.15 | 0.50 | 0.20 | 0.65 | 15 | 1.00 | 6.88 | 1900 | 0.70 | 0.90 | 35.19 | 42.07 | 1.88 | 3.29 | 0.37 | 2.14 | Bex |
| DP1 | 7.60 | | | 1.14 | 3.80 | | | | | | | | 50.73 | 1.67 | 2.91 | 1.90 | 11.07 | DP1 |
| DEVELOPED CONDITIONS | | | | | | | | | | | | | | | | | | |
| OS1 | 54.50 | | | | | | | | | | | | | Flows from this off-site are drain into the railroad ditch and by-pass the proposed development | | | | |
| A | 7.30 | 0.36 | 0.62 | 2.63 | 4.53 | 50 | 1.00 | 9.78 | 1900 | 0.70 | 0.90 | 35.19 | 44.97 | 1.80 | 3.15 | 4.74 | 14.26 | A |
| B | 1.37 | 0.15 | 0.50 | 0.56 | 1.59 | | | | | | | | 44.97 | 1.80 | 3.15 | 1.00 | 5.00 | |
| DP1 | 8.67 | | | 0.77 | 2.28 | 12 | 2.00 | 4.90 | 1900 | 0.70 | 0.90 | 35.19 | 40.08 | 1.94 | 3.39 | 0.40 | 2.32 | B |
| | | | | | | | | | | | | | 44.97 | 1.80 | 3.15 | 1.38 | 7.17 | DP1 |
| DITCH CAPACITY CALCULATION SHEET | | | | | | | | | | | | | | | | | | |
| Swale | | | | | | | | | | | | | | | | | | |
| Location | Q5 cfs | Q100 cfs | S % | B ft | Z | d100 ft | V fps | Froude | Riprap | | | | | | | | | |
| | | | | | | | | # | Size | | | | | | | | | |
| Outlet Swale | 1.00 | 5.00 | 0.70 | 0.00 | 10:1 | 0.60 | 1.50 | 0.52 | | | | | | | | | | |
| Spillway | 4.70 | 14.30 | 1.00 | 10.00 | 4:1 | 0.50 | 2.20 | 0.57 | 0.03 | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| FOREBAY CALCULATION SHEET | | | | | | | | | | | | | | | | | | |
| (Per Table EDB-4) | | | | | | | | | | | | | | | | | | |
| RELEASE RATE | OPENING | VOLUME | | FOREBAY DEPTH | | TRICKLE CHAN CAP | | OUTLET Q = 0.28 cfs | | | | | | | | | | |
| 2% 100 yr slm | Q = C x D^3/2 | 2% WQCV | | D = 6" | | | | | | | | | | | | | | |
| 0.02 X 14.3 = 0.28 cfs | @W = 0.26' | 0.02 X 0.122 ac ft = 0.002 ac ft | | | | | | @d = 4", b= 1', s =0.5% | | | | | | | | | | |
| | Q = 0.28 cfs | 0.002 ac ft x 43560 = 87.1 cf | | | | | | MAX Q = 0.79 cfs | | | | | | | | | | |
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UD-Detention, Version 3.07 (February 2017)

Basin ID: A

Selected BMP Type =

Note: L / W Ratio > 8
 L / W Ratio = 11.4

| | | |
|--|-------|-----------------|
| Zone 1 Volume (WQCV) = | 0.122 | acre-foot |
| Zone 2 Volume (EVR - Zone 1) = | 0.208 | acre-foot |
| Zone 3 (100yr + 1/2 EWR - Zone 2) = | 0.373 | acre-foot |
| Total Detention Basin Volume = | 0.703 | acre-foot |
| Initial Surge Volume (SV) = | user | ft ³ |
| Initial Surge Depth (SD) = | user | ft |
| Total Available Detention Depth (H_{tad}) = | user | ft |
| Depth of Trickle Channel (H_{tc}) = | user | ft |
| Slope of Trickle Channel (S_{tc}) = | user | ft/ft |
| Slopes of Main Basin Sides (S_{mb}) = | user | H:V |
| Basin Length-to-Width Ratio (R_{bw}) = | user | |

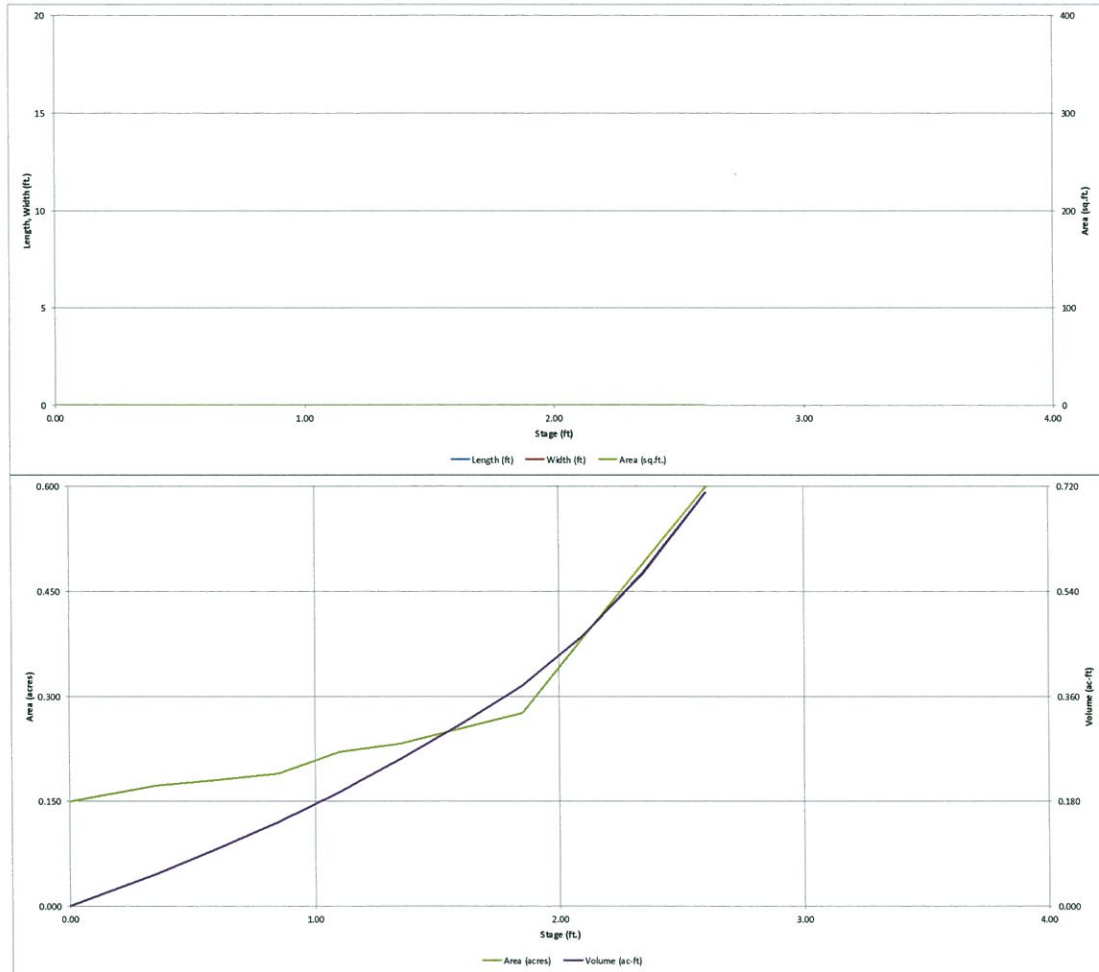
Optional User Override
1-hr Precipitation

| | |
|------|--------|
| 1.19 | inches |
| 1.50 | inches |
| 1.75 | inches |
| 2.00 | inches |
| 2.25 | inches |
| 2.52 | inches |
| 3.01 | inches |

S Acid Bus Ctr Copy of UD-Detention v3.07.xlsm, Basin

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)

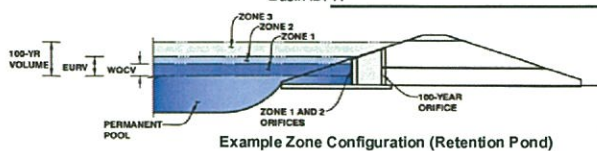


Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)

Project: s Academy Business Ctr

Basin ID: A



Example Zone Configuration (Retention Pond)

| | Stage (ft) | Zone Volume (ac-ft) | Outlet Type |
|----------------------|------------|---------------------|------------------------|
| Zone 1 (WQCV) | 0.65 | 0.122 | Orifice Plate |
| Zone 2 (EURV) | 1.50 | 0.208 | Orifice Plate |
| Zone 3 (100+1/2WQCV) | 2.42 | 0.373 | Weir & Pipe (Restrict) |
| | | 0.703 | Total |

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

| | | |
|-----------------------------------|-----|--|
| Underdrain Orifice Invert Depth = | N/A | ft (distance below the filtration media surface) |
| Underdrain Orifice Diameter = | N/A | inches |

Calculated Parameters for Underdrain

| | | |
|-------------------------------|-----|-----------------|
| Underdrain Orifice Area = | N/A | ft ² |
| Underdrain Orifice Centroid = | N/A | feet |

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

| | | |
|--|------|---|
| Invert of Lowest Orifice = | 0.00 | ft (relative to basin bottom at Stage = 0 ft) |
| Depth at top of Zone using Orifice Plate = | 1.50 | ft (relative to basin bottom at Stage = 0 ft) |
| Orifice Plate: Orifice Vertical Spacing = | 6.00 | inches |
| Orifice Plate: Orifice Area per Row = | 2.45 | sq. inches (diameter = 1-3/4 inches) |

Calculated Parameters for Plate

| | | |
|----------------------------|-----------|-----------------|
| WQ Orifice Area per Row = | 1.701E-02 | ft ² |
| Elliptical Half-Width = | N/A | feet |
| Elliptical Slot Centroid = | N/A | feet |
| Elliptical Slot Area = | N/A | ft ² |

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

| | Row 1 (required) | Row 2 (optional) | Row 3 (optional) | Row 4 (optional) | Row 5 (optional) | Row 6 (optional) | Row 7 (optional) | Row 8 (optional) |
|--------------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| Stage of Orifice Centroid (ft) | 0.00 | 0.50 | 1.00 | | | | | |
| Orifice Area (sq. inches) | 2.45 | 2.45 | 2.45 | | | | | |

| | Row 9 (optional) | Row 10 (optional) | Row 11 (optional) | Row 12 (optional) | Row 13 (optional) | Row 14 (optional) | Row 15 (optional) | Row 16 (optional) |
|--------------------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Stage of Orifice Centroid (ft) | | | | | | | | |
| Orifice Area (sq. inches) | | | | | | | | |

User Input: Vertical Orifice (Circular or Rectangular)

| | Not Selected | Not Selected | |
|---|--------------|--------------|---|
| Invert of Vertical Orifice = | N/A | N/A | ft (relative to basin bottom at Stage = 0 ft) |
| Depth at top of Zone using Vertical Orifice = | N/A | N/A | ft (relative to basin bottom at Stage = 0 ft) |
| Vertical Orifice Diameter = | N/A | N/A | inches |

Calculated Parameters for Vertical Orifice

| | Not Selected | Not Selected | |
|-----------------------------|--------------|--------------|-----------------|
| Vertical Orifice Area = | N/A | N/A | ft ² |
| Vertical Orifice Centroid = | N/A | N/A | feet |

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

| | Zone 3 Weir | Not Selected | |
|---|-------------|--------------|---|
| Overflow Weir Front Edge Height, H _o = | 1.50 | N/A | ft (relative to basin bottom at Stage = 0 ft) |
| Overflow Weir Front Edge Length = | 3.00 | N/A | feet |
| Overflow Weir Slope = | 0.00 | N/A | H:V (enter zero for flat grate) |
| Horiz. Length of Weir Sides = | 3.00 | N/A | feet |
| Overflow Grate Open Area % = | 70% | N/A | % , grate open area/total area |
| Debris Clogging % = | 50% | N/A | % |

Calculated Parameters for Overflow Weir

| | Zone 3 Weir | Not Selected | |
|--|-------------|--------------|-----------------|
| Height of Grate Upper Edge, H _u = | 1.50 | N/A | feet |
| Over Flow Weir Slope Length = | 3.00 | N/A | feet |
| Grate Open Area / 100-yr Orifice Area = | 6.93 | N/A | should be ≥ 4 |
| Overflow Grate Open Area w/o Debris = | 6.30 | N/A | ft ² |
| Overflow Grate Open Area w/ Debris = | 3.15 | N/A | ft ² |

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

| | Zone 3 Restrictor | Not Selected | |
|---|-------------------|--------------|--|
| Depth to Invert of Outlet Pipe = | 0.00 | N/A | ft (distance below basin bottom at Stage = 0 ft) |
| Outlet Pipe Diameter = | 18.00 | N/A | inches |
| Restrictor Plate Height Above Pipe Invert = | 9.20 | | inches |

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

| | Zone 3 Restrictor | Not Selected | |
|--|-------------------|--------------|-----------------|
| Outlet Orifice Area = | 0.91 | N/A | ft ² |
| Outlet Orifice Centroid = | 0.44 | N/A | feet |
| Half-Central Angle of Restrictor Plate on Pipe = | 1.59 | N/A | radians |

User Input: Emergency Spillway (Rectangular or Trapezoidal)

| | | |
|-------------------------------------|------|---|
| Spillway Invert Stage = | 2.42 | ft (relative to basin bottom at Stage = 0 ft) |
| Spillway Crest Length = | 8.00 | feet |
| Spillway End Slopes = | 4.00 | H:V |
| Freeboard above Max Water Surface = | 1.00 | feet |

Calculated Parameters for Spillway

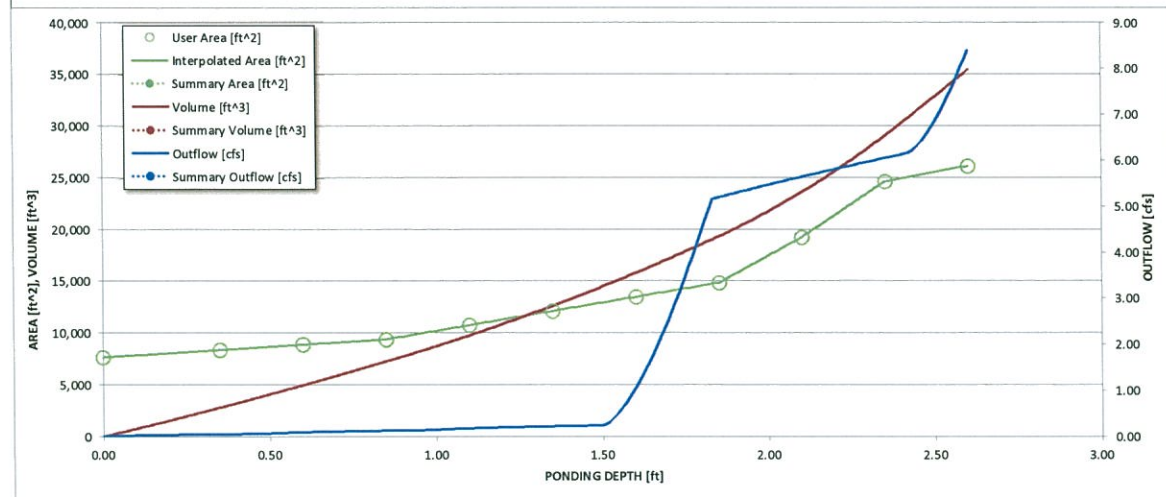
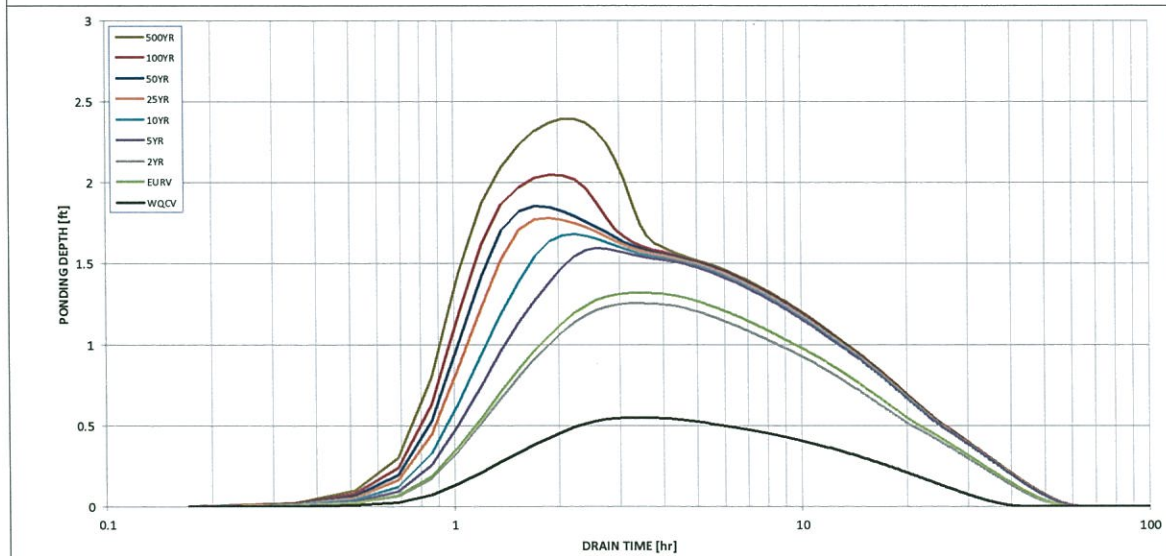
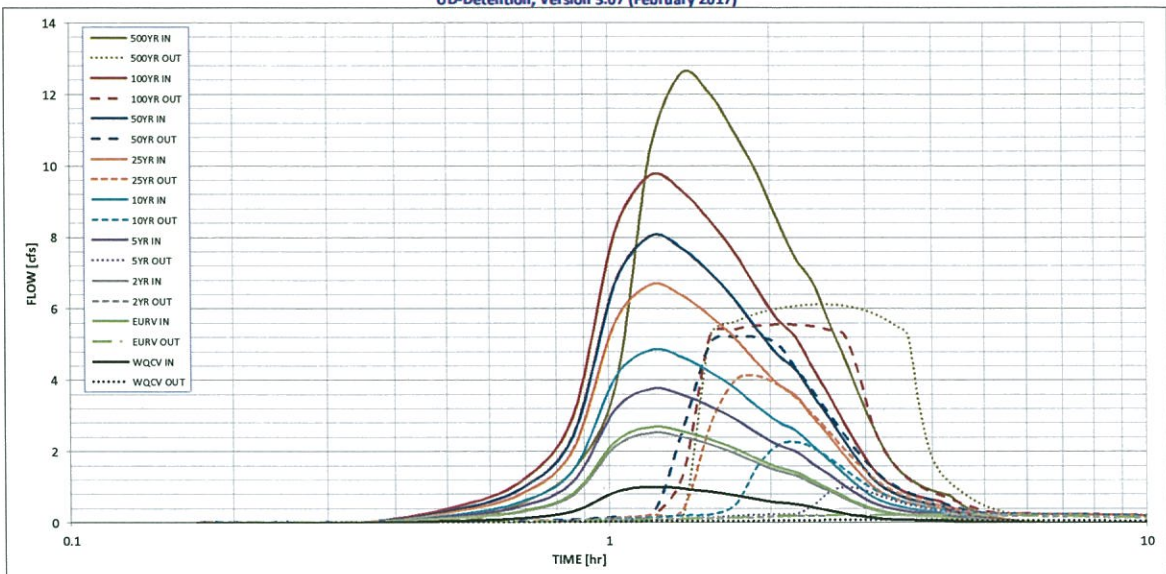
| | | |
|----------------------------------|------|-------|
| Spillway Design Flow Depth = | 0.48 | feet |
| Stage at Top of Freeboard = | 3.90 | feet |
| Basin Area at Top of Freeboard = | 0.60 | acres |

Routed Hydrograph Results

| | WQCV | EURV | 2 Year | 5 Year | 10 Year | 25 Year | 50 Year | 100 Year | 500 Year |
|---|-------|-------|--------|------------------|------------------|------------------|----------------|----------------|----------------|
| Design Storm Return Period = | 0.53 | 1.07 | 1.19 | 1.50 | 1.75 | 2.00 | 2.25 | 2.52 | 3.01 |
| One-Hour Rainfall Depth (in) = | 0.122 | 0.330 | 0.310 | 0.464 | 0.601 | 0.830 | 1.003 | 1.218 | 1.579 |
| OPTIONAL Override Runoff Volume (acre-ft) = | | | | | | | | | |
| Inflow Hydrograph Volume (acre-ft) = | 0.121 | 0.330 | 0.310 | 0.463 | 0.600 | 0.830 | 1.002 | 1.217 | 1.578 |
| Predevelopment Unit Peak Flow, q (cfs/acre) = | 0.00 | 0.00 | 0.01 | 0.07 | 0.19 | 0.47 | 0.62 | 0.82 | 1.15 |
| Predevelopment Peak Q (cfs) = | 0.0 | 0.0 | 0.1 | 0.5 | 1.4 | 3.4 | 4.5 | 6.0 | 8.4 |
| Peak Inflow Q (cfs) = | 1.0 | 2.7 | 2.5 | 3.7 | 4.8 | 6.7 | 8.0 | 9.7 | 12.6 |
| Peak Outflow Q (cfs) = | 0.1 | 0.2 | 0.2 | 1.0 | 2.3 | 4.1 | 5.2 | 5.5 | 6.1 |
| Ratio Peak Outflow to Predevelopment Q = | N/A | N/A | N/A | 2.0 | 1.6 | 1.2 | 1.2 | 0.9 | 0.7 |
| Structure Controlling Flow = | Plate | Plate | Plate | Overflow Grate 1 | Overflow Grate 1 | Overflow Grate 1 | Outlet Plate 1 | Outlet Plate 1 | Outlet Plate 1 |
| Max Velocity through Grate 1 (fps) = | N/A | N/A | N/A | 0.1 | 0.3 | 0.6 | 0.8 | 0.8 | 0.9 |
| Max Velocity through Grate 2 (fps) = | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Time to Drain 97% of Inflow Volume (hours) = | 37 | 48 | 47 | 49 | 47 | 44 | 42 | 40 | 37 |
| Time to Drain 99% of Inflow Volume (hours) = | 40 | 53 | 52 | 55 | 54 | 52 | 51 | 50 | 49 |
| Maximum Ponding Depth (ft) = | 0.55 | 1.32 | 1.25 | 1.59 | 1.68 | 1.78 | 1.85 | 2.05 | 2.39 |
| Area at Maximum Ponding Depth (acres) = | 0.20 | 0.27 | 0.27 | 0.31 | 0.32 | 0.33 | 0.34 | 0.42 | 0.57 |
| Maximum Volume Stored (acre-ft) = | 0.102 | 0.278 | 0.262 | 0.359 | 0.388 | 0.417 | 0.444 | 0.516 | 0.690 |

Detention Basin Outlet Structure Design

UD-Detention, Version 3.07 (February 2017)



| S-A-V-D Chart Axis Override | X-axis | Left Y-Axis | Right Y-Axis |
|-----------------------------|--------|-------------|--------------|
| minimum bound | | | |
| maximum bound | | | |

**PRELIMINARY/FINAL DRAINAGE REPORT
SOUTH ACADEMY BUSINESS CENTER**

**APPENDIX C
DESIGN CHARTS**

Table 6-6. Runoff Coefficients for Rational Method
(Source: UDFCD 2001)

| Land Use or Surface Characteristics | Percent Impervious | Runoff Coefficients | | | | | | | | | | | |
|--|--------------------|---------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|----------|---------|
| | | 2-year | | 5-year | | 10-year | | 25-year | | 50-year | | 100-year | |
| | | HSG A&B | HSG C&D | HSG A&B | HSG C&D | HSG A&B | HSG C&D | HSG A&B | HSG C&D | HSG A&B | HSG C&D | HSG A&B | HSG C&D |
| Business | | | | | | | | | | | | | |
| Commercial Areas | 95 | 0.79 | 0.80 | 0.81 | 0.82 | 0.83 | 0.84 | 0.85 | 0.87 | 0.87 | 0.88 | 0.88 | 0.89 |
| Neighborhood Areas | 70 | 0.45 | 0.49 | 0.49 | 0.53 | 0.53 | 0.57 | 0.58 | 0.62 | 0.60 | 0.65 | 0.62 | 0.68 |
| Residential | | | | | | | | | | | | | |
| 1/8 Acre or less | 65 | 0.41 | 0.45 | 0.45 | 0.49 | 0.49 | 0.54 | 0.54 | 0.59 | 0.57 | 0.62 | 0.59 | 0.65 |
| 1/4 Acre | 40 | 0.23 | 0.28 | 0.30 | 0.35 | 0.36 | 0.42 | 0.42 | 0.50 | 0.46 | 0.54 | 0.50 | 0.58 |
| 1/3 Acre | 30 | 0.18 | 0.22 | 0.25 | 0.30 | 0.32 | 0.38 | 0.39 | 0.47 | 0.43 | 0.52 | 0.47 | 0.57 |
| 1/2 Acre | 25 | 0.15 | 0.20 | 0.22 | 0.28 | 0.30 | 0.36 | 0.37 | 0.46 | 0.41 | 0.51 | 0.46 | 0.56 |
| 1 Acre | 20 | 0.12 | 0.17 | 0.20 | 0.26 | 0.27 | 0.34 | 0.35 | 0.44 | 0.40 | 0.50 | 0.44 | 0.55 |
| Industrial | | | | | | | | | | | | | |
| Light Areas | 80 | 0.57 | 0.60 | 0.59 | 0.63 | 0.63 | 0.66 | 0.66 | 0.70 | 0.68 | 0.72 | 0.70 | 0.74 |
| Heavy Areas | 90 | 0.71 | 0.73 | 0.73 | 0.75 | 0.75 | 0.77 | 0.78 | 0.80 | 0.80 | 0.82 | 0.81 | 0.83 |
| Parks and Cemeteries | 7 | 0.05 | 0.09 | 0.12 | 0.19 | 0.20 | 0.29 | 0.30 | 0.40 | 0.34 | 0.46 | 0.39 | 0.52 |
| Playgrounds | 13 | 0.07 | 0.13 | 0.16 | 0.23 | 0.24 | 0.31 | 0.32 | 0.42 | 0.37 | 0.48 | 0.41 | 0.54 |
| Railroad Yard Areas | 40 | 0.23 | 0.28 | 0.30 | 0.35 | 0.36 | 0.42 | 0.42 | 0.50 | 0.46 | 0.54 | 0.50 | 0.58 |
| Undeveloped Areas | | | | | | | | | | | | | |
| Historic Flow Analysis-- Greenbelts, Agriculture | 2 | 0.03 | 0.05 | 0.09 | 0.16 | 0.17 | 0.26 | 0.26 | 0.38 | 0.31 | 0.45 | 0.36 | 0.51 |
| Pasture/Meadow | 0 | 0.02 | 0.04 | 0.08 | 0.15 | 0.15 | 0.25 | 0.25 | 0.37 | 0.30 | 0.44 | 0.35 | 0.50 |
| Forest | 0 | 0.02 | 0.04 | 0.08 | 0.15 | 0.15 | 0.25 | 0.25 | 0.37 | 0.30 | 0.44 | 0.35 | 0.50 |
| Exposed Rock | 100 | 0.89 | 0.89 | 0.90 | 0.90 | 0.92 | 0.92 | 0.94 | 0.94 | 0.95 | 0.95 | 0.96 | 0.96 |
| Offsite Flow Analysis (when landuse is undefined) | 45 | 0.26 | 0.31 | 0.32 | 0.37 | 0.38 | 0.44 | 0.44 | 0.51 | 0.48 | 0.55 | 0.51 | 0.59 |
| Streets | | | | | | | | | | | | | |
| Paved | 100 | 0.89 | 0.89 | 0.90 | 0.90 | 0.92 | 0.92 | 0.94 | 0.94 | 0.95 | 0.95 | 0.96 | 0.96 |
| Gravel | 80 | 0.57 | 0.60 | 0.59 | 0.63 | 0.63 | 0.66 | 0.66 | 0.70 | 0.68 | 0.72 | 0.70 | 0.74 |
| Drive and Walks | 100 | 0.89 | 0.89 | 0.90 | 0.90 | 0.92 | 0.92 | 0.94 | 0.94 | 0.95 | 0.95 | 0.96 | 0.96 |
| Roofs | 90 | 0.71 | 0.73 | 0.73 | 0.75 | 0.75 | 0.77 | 0.78 | 0.80 | 0.80 | 0.82 | 0.81 | 0.83 |
| Lawns | 0 | 0.02 | 0.04 | 0.08 | 0.15 | 0.15 | 0.25 | 0.25 | 0.37 | 0.30 | 0.44 | 0.35 | 0.50 |

Figure 6-25. Estimate of Average Concentrated Shallow Flow

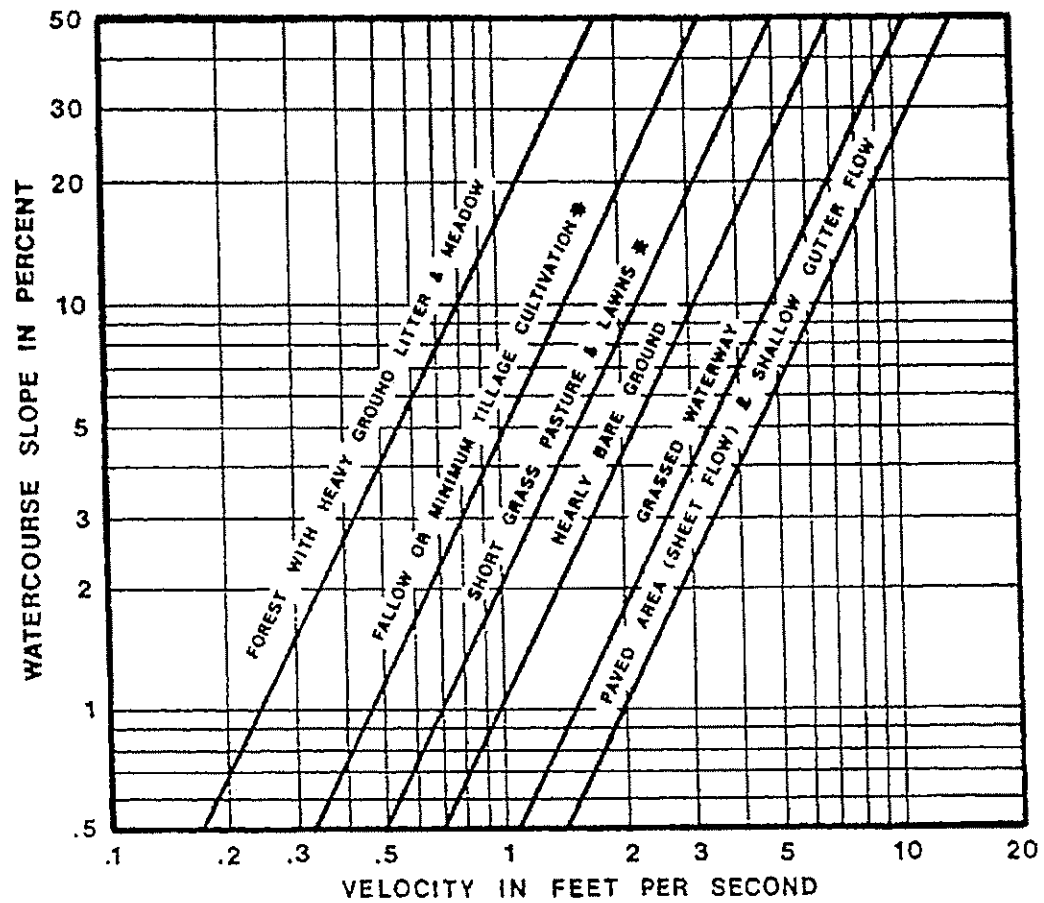
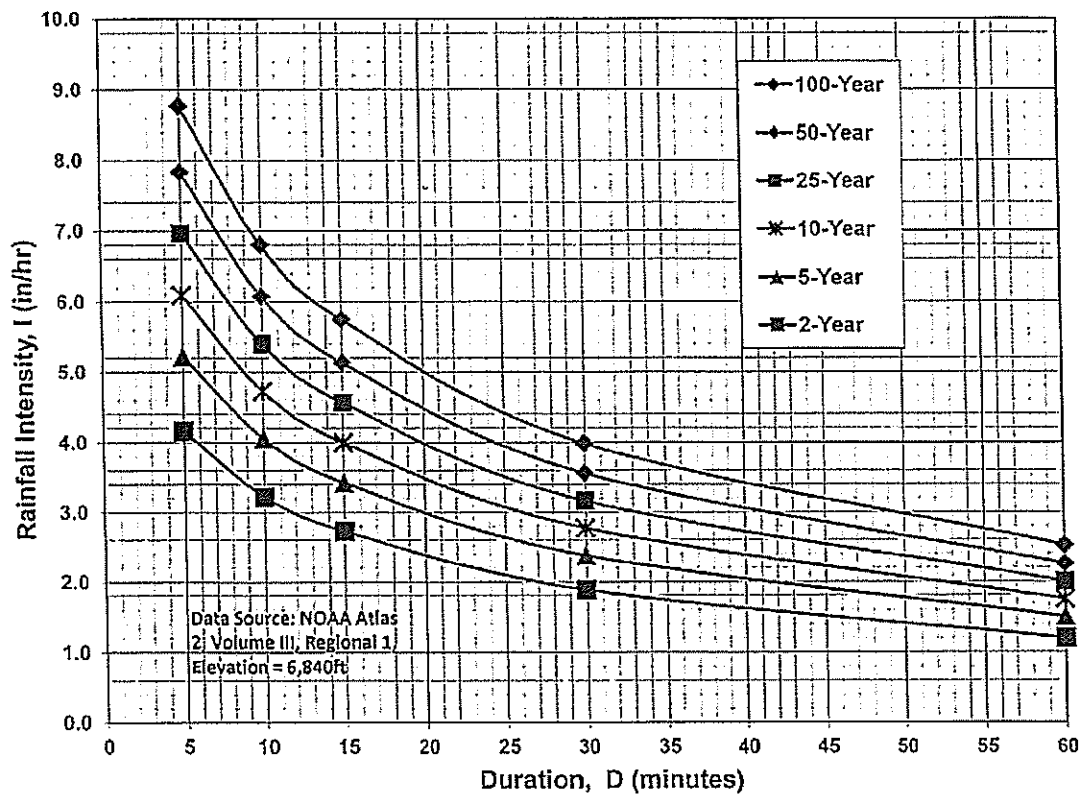


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency



IDF Equations

$$I_{100} = -2.52 \ln(D) + 12.735$$

$$I_{50} = -2.25 \ln(D) + 11.375$$

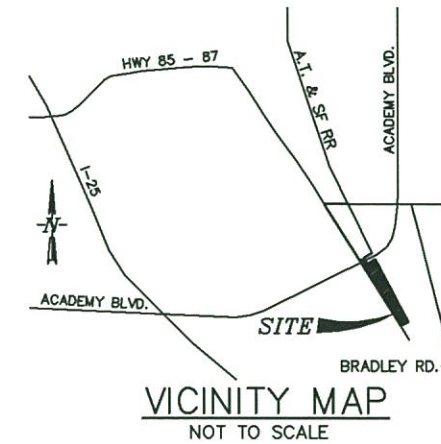
$$I_{25} = -2.00 \ln(D) + 10.111$$

$$I_{10} = -1.75 \ln(D) + 8.847$$

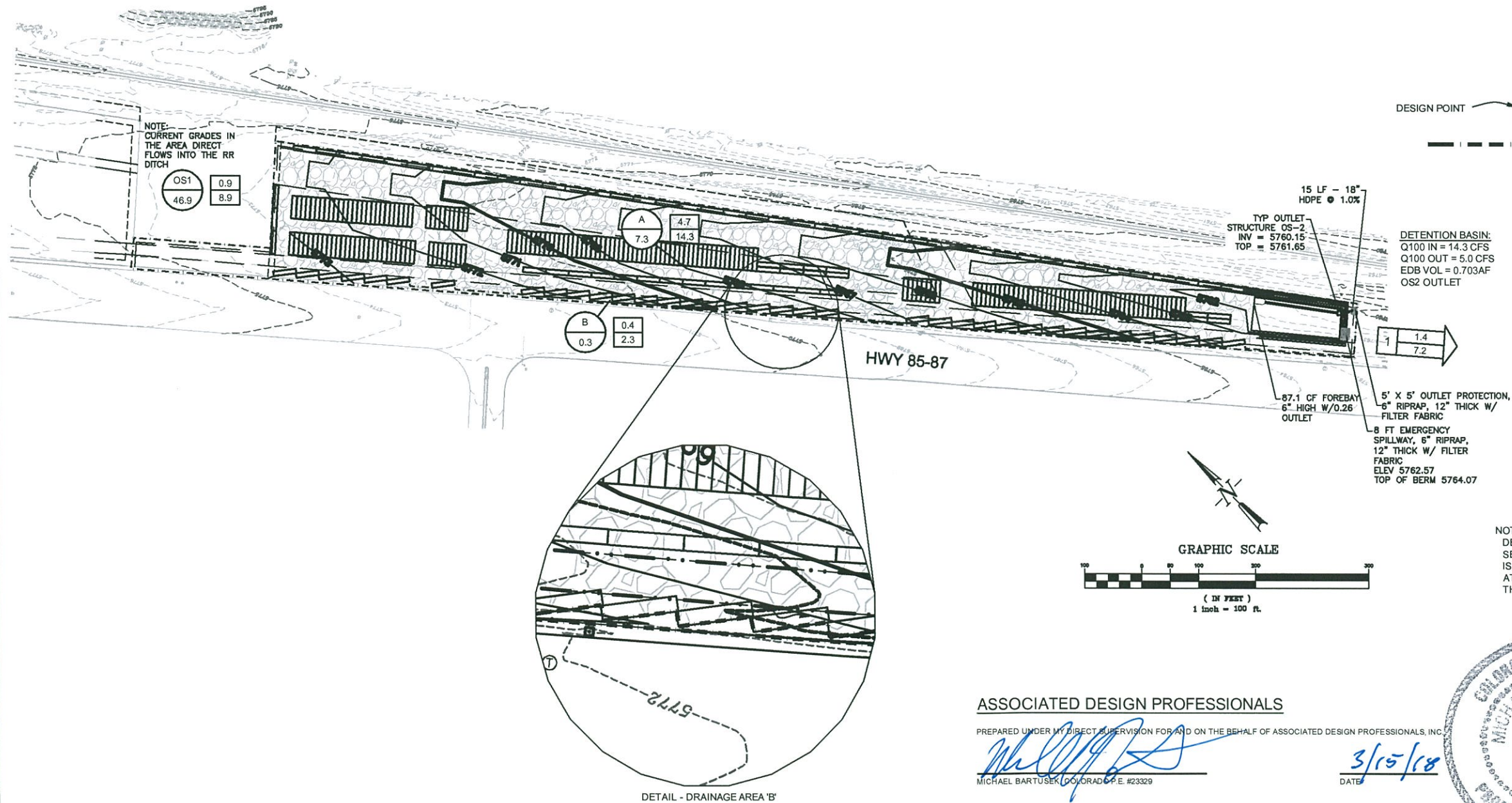
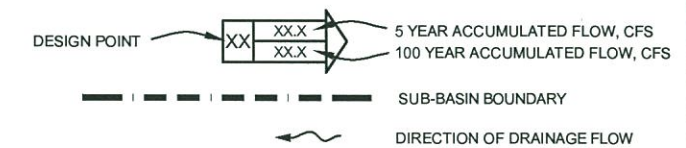
$$I_5 = -1.50 \ln(D) + 7.583$$

$$I_2 = -1.19 \ln(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure.



LEGEND



NOTE:
DETENTION POND AREA TO BE UTILIZED AS A
SEDIMENTATION BASIN UNTIL EARTH MOVING
IS COMPLETED AND THE GROUND STABILIZED,
AT WHICH TIME IT WILL BE CLEANED OUT AND
THE DETENTION POND STRUCTURES ADDED.

ASSOCIATED DESIGN PROFESSIONALS

PREPARED UNDER MY DIRECT SUPERVISION FOR AND ON THE BEHALF OF ASSOCIATED DESIGN PROFESSIONALS, INC.

MICHAEL BARTUSEK COLORADO P.E. #23329

DATE 3/15/18

